

Your Project Calculations



Project Name: RUSTED GATE VERSION 2

S3D Model Link:

https://platform.skyciv.com/structural?preload_name=RUSTED%20GATE%20VERSION%202&preload_path=Shared%20Enterprise%20Folder/MT_Solar_Projects/5_2023

Public Model Link:

https://platform.skyciv.com/structural-viewer?project_id=lfktgBb3xSCfDvBYtBklelRkGImGG0UEcCft7wvHOYVvbfIvyudBjXt01Irs7qw

Array Specification

| | |
|-----------------------------|------------------------------|
| Product: | Beam |
| Unique ID: | 1P-0-6TOP-SD-72-L-4Hx3W-JFK4 |
| Duty Classification: | SD |
| Module Width: | 40.00 in |
| Module Length: | 79.00in |
| Number of Rows: | 4 |
| Number of Columns: | 3 |
| Total Number of Modules: | 12 |
| Desired Tilt Angle: | 25 |
| Front Edge Clearance: | 10 |
| Total Array Height at Tilt: | 15.67 ft |
| Total Frame Length: | 19.50 ft |
| Frame Weight: | 1097 lbs |
| Array Dimensions N/S: | 13.50 ft |
| Array Dimensions E/W: | 20.00 ft |
| Rail Length: | 162.00 in |
| Rail Spacing: | 3.29 ft |
| Rail Check: | Not Checked |

Support Specifications

| | |
|--------------------------|-----------------|
| Pole Size: | 6in Pipe Sch 80 |
| Pole Length above Grade: | 12.85 ft |
| Number of Poles: | 1 |
| Pole Spacing: | 0 |

Foundation Specifications

| | |
|---------------------------------|----------------------|
| Foundation Type: | Square |
| Foundation Dimensions: | 48 x 48 in |
| Foundation Depth (below grade): | Pile 1: 6.25 ft |
| Foundation Volume: | 3.704 y ³ |
| Foundation Result: | PASSED |
| Mount Twist: | 0.000002 kip |

Site Info

| | |
|----------------------------|---|
| Risk Category: | I |
| Exposure: | C |
| Soil Classification: | sand |
| Site Location: | 5700 Upton Rd, Central Point, OR 97502, USA |
| Wind Speed: | 90 mph |
| Snow Load: | 15 psf |
| Design Uplift Pressure: | Multiple pressures |
| Design Downforce Pressure: | Multiple pressures |
| Design Snow Pressure: | 0.007423 ksf |



Design Disclaimer

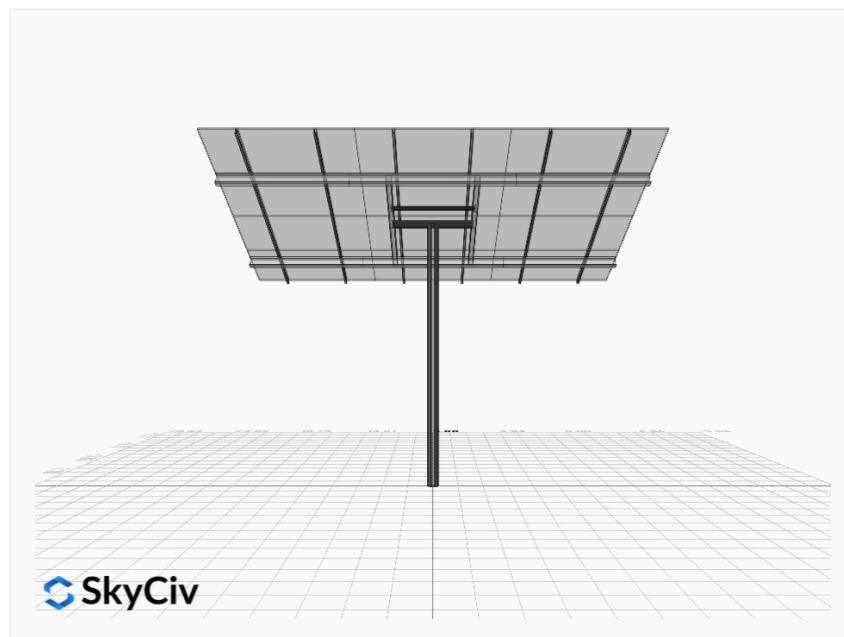
This software should be used for preliminary designs and should not be used as a final design unless reviewed, verified and designed by a qualified structural engineer.

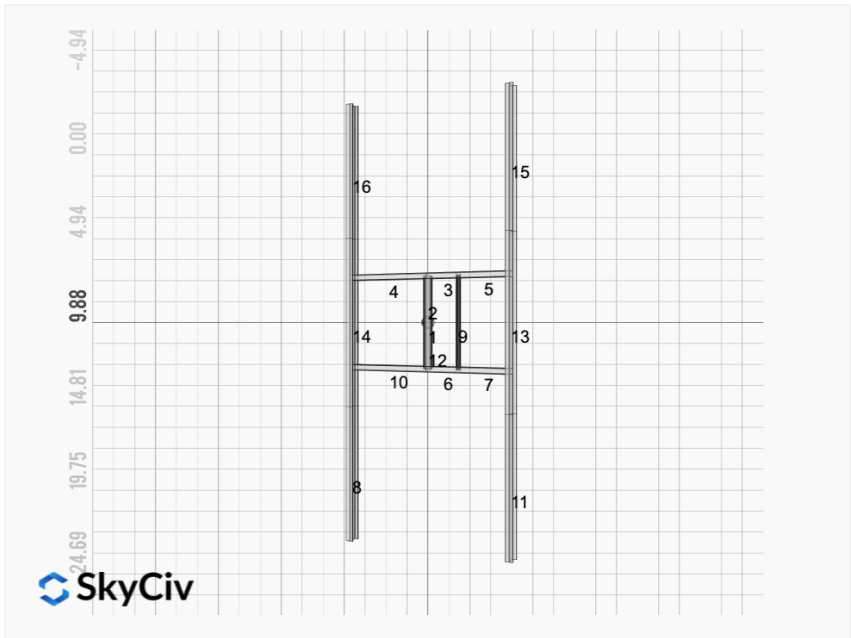
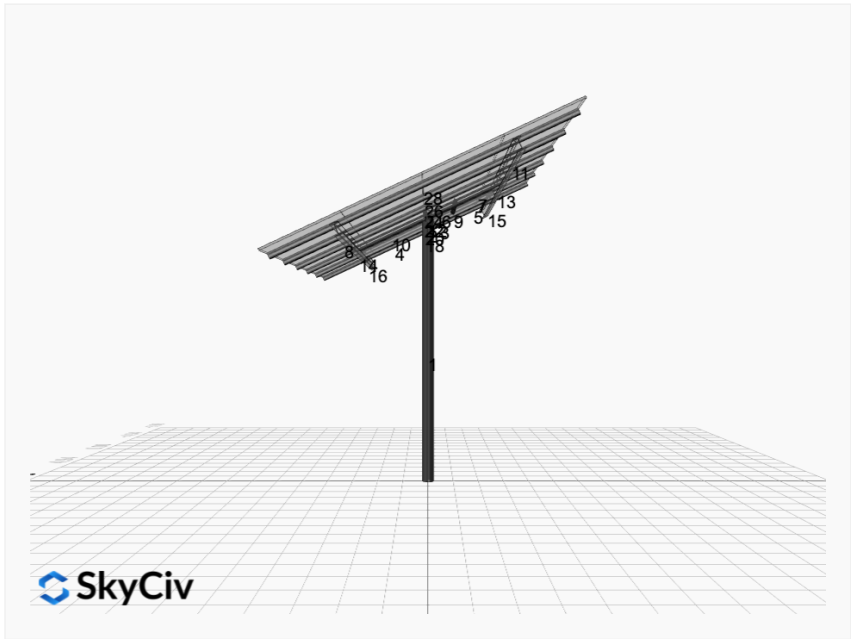
AutoDesigner Input

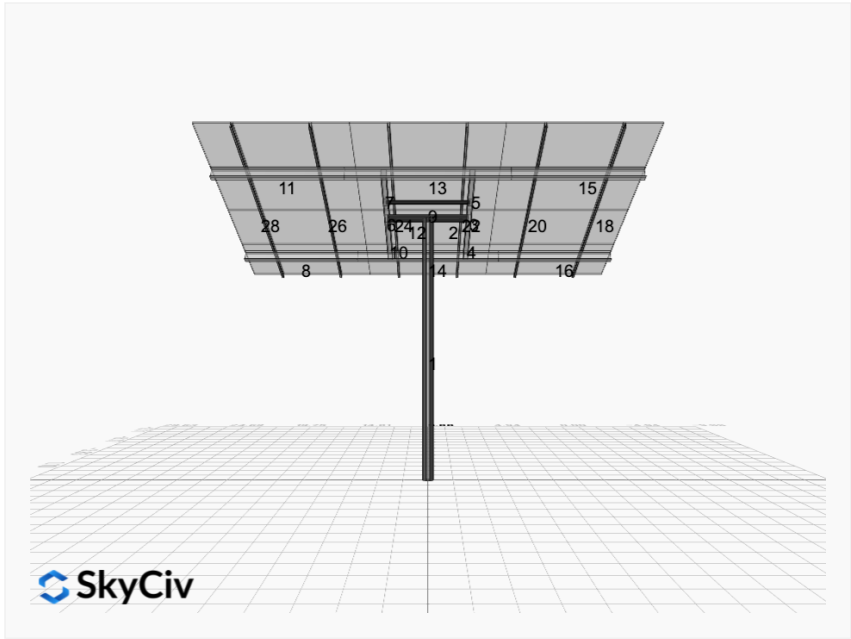
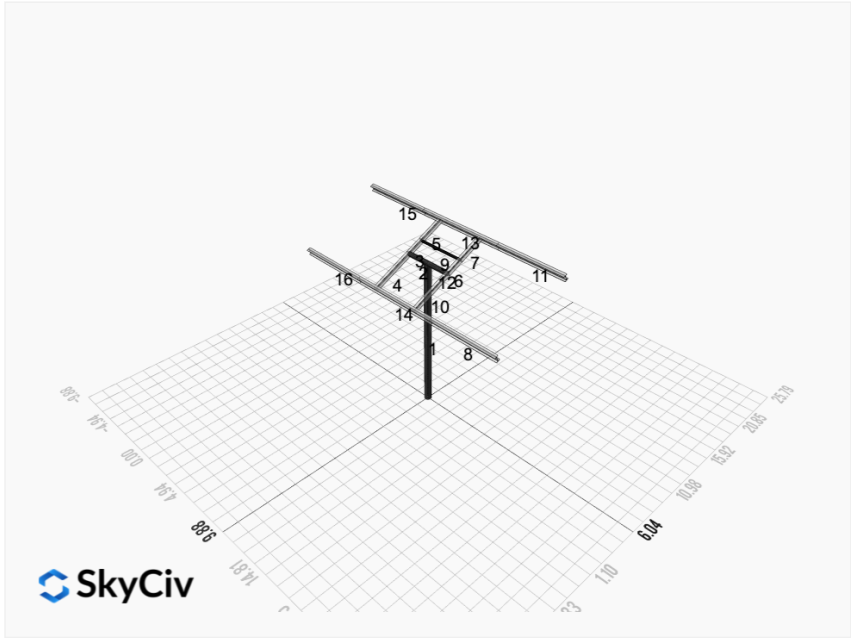
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Design Notes:

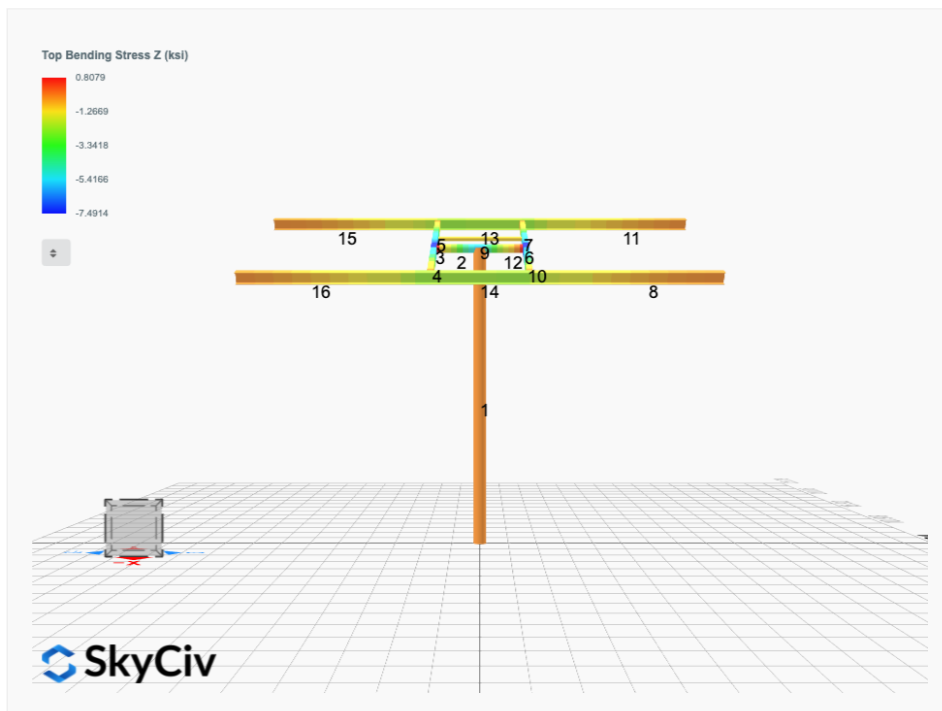
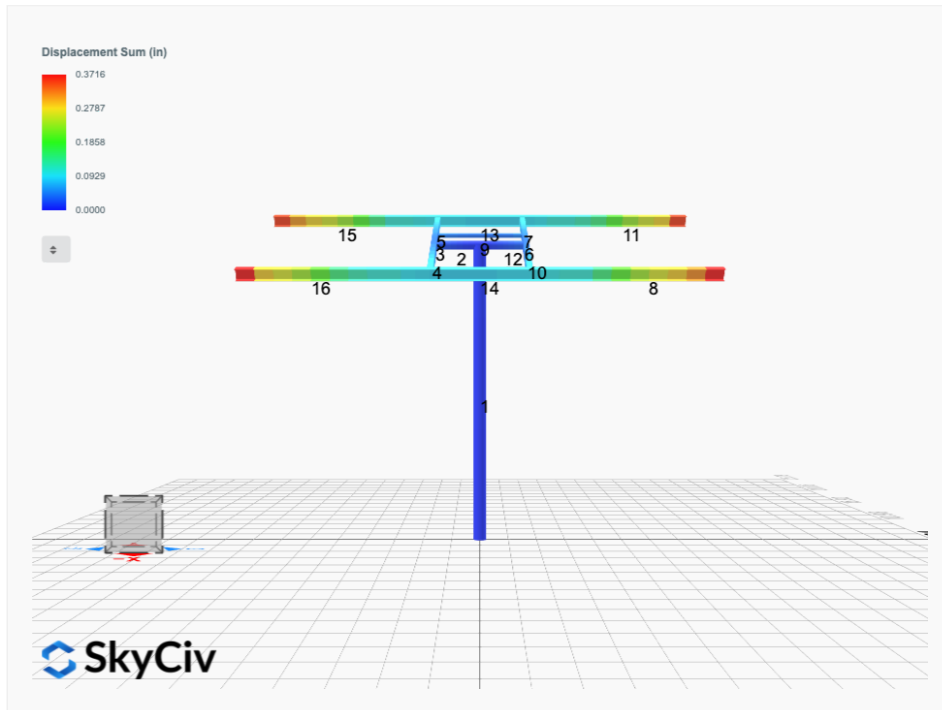
- AISC Deflection checks are set to L/1 due to structure design intent
- Foundation Design and Sizing is approximate only

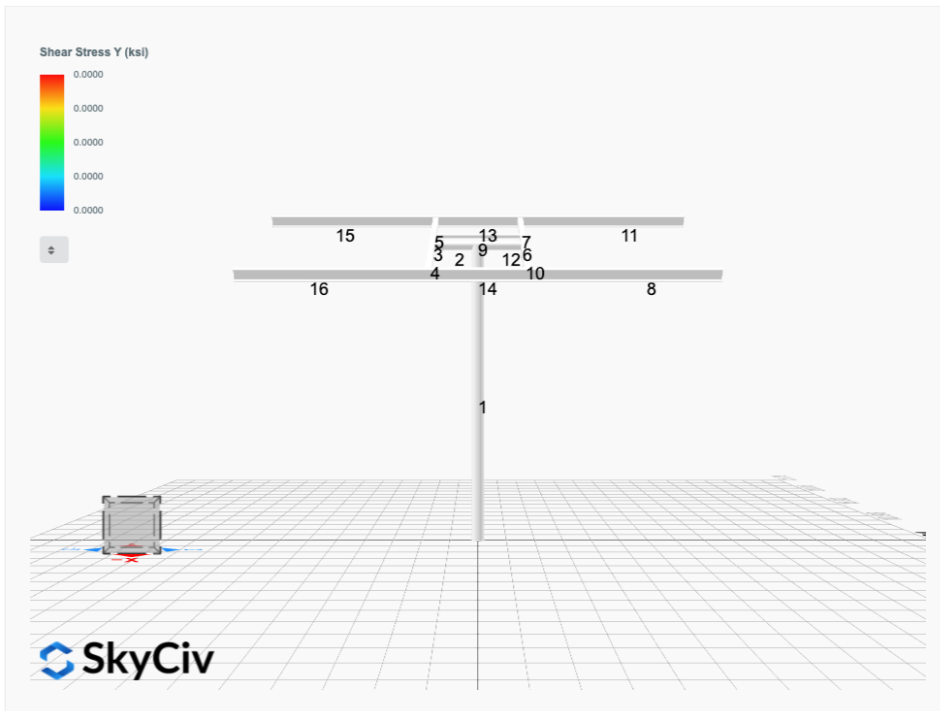
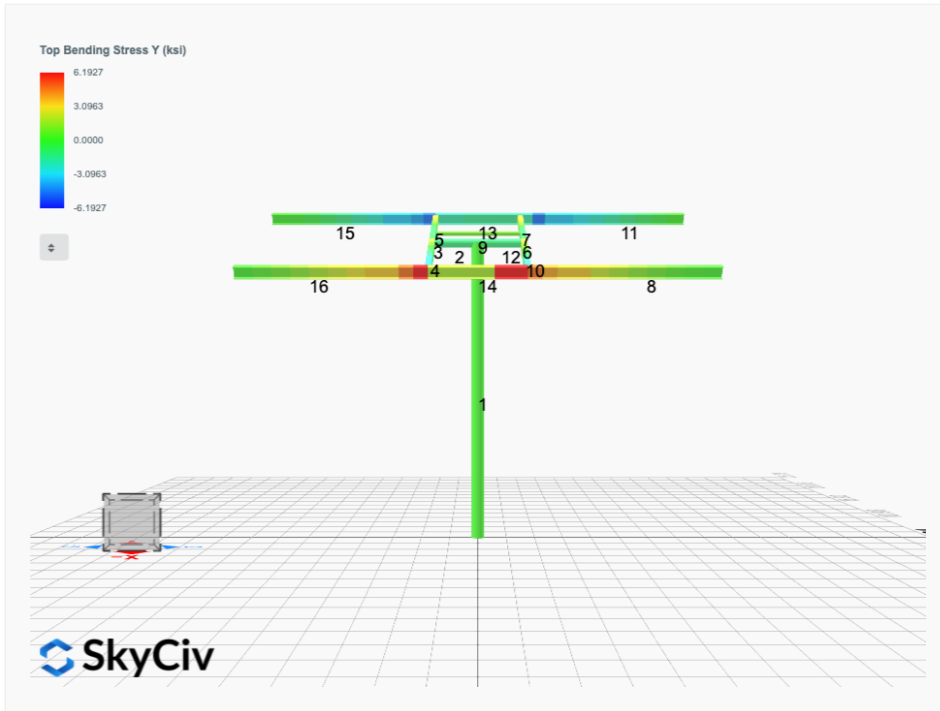


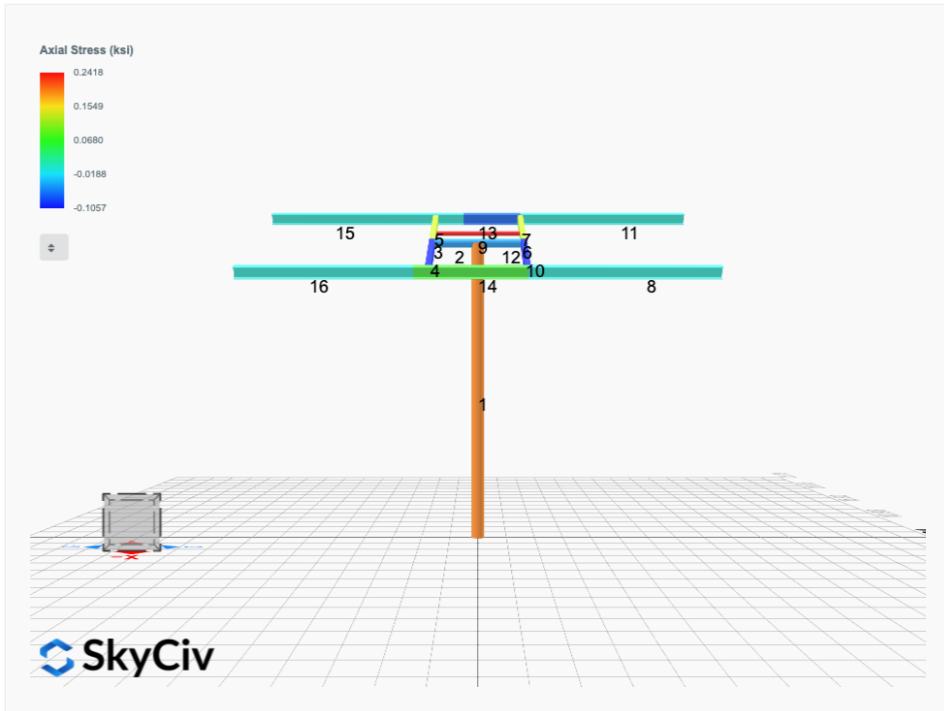




FEM Results (Envelope Worst Case for each member)







Reaction Forces for Foundation 1 (Node ID#1), (kip, kip-ft)

ASD Load Combination Results

| Name | Fx | Fy | Fz | Mx | My | Mz |
|---|---------|---------|---------|--------|---------|----------|
| ULS: 1. D | 0.0000 | 2.1314 | -0.0000 | 0.0000 | -0.0000 | 0.0214 |
| ULS: 2. D + L | 0.0000 | 2.1314 | -0.0000 | 0.0000 | -0.0000 | 0.0214 |
| ULS: 3. D + (S or Lr or R) | 0.0000 | 3.9023 | 0.0000 | 0.0000 | -0.0000 | 0.0258 |
| ULS: 3. D + (S or Lr or R) | 0.0000 | 2.1314 | -0.0000 | 0.0000 | -0.0000 | 0.0214 |
| ULS: 4. D + 0.75L + 0.75(S or Lr or R) | 0.0000 | 3.4596 | 0.0000 | 0.0000 | -0.0000 | 0.0247 |
| ULS: 4. D + 0.75L + 0.75(S or Lr or R) | 0.0000 | 2.1314 | -0.0000 | 0.0000 | -0.0000 | 0.0214 |
| ULS: 5b. D + 0.7E | 0.0000 | 2.1314 | -0.0000 | 0.0000 | -0.0000 | 0.0214 |
| ULS: 6b. D + 0.75L + 0.75(0.7)E + 0.75S | 0.0000 | 3.4596 | 0.0000 | 0.0000 | -0.0000 | 0.0247 |
| ULS: 8. 0.6D + 0.7E | 0.0000 | 1.2789 | -0.0000 | 0.0000 | -0.0000 | 0.0128 |
| ULS: 5a. D + 0.6W_Wind downforce Case A only | -1.5530 | 5.4619 | -0.0000 | 0.0000 | -0.0000 | 21.0262 |
| ULS: 5a. D + 0.6W_Wind downforce Case B only | -1.5530 | 5.4619 | -0.0000 | 0.0000 | -0.0000 | 21.0262 |
| ULS: 5a. D + 0.6W_Wind uplift Case A only | 1.3589 | -0.7828 | -0.0000 | 0.0000 | -0.0000 | -16.6587 |
| ULS: 5a. D + 0.6W_Wind uplift Case B only | 1.1648 | -0.3665 | -0.0000 | 0.0000 | -0.0000 | -21.8598 |
| ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind downforce Case A only | -1.1648 | 5.9575 | -0.0000 | 0.0000 | -0.0000 | 15.7783 |
| ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind downforce Case B only | -1.1648 | 5.9575 | -0.0000 | 0.0000 | -0.0000 | 15.7783 |
| ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind uplift Case A only | 1.0192 | 1.2740 | -0.0000 | 0.0000 | -0.0000 | -12.4853 |
| ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind uplift Case B only | 0.8736 | 1.5862 | 0.0000 | 0.0000 | -0.0000 | -16.3862 |
| ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind downforce Case A only | -1.1648 | 4.6293 | -0.0000 | 0.0000 | -0.0000 | 15.7750 |
| ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind downforce Case B only | -1.1648 | 4.6293 | -0.0000 | 0.0000 | -0.0000 | 15.7750 |
| ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind uplift Case A only | 1.0192 | -0.0542 | -0.0000 | 0.0000 | -0.0000 | -12.4887 |
| ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind uplift Case B only | 0.8736 | 0.2580 | -0.0000 | 0.0000 | -0.0000 | -16.3895 |
| ULS: 7. 0.6D + 0.6W_Wind downforce Case A only | -1.5530 | 4.6094 | -0.0000 | 0.0000 | -0.0000 | 21.0176 |
| ULS: 7. 0.6D + 0.6W_Wind downforce Case B only | -1.5530 | 4.6094 | -0.0000 | 0.0000 | -0.0000 | 21.0176 |
| ULS: 7. 0.6D + 0.6W_Wind uplift Case A only | 1.3589 | -1.6353 | -0.0000 | 0.0000 | -0.0000 | -16.6672 |
| ULS: 7. 0.6D + 0.6W_Wind uplift Case B only | 1.1648 | -1.2190 | 0.0000 | 0.0000 | -0.0000 | -21.8684 |

Worst Case Reactions LRFD

These calculations are taken directly from the FEA via SkyCiv and are used in the Concrete Checks of the Foundation Module.
Note: Worst case values are assumed as downforce wind load cases.

| Result | Value (kip, kip-ft) |
|------------------|---------------------|
| Axial | 8.9940 |
| Shear X | -2.5884 |
| Shear Z | -0.0000 |
| Moment X | -0.0000 |
| Moment Y (Twist) | 0.0000 |
| Moment Z | 37.4396 |

Worst Case Reactions ASD

These results are taken from the worst case values in the above table and are used in the Soil Checks in the Foundation Module.
Note: Worst case values are assumed as downforce wind load cases.

| Result | Value (kip, kip-ft) |
|------------------|---------------------|
| Axial | 5.9575 |
| Shear X | -1.5530 |
| Shear Z | -0.0000 |
| Moment X | 0.0000 |
| Moment Y (Twist) | 0.0000 |
| Moment Z | 21.8684 |

Project Details

Design Code: AISC 360-16 LRFD
 Provision: LRFD
 Country: United States

User Name: sales@mtsolar.us
 Project Name: RUSTED GATE VERSION 2
 Unit System: imperial



Design Input Information

| Design Factors | | | |
|----------------|----------|----------|----------|
| Φ_t | Φ_c | Φ_b | Φ_v |
| 0.9 | 0.9 | 0.9 | 0.9 |

| Design Materials | | | |
|------------------|---------|----------------------|----------------------|
| ID | E (ksi) | F _y (ksi) | F _u (ksi) |
| 1 | 29000 | 50 | 65 |

Section Dimensions

| ID | Name | d (in) | t _w (in) | | | | |
|----|-----------------|--------|---------------------|--|--|--|--|
| 1 | 2in Pipe Sch 40 | 2.38 | 0.15 | | | | |
| 4 | 4in Pipe Sch 40 | 4.50 | 0.24 | | | | |
| 8 | 6in Pipe Sch 80 | 6.63 | 0.43 | | | | |

| ID | Name | d (in) | b (in) | t _w (in) | t _b (in) | r (in) | |
|----|------------|--------|--------|---------------------|---------------------|--------|--|
| 15 | HSS5x3x1/8 | 5.00 | 3.00 | 0.12 | 0.12 | 0.12 | |

| ID | Name | d (in) | t _w (in) | b _t (in) | b _b (in) | t _t (in) | t _b (in) | r (in) |
|----|------|--------|---------------------|---------------------|---------------------|---------------------|---------------------|--------|
| 18 | W6x9 | 5.90 | 0.17 | 3.94 | 3.94 | 0.21 | 0.21 | 0.25 |

| Section Properties | | | | | | | | |
|--------------------|-----------------|----------------------|----------------------|------------------------------------|------------------------------------|-----------------------------------|------------------------------------|------------------------------------|
| ID | Name | A (in ²) | J (in ⁴) | I _{yp} (in ⁴) | I _{zp} (in ⁴) | I _w (in ⁶) | S _{yp} (in ³) | S _{zp} (in ³) |
| 1 | 2in Pipe Sch 40 | 1.07 | 1.33 | 0.67 | 0.67 | 0.00 | 0.76 | 0.76 |
| 4 | 4in Pipe Sch 40 | 3.17 | 14.47 | 7.23 | 7.23 | 0.00 | 4.31 | 4.31 |

| | | | | | | |
|----|--------|--------|-------|-------|-------|-------|
| 10 | 79.65 | 72.01 | 10.99 | 4.60 | 29.14 | 16.61 |
| 11 | 120.60 | 21.74 | 23.36 | 6.45 | 30.09 | 45.74 |
| 12 | 142.83 | 141.72 | 16.17 | 16.17 | 42.85 | 42.85 |
| 13 | 120.60 | 98.23 | 17.96 | 6.45 | 30.09 | 45.74 |
| 14 | 120.60 | 98.23 | 17.96 | 6.45 | 30.09 | 45.74 |
| 15 | 120.60 | 21.74 | 23.36 | 6.45 | 30.09 | 45.74 |
| 16 | 120.60 | 21.74 | 23.36 | 6.45 | 30.09 | 45.74 |

Design Ratio

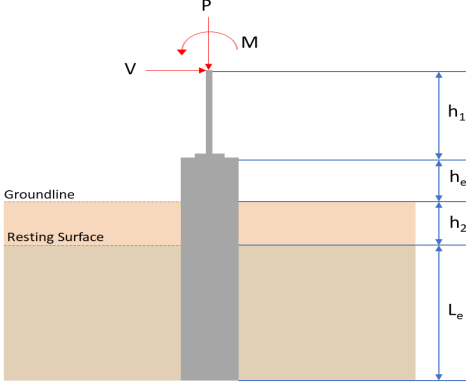
| Member ID | P | M _z | M _y | V _y | V _z | (P,M _z ,M _y) | Worst LC | KL/r | δ | Status |
|-----------|-------|----------------|----------------|----------------|----------------|-------------------------------------|----------|--------------|--------------|--------|
| 1 | 0.103 | 0.602 | 0.000 | 0.023 | 0.000 | 0.629 | #13 | 0.738 | Not Required | Pass |
| 2 | 0.004 | 0.484 | 0.175 | 0.100 | 0.030 | 0.660 | #13 | 0.034 | Not Required | Pass |
| 3 | 0.007 | 0.759 | 0.061 | 0.077 | 0.004 | 0.788 | #13 | 0.044 | Not Required | Pass |
| 4 | 0.006 | 0.738 | 0.239 | 0.074 | 0.028 | 0.825 | #13 | 0.078 | Not Required | Pass |
| 5 | 0.007 | 0.471 | 0.253 | 0.076 | 0.038 | 0.512 | #13 | 0.073 | Not Required | Pass |
| 6 | 0.007 | 0.760 | 0.061 | 0.077 | 0.004 | 0.789 | #13 | 0.044 | Not Required | Pass |
| 7 | 0.007 | 0.471 | 0.253 | 0.076 | 0.038 | 0.512 | #13 | 0.073 | Not Required | Pass |
| 8 | 0.000 | 0.169 | 0.144 | 0.044 | 0.007 | 0.289 | #21 | Not Required | Not Required | Pass |
| 9 | 0.016 | 0.090 | 0.047 | 0.001 | 0.000 | 0.142 | #13 | 0.198 | Not Required | Pass |
| 10 | 0.006 | 0.738 | 0.239 | 0.074 | 0.028 | 0.825 | #13 | 0.078 | Not Required | Pass |
| 11 | 0.000 | 0.174 | 0.144 | 0.045 | 0.007 | 0.291 | #21 | Not Required | Not Required | Pass |
| 12 | 0.004 | 0.484 | 0.175 | 0.100 | 0.030 | 0.660 | #13 | 0.034 | Not Required | Pass |
| 13 | 0.005 | 0.381 | 0.241 | 0.058 | 0.009 | 0.560 | #21 | 0.177 | Not Required | Pass |
| 14 | 0.005 | 0.378 | 0.241 | 0.057 | 0.009 | 0.555 | #21 | 0.177 | Not Required | Pass |
| 15 | 0.000 | 0.174 | 0.144 | 0.045 | 0.007 | 0.291 | #21 | Not Required | Not Required | Pass |
| 16 | 0.000 | 0.169 | 0.144 | 0.044 | 0.007 | 0.289 | #21 | Not Required | Not Required | Pass |

Definitions

| | |
|-------------------------------------|---|
| Φ_t | Safety factor for tensile |
| Φ_c | Safety factor for compression |
| Φ_b | Safety factor for flexure |
| Φ_v | Safety factor for shear |
| E | Modulus of elasticity |
| F _y | Specified minimum yield stress |
| F _u | Specified minimum tensile strength |
| A | Cross-sectional area |
| J | Torsional constant |
| I _{yp} | Moment of inertia about the Y axes |
| I _{zp} | Moment of inertia about the Z axes |
| I _w | Warping constant |
| S _{yp} | Plastic section modulus about the Y axis |
| S _{zp} | Plastic section modulus about the Z axis |
| KL | Effective length |
| C _b | Buckling modification factor (from all load combinations) |
| L _b | Length between braced points |
| LST | Limited slenderness for tension |
| LSC | Limited slenderness for compression |
| LD | Limited deflection |
| P _n | Nominal axial strength (tension/compression) |
| M _n | Nominal flexural strength (about Z/Y axis) |
| V _n | Nominal shear strength (along Z/Y axis) |
| P | Design ratio in case of axial force |
| M _z | Design ratio in case of bending about Z axis |
| M _y | Design ratio in case of bending about Y axis |
| V _y | Design ratio in case of shear along Y axis |
| V _z | Design ratio in case of shear along Z axis |
| (P,M _z ,M _y) | Design ratio in case of axial force and bending action |
| KL/r | Design ratio in case of section slenderness |
| δ | Design ratio in case of member deflection |
| OK | Capacity is provided |

OK
NG

Capacity is provided
Capacity is not provided

| REFERENCES | CALCULATIONS | RESULTS | | | | | | | | | | | | | | | | | | | | | | | | | | |
|----------------|--|--|---|--|---|---|---|----------|---------|----------------|-----|------|-----------|-------|-------|-------------|--------|--------|-------------|-------|-------|---------------|-------|-------|---------------|--------|--------|--|
| | <p>SkyCiv Foundation Design Pile Foundation</p> <p>Design Information : Design code : IBC 2021 (International Building Code) Unit System : Imperial</p> | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | <p>Pile Input</p>  <p>Geometry Pile shape: rectangular $b = 48$ in - Pile width $D = 48$ in - Pile depth $L = 6.25$ ft - Total pile length $h_1 = 0$ ft - Lateral load height from the top of the pile, $h_2 = 0$ ft - Depth to resting surface $h_e = 0$ ft - Length of pile above the ground</p> <p>Tabulation of Soil Parameters</p> <table border="1" data-bbox="416 1102 1193 1191"> <thead> <tr> <th>Layer</th> <th>Label</th> <th>Allowable Bearing Pressure (q_a) (psf)</th> <th>Allowable Lateral Pressure (R) (psf/ft)</th> </tr> </thead> <tbody> <tr> <td>1</td> <td>Sand, silty sand, clayey sand, silty gravel & clayey gravel</td> <td>2000.000</td> <td>150.000</td> </tr> </tbody> </table> <p>Tabulation of Loads</p> <table border="1" data-bbox="676 1285 935 1458"> <thead> <tr> <th>Load Component</th> <th>ASD</th> <th>LRFD</th> </tr> </thead> <tbody> <tr> <td>P (kip)</td> <td>5.957</td> <td>8.994</td> </tr> <tr> <td>V_x (kip)</td> <td>-1.553</td> <td>-2.588</td> </tr> <tr> <td>V_z (kip)</td> <td>0.000</td> <td>0.000</td> </tr> <tr> <td>M_x (kipft)</td> <td>0.000</td> <td>0.000</td> </tr> <tr> <td>M_z (kipft)</td> <td>21.868</td> <td>37.440</td> </tr> </tbody> </table> <p>Material Properties $f'_{ck} = 3$ ksi - Concrete strength,</p> | Layer | Label | Allowable Bearing Pressure (q_a) (psf) | Allowable Lateral Pressure (R) (psf/ft) | 1 | Sand, silty sand, clayey sand, silty gravel & clayey gravel | 2000.000 | 150.000 | Load Component | ASD | LRFD | P (kip) | 5.957 | 8.994 | V_x (kip) | -1.553 | -2.588 | V_z (kip) | 0.000 | 0.000 | M_x (kipft) | 0.000 | 0.000 | M_z (kipft) | 21.868 | 37.440 | |
| Layer | Label | Allowable Bearing Pressure (q_a) (psf) | Allowable Lateral Pressure (R) (psf/ft) | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1 | Sand, silty sand, clayey sand, silty gravel & clayey gravel | 2000.000 | 150.000 | | | | | | | | | | | | | | | | | | | | | | | | | |
| Load Component | ASD | LRFD | | | | | | | | | | | | | | | | | | | | | | | | | | |
| P (kip) | 5.957 | 8.994 | | | | | | | | | | | | | | | | | | | | | | | | | | |
| V_x (kip) | -1.553 | -2.588 | | | | | | | | | | | | | | | | | | | | | | | | | | |
| V_z (kip) | 0.000 | 0.000 | | | | | | | | | | | | | | | | | | | | | | | | | | |
| M_x (kipft) | 0.000 | 0.000 | | | | | | | | | | | | | | | | | | | | | | | | | | |
| M_z (kipft) | 21.868 | 37.440 | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | <p>Required depth to resist lateral loads (ASD) H - Point of application of the lateral load</p> $H = h_1 + h_2 + h_e$ $H = (0 \text{ ft}) + (0 \text{ ft}) + (0 \text{ ft})$ $H = 0 \text{ ft}$ <p>Considering x-direction: H_o - Lateral force per length of pile,</p> $H_o = \frac{V_x}{1.57 D}$ $H_o = \frac{(-1.553 \text{ kip})}{1.57 \times (48 \text{ in})}$ $H_o = -0.24729 \text{ kip/ft}$ <p>M_o - Moment per length of pile,</p> $M_o = \frac{M_z + (V_x H)}{1.57 D}$ | | | | | | | | | | | | | | | | | | | | | | | | | | | |

| | | |
|----------|--|---|
| | $M_o = \frac{(21.868 \text{ kipft}) + ((-1.553 \text{ kip}) \times (0 \text{ ft}))}{1.57 \times (48 \text{ in})}$ $M_o = 3.4822 \text{ kipft/ft}$ <p>Required depth of embedment in earth:</p> $L_x^3 - \left(14.14 \times \frac{H_o \times L_x}{R}\right) - \left(18.85 \times \frac{M_o}{R}\right) = 0$ <p>Solving the cubic equation: $L_{e,x} = 5.7775 \text{ ft}$ - Required depth in x-direction,</p> <p>Considering z-direction: $L_{e,z} = 0 \text{ ft}$ - Required depth in z-direction,</p> <p>Minimum embedded depth required: $L_{e,req}$ - Depth of pile required,</p> $L_{e,req} = \text{MAX}[L_{e,x}, L_{e,z}]$ $L_{e,req} = \text{MAX}[(5.7775 \text{ ft}), (0 \text{ ft})]$ $L_{e,req} = 5.778 \text{ ft}$ <p>L_e - Actual embedded length of pile,</p> $L_e = L - h_e - h_2$ $L_e = (6.25 \text{ ft}) - (0 \text{ ft}) - (0 \text{ ft})$ $L_e = 6.25 \text{ ft}$ <p><i>Ratio</i> - Embedded depth</p> $\text{Ratio} = \frac{L_{e,req}}{L_e}$ $\text{Ratio} = \frac{(5.778 \text{ ft})}{(6.25 \text{ ft})}$ $\text{Ratio} = 0.92448$ | <p>Status: PASS Ratio: 0.920</p> |
| | <p>End-bearing Capacity (ASD)</p> <p>A - Pile cross-section area</p> $A = b D$ $A = (48 \text{ in}) \times (48 \text{ in})$ $A = 16 \text{ ft}^2$ <p>q - End-bearing pressure</p> $q = \frac{P_u}{A}$ $q = \frac{(5.957 \text{ kip})}{(16 \text{ ft}^2)}$ $q = 0.37231 \text{ kip/ft}^2$ <p>Check bearing capacity ratio:</p> <p><i>Ratio</i> - Capacity</p> $\text{Ratio} = \frac{q}{q_o}$ $\text{Ratio} = \frac{(0.37231 \text{ kip/ft}^2)}{(2000 \text{ psf})}$ $\text{Ratio} = 0.18616$ | <p>Status: PASS Ratio: 0.190</p> |
| Czerniak | <p>Lateral Soil Pressure (ASD):</p> <p>L/D - Length to least lateral dimension ratio,</p> $L/D = \frac{L}{D}$ $L/D = \frac{(6.25 \text{ ft})}{(48 \text{ in})}$ | |

$$L/D = 1.5625$$

Since $L/D \leq 10$,

Pile is short.

Considering x-direction:

$H_o = -0.24729$ kip/ft - Lateral force per length of pile,

$M_o = 3.4822$ kipft/ft - Overturning moment per length of pile,

a - Distance from resting surface to pivot point,

$$a = \frac{(4 M_o L_e) + (3 H_o L_e^2)}{(6 M_o) + (4 H_o L_e)}$$

$$a = \frac{(4 \times (3.4822 \text{ kipft/ft}) \times (6.25 \text{ ft})) + (3 \times (-0.24729 \text{ kip/ft}) \times (6.25 \text{ ft})^2)}{(6 \times (3.4822 \text{ kipft/ft})) + (4 \times (-0.24729 \text{ kip/ft}) \times (6.25 \text{ ft}))}$$

$$a = 4.2856 \text{ ft}$$

p - Earth pressure against the pile at distance $a/2$ from resting surface,

$$p = \frac{0.75 [(4 M_o) + (3 H_o L_e)]^2}{L_e^2 [(3 M_o) + (2 H_o L_e)]}$$

$$p = \frac{0.75 \times [(4 \times (3.4822 \text{ kipft/ft})) + (3 \times (-0.24729 \text{ kip/ft}) \times (6.25 \text{ ft}))]^2}{(6.25 \text{ ft})^2 \times [(3 \times (3.4822 \text{ kipft/ft})) + (2 \times (-0.24729 \text{ kip/ft}) \times (6.25 \text{ ft}))]}$$

$$p = 0.22538 \text{ kip/ft}^2$$

s - Earth pressure against the pile at distance L_e ,

$$s = \frac{6 [(2 M_o) + (H_o L_e)]}{L_e^2}$$

$$s = \frac{6 \times [(2 \times (3.4822 \text{ kipft/ft})) + ((-0.24729 \text{ kip/ft}) \times (6.25 \text{ ft}))]}{(6.25 \text{ ft})^2}$$

$$s = 0.83232 \text{ kip/ft}^2$$

Check lateral soil pressure capacity:

p_a - Allowable lateral soil pressure at depth $a/2$,

$$p_a = R \frac{a}{2}$$

$$p_a = (150 \text{ psf/ft}) \times \frac{(4.2856 \text{ ft})}{2}$$

$$p_a = 0.32142 \text{ kip/ft}^2$$

Ratio - Lateral soil capacity

$$\text{Ratio} = \frac{p}{p_a}$$

$$\text{Ratio} = \frac{(0.22538 \text{ kip/ft}^2)}{(0.32142 \text{ kip/ft}^2)}$$

$$\text{Ratio} = 0.70119$$

p_s - Allowable lateral soil pressure at depth L_e ,

$$p_s = R L_e$$

$$p_s = (150 \text{ psf/ft}) \times (6.25 \text{ ft})$$

$$p_s = 0.9375 \text{ kip/ft}^2$$

Ratio - Lateral soil capacity

$$\text{Ratio} = \frac{s}{p_s}$$

$$\text{Ratio} = \frac{(0.83232 \text{ kip/ft}^2)}{(0.9375 \text{ kip/ft}^2)}$$

$$\text{Ratio} = 0.88781$$

Status: **PASS**
Ratio: **0.700**

Status: **PASS**
Ratio: **0.890**





Shear force and Bending moment (x-direction, LRFD)

H_o - Lateral force per length of pile,

$$H_o = \frac{V_x}{1.57 D}$$

$$H_o = \frac{(-2.588 \text{ kip})}{1.57 \times (48 \text{ in})}$$

$$H_o = -0.4121 \text{ kip/ft}$$

M_o - Moment per length of pile,

$$M_o = \frac{M_x + (V_x H)}{1.57 D}$$

$$M_o = \frac{(37.44 \text{ kipft}) + ((-2.588 \text{ kip}) \times (0 \text{ ft}))}{1.57 \times (48 \text{ in})}$$

$$M_o = 5.9618 \text{ kipft/ft}$$

E - Distance from lateral load to resisting surface,

$$E = \frac{M_o}{H_o}$$

$$E = \frac{(5.9618 \text{ kipft/ft})}{(-0.4121 \text{ kip/ft})}$$

$$E = 14.467 \text{ ft}$$

a - Distance from resting surface to pivot point,

$$a = \frac{(4 M_o L_c) + (3 H_o L_c^2)}{(6 M_o) + (4 H_o L_c)}$$

$$a = \frac{(4 \times (5.9618 \text{ kipft/ft}) \times (6.25 \text{ ft})) + (3 \times (-0.4121 \text{ kip/ft}) \times (6.25 \text{ ft})^2)}{(6 \times (5.9618 \text{ kipft/ft})) + (4 \times (-0.4121 \text{ kip/ft}) \times (6.25 \text{ ft}))}$$

$$a = 4.2831 \text{ ft}$$

V_{max} - Max shear force located at depth a ,

$$V_{max} = (H_o D) \left[1 - \left[3 \left(\frac{4 E}{L_c} + 3 \right) \left(\frac{a}{L_c} \right)^2 \right] + \left[4 \left(\frac{3 E}{L_c} + 2 \right) \left(\frac{a}{L_c} \right)^3 \right] \right]$$

$$V_{max} = ((-0.4121 \text{ kip/ft}) \times (48 \text{ in})) \times \left[1 - \left[3 \times \left(\frac{4 \times (14.467 \text{ ft})}{(6.25 \text{ ft})} + 3 \right) \times \left(\frac{(4.2831 \text{ ft})}{(6.25 \text{ ft})} \right)^2 \right] + \left[4 \times \left(\frac{3 \times (14.467 \text{ ft})}{(6.25 \text{ ft})} + 2 \right) \times \left(\frac{(4.2831 \text{ ft})}{(6.25 \text{ ft})} \right)^3 \right] \right]$$

$$V_{max} = 7.8417 \text{ kip}$$

M_{max} - Max bending moment located at depth $a/2$,

$$M_{max} = (H_o D L_c) \left[\left(\frac{E}{L_c} + \frac{a}{2 L_c} \right) - \left[\left(\frac{4 E}{L_c} + 3 \right) \left(\frac{a}{2 L_c} \right)^3 \right] + \left[\left(\frac{3 E}{L_c} + 2 \right) \left(\frac{a}{2 L_c} \right)^4 \right] \right]$$

$$M_{max} = ((-0.4121 \text{ kip/ft}) \times (48 \text{ in}) \times (6.25 \text{ ft})) \times \left[\left(\frac{(14.467 \text{ ft})}{(6.25 \text{ ft})} + \frac{(4.2831 \text{ ft})}{2 \times (6.25 \text{ ft})} \right) - \left[\left(\frac{4 \times (14.467 \text{ ft})}{(6.25 \text{ ft})} + 3 \right) \times \left(\frac{(4.2831 \text{ ft})}{2 \times (6.25 \text{ ft})} \right)^3 \right] + \left[\left(\frac{3 \times (14.467 \text{ ft})}{(6.25 \text{ ft})} + 2 \right) \times \left(\frac{(4.2831 \text{ ft})}{2 \times (6.25 \text{ ft})} \right)^4 \right] \right]$$

$$M_{max} = 23.567 \text{ kipft}$$

Minimum Reinforcement Check (LRFD)

Parameters:

$f'_{ck} = 3 \text{ ksi}$ - Concrete strength,
 $f_{yk} = 60 \text{ ksi}$ - Longitudinal reinforcement strength,
 $\phi = 0.65$ - Reduction factor for axial strength,
 $\alpha = 0.8$ - Alpha factor for axial strength,
 $A_g = 2304 \text{ in}^2$ - Gross area of concrete,

Table 22.4.2.1

Longitudinal reinforcement:

Required reinforcement due to axial load, $A_{st,required}$

22.4.2.2, 10.6.1.1

$A_{st,required}$

$$A_{st,required} = \text{Min} \left[\frac{\frac{P}{\phi \alpha} - (0.85 f'_{ck} A_g)}{f_{yk} - (0.85 f'_{ck})}, (0.08 A_g) \right]$$

$$A_{st,required} = \text{Min} \left[\frac{\frac{(8.994 \text{ kip})}{(0.65) \times (0.8)} - (0.85 \times (3 \text{ ksi}) \times (2304 \text{ in}^2))}{(60 \text{ ksi}) - (0.85 \times (3 \text{ ksi}))}, (0.08 \times (2304 \text{ in}^2)) \right]$$

$$A_{st,required} = -101.97 \text{ in}^2$$

A_{min} - Governing minimum reinforcement area,

$$A_{min} = \text{Max} [A_{st,required}, (0.0018 A_g)]$$

$$A_{min} = \text{Max} [(-101.97 \text{ in}^2), (0.0018 \times (2304 \text{ in}^2))]$$

$$A_{min} = 4.1472 \text{ in}^2$$

n_{rebar} - Required number of reinforcement,

$$n_{rebar} = \frac{A_{min}}{A_{rebar}}$$

$$n_{rebar} = \frac{(4.1472 \text{ in}^2)}{(0.3068 \text{ in}^2)}$$

$$n_{rebar} = 14$$

A_{st} - Actual total reinforcement area,

$$A_{st} = n_{rebar} \frac{\pi d_{bar}^2}{4}$$

$$A_{st} = (14) \times \frac{\pi \times (0.625 \text{ in})^2}{4}$$

$$A_{st} = 4.2951 \text{ in}^2$$

Ratio - Capacity

$$\text{Ratio} = \frac{A_{min}}{A_{st}}$$

$$\text{Ratio} = \frac{(4.1472 \text{ in}^2)}{(4.2951 \text{ in}^2)}$$

$$\text{Ratio} = 0.96556$$

Status: **PASS**
Ratio: **0.970**

25.2.3

s_{rebar} - Minimum spacing of reinforcement,

$$s_{rebar} = \text{Max} [1.5, (1.5 d_{bar})]$$

$$s_{rebar} = \text{Max} [1.5, (1.5 \times (0.625 \text{ in}))]$$

$$s_{rebar} = 1.5 \text{ in}$$

Ties:

25.7.2.2 Since longitudinal reinforcement is \leq No. 10 \emptyset : Use #3(0.375 in)

25.7.2.1

s_{ties} - Maximum spacing of ties,

$$s_{ties} = \text{Min} [(16 d_{bar}), (48 d_{ties}), \text{Min} (D, b)]$$

$$s_{ties} = \text{Min} [(16 \times (0.625 \text{ in})), (48 \times (0.375 \text{ in})), \text{Min} ((48 \text{ in}), (48 \text{ in}))]$$

$$s_{ties} = 10 \text{ in}$$

Summary:

Main reinforcement: **14 - #5 (0.625 in)**

Axial Compression Strength (ACI 318-19, LRFD)22.4.2.2 ϕP_N - Allowable axial compressive strength

$$\phi P_N = \phi 0.80 [(0.85 f'_{ck} [A_g - A_{st}] + (f_{yk} A_{st})]$$

$$\phi P_N = (0.65) \times 0.80 \times [(0.85 \times (3 \text{ ksi}) \times [(2304 \text{ in}^2) - (4.2951 \text{ in}^2)]) + ((60 \text{ ksi}) \times (4.2951 \text{ in}^2))]$$

$$\phi P_N = 3183.4 \text{ kip}$$

Ratio - Capacity

$$\text{Ratio} = \frac{P}{\phi P_N}$$

$$\text{Ratio} = \frac{(8.994 \text{ kip})}{(3183.4 \text{ kip})}$$

$$\text{Ratio} = 0.0028253$$

Status: **PASS**
Ratio: **0.000****Shear Strength (ACI 318-19, LRFD)****Parameters:** $b_w = 48 \text{ in}$ - Effective width,22.5.2.2 d - Effective depth

$$d = 0.80 D$$

$$d = 0.80 \times (48 \text{ in})$$

$$d = 38.4 \text{ in}$$

22.5.5.1.3 λ_s - size effect modification factor

$$\lambda_s = \text{MIN} \left[\sqrt{\frac{2}{1 + \frac{d}{10}}}, 1 \right]$$

$$\lambda_s = \text{MIN} \left[\sqrt{\frac{2}{1 + \frac{(38.4 \text{ in})}{10}}}, 1 \right]$$

$$\lambda_s = 0.64282$$

The following variables were converted to be consistent with empirical formula $f'_{ck} = 3 \text{ ksi} \rightarrow 3000 \text{ psi}$,22.5.5.1.1 $V_{c,max}$ - Max shear strength of concrete

$$V_{c,max} = 5 \lambda_s \sqrt{f'_{ck}} b_w d$$

$$V_{c,max} = 5 \times (0.64282) \times \sqrt{(3000 \text{ psi})} \times (48 \text{ in}) \times (38.4 \text{ in})$$

$$V_{c,max} = 324.49 \text{ kip}$$

The following variables were converted to be consistent with empirical formula $f'_{ck} = 3 \text{ ksi} \rightarrow 3000 \text{ psi}$, $P = 8.994 \text{ kip} \rightarrow 8994 \text{ lbf}$,22.5.5.1.1(a) $V_{c,a}$ - Shear strength of concrete (a)

$$V_{c,a} = \left[2 \lambda_s \sqrt{f'_{ck}} + \frac{P}{6 A_g} \right] b_w d$$

$$V_{c,a} = \left[2 \times (0.64282) \times \sqrt{(3000 \text{ psi})} + \frac{(8994 \text{ lbf})}{6 \times (2304 \text{ in}^2)} \right] \times (48 \text{ in}) \times (38.4 \text{ in})$$

$$V_{c,a} = 130.99 \text{ kip}$$

The following variables were converted to be consistent with empirical formula $f'_{ck} = 3 \text{ ksi} \rightarrow 3000 \text{ psi}$,22.5.5.1.2 $V_{c,b}$ - Shear strength of concrete (b)

$$V_{c,b} = \left[2 \lambda_s \sqrt{f'_{ck}} + (0.05 f'_{ck}) \right] b_w d$$

$$V_{c,b} = \left[2 \times (0.64282) \times \sqrt{(3000 \text{ psi})} + (0.05 \times (3000 \text{ psi})) \right] \times (48 \text{ in}) \times (38.4 \text{ in})$$

$$V_{c,b} = 406.27 \text{ kip}$$

 V_c - Governing shear strength of concrete

$$V_c = \text{Min}[V_{c,max}, V_{c,a}, V_{c,b}]$$

$$V_c = \text{Min}[(324.49 \text{ kip}), (130.99 \text{ kip}), (406.27 \text{ kip})]$$

$$V_c = 130.99 \text{ kip}$$

| | | |
|------------------|---|---|
| <p>22.5.1.2</p> | <p>The following variables were converted to be consistent with empirical formula $f'_{ck} = 3 \text{ ksi} \rightarrow 3000 \text{ psi}$.</p> <p>$V_{s,a}$ - Shear strength of steel (a)</p> $V_{s,a} = 8 \sqrt{f'_{ck}} b_w d$ $V_{s,a} = 8 \times \sqrt{(3000 \text{ psi})} \times (48 \text{ in}) \times (38.4 \text{ in})$ $V_{s,a} = 807.65 \text{ kip}$ <p>A_v - Ties rebar area,</p> $A_v = \frac{\pi d_{ties}^2}{4}$ $A_v = \frac{\pi \times (0.375 \text{ in})^2}{4}$ $A_v = 0.11045 \text{ in}^2$ <p>22.5.8.5.3 $V_{s,b}$ - Shear strength of steel (b)</p> $V_{s,b} = \frac{2 A_v f_{ywk} d}{s_{ties}}$ $V_{s,b} = \frac{2 \times (0.11045 \text{ in}^2) \times (60 \text{ ksi}) \times (38.4 \text{ in})}{(10 \text{ in})}$ $V_{s,b} = 50.894 \text{ kip}$ <p>V_s - Governing shear strength of steel</p> $V_s = \text{MIN}[V_{s,a}, V_{s,b}]$ $V_s = \text{MIN}[(807.65 \text{ kip}), (50.894 \text{ kip})]$ $V_s = 50.894 \text{ kip}$ <p>22.5.1.1 ϕV_n - Allowable shear strength</p> $\phi V_n = \phi (V_c + V_s)$ $\phi V_n = (0.65) \times ((130.99 \text{ kip}) + (50.894 \text{ kip}))$ $\phi V_n = 118.23 \text{ kip}$ <p>Considering x-direction:</p> <p>$V_{max} = 7.8417 \text{ kip}$ - Maximum shear force in the x-direction, Ratio - Capacity</p> $\text{Ratio} = \frac{V_{max}}{\phi V_n}$ $\text{Ratio} = \frac{(7.8417 \text{ kip})}{(118.23 \text{ kip})}$ $\text{Ratio} = 0.066328$ | <p>Status: PASS Ratio: 0.070</p> |
| <p>14.5.2.1b</p> | <p>Flexural Strength (ACI 318-19, LRFD)</p> <p>S_m - Section modulus</p> $S_m = \frac{b D^2}{6}$ $S_m = \frac{(48 \text{ in}) \times (48 \text{ in})^2}{6}$ $S_m = 18432 \text{ in}^3$ <p>$\lambda = 1$ - Concrete modification factor (Normal concrete), Allowable flexural strength: M_n shall be the lesser of:</p> <p>$\phi M_{n,1}$</p> $\phi M_{n,1} = \phi \times 5 \times \lambda \times \sqrt{f'_c} \times S_m$ $\phi M_{n,1} = 0.65 \times 5 \times 1 \times \sqrt{(3 \text{ ksi})} \times 18432.001 \text{ in}^3$ $\phi M_{n,1} = 273.423 \text{ kip ft}$ <p>$\phi M_{n,2}$</p> $\phi M_{n,2} = \phi \times 0.85 \times f'_c \times S_m$ | |

$$\phi M_{n,z} = \phi S_x F_y$$

$$\phi M_{n,z} = (0.65) \times 0.85 \times (3 \text{ ksi}) \times (18432 \text{ in}^3)$$

$$\phi M_{n,z} = 2545.9 \text{ kipft}$$

Therefore,

ϕM_n - Allowable flexural strength,

$$\phi M_n = \text{MIN}[\phi M_{n,1}, \phi M_{n,2}]$$

$$\phi M_n = \text{MIN}[(273.42 \text{ kipft}), (2545.9 \text{ kipft})]$$

$$\phi M_n = 273.42 \text{ kipft}$$

Considering x-direction:

$M_{max} = 23.567 \text{ kipft}$ - Maximum moment in the x-direction,

Ratio - Capacity

$$\text{Ratio} = \frac{M_{max}}{\phi M_n}$$

$$\text{Ratio} = \frac{(23.567 \text{ kipft})}{(273.42 \text{ kipft})}$$

$$\text{Ratio} = 0.086191$$

Status: **PASS**
Ratio: **0.090**