

Your Project Calculations



Project Name: MTSOLAR_32GD72009EB65

S3D Model Link:

https://platform.skyciv.com/structural?preload_name=MTSOLAR_32GD72009EB65&preload_path=Shared%20Enterprise%20Folder/MT_Solar_Projects/9_2023

Public Model Link:

https://platform.skyciv.com/structural-viewer?project_id=ltH5DbpRCIsathYPEeX0BVfFLKW3LZoHB8A3umpZxOvU10Uv11yWzPujwMGf4v4i

Array Specification

Product:	Beam
Unique ID:	4P-19.75-10TOP-HD-72-L-3Hx12W-GDB3
Duty Classification:	HD
Module Width:	39.50 in
Module Length:	79.10in
Number of Rows:	3
Number of Columns:	12
Total Number of Modules:	36
Desired Tilt Angle:	30
Front Edge Clearance:	23
Total Array Height at Tilt:	27.97 ft
Total Frame Length:	78.75 ft
Frame Weight:	6567 lbs
Array Dimensions N/S:	10.00 ft
Array Dimensions E/W:	80.10 ft
Rail Length:	120.00 in
Rail Spacing:	3.30 ft
Rail Check:	Not Checked

Support Specifications

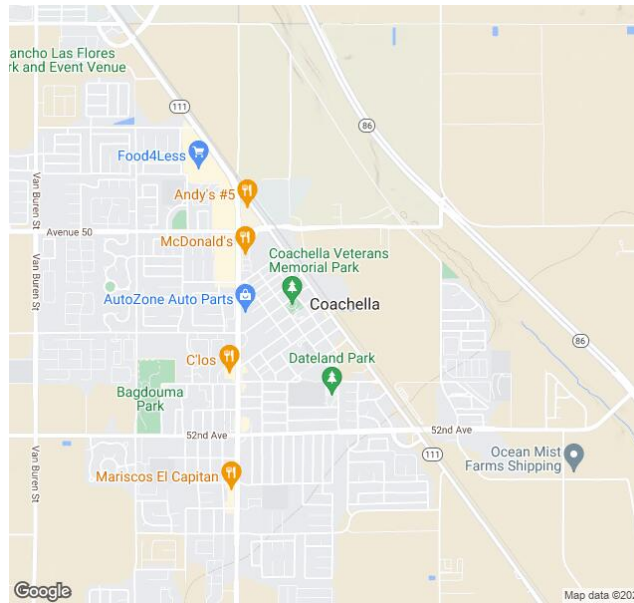
Pole Size:	10in Pipe Sch 40
Pole Length above Grade:	25.50 ft
Number of Poles:	4
Pole Spacing:	19.75 ft

Foundation Specifications

Foundation Type:	Square
Foundation Dimensions:	48 x 48 in
Foundation Depth (below grade):	Pile 1: 9.25 ft Pile 2: 9.00 ft Pile 3: 9.00 ft Pile 4: 9.25 ft
Foundation Volume:	21.630 y ³
Foundation Result:	PASSED
Mount Twist:	0.778884 kip

Site Info

Risk Category:	I
Exposure:	C
Soil Classification:	sand
Site Location:	PW2R+JH Coachella, CA, USA
Wind Speed:	110 mph
Snow Load:	0 psf
Design Uplift Pressure:	Multiple pressures
Design Downforce Pressure:	Multiple pressures
Design Snow Pressure:	0.000000 ksf



Design Disclaimer

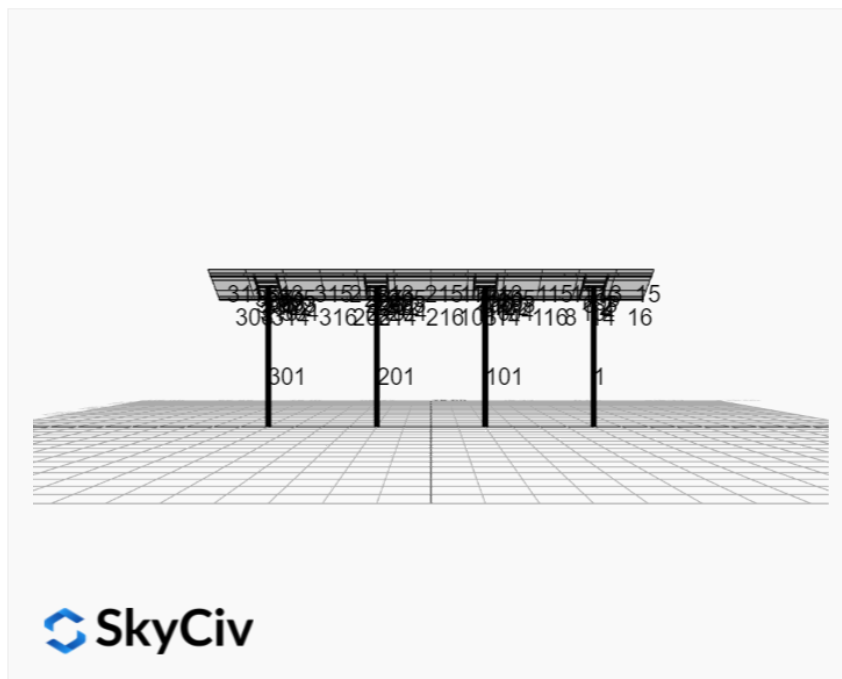
This software should be used for preliminary designs and should not be used as a final design unless reviewed, verified and designed by a qualified structural engineer.

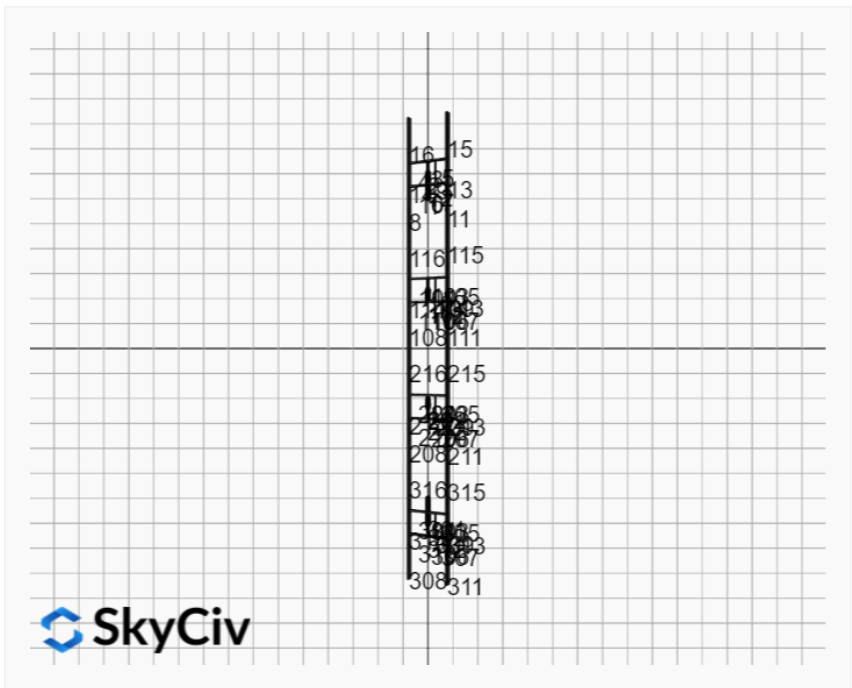
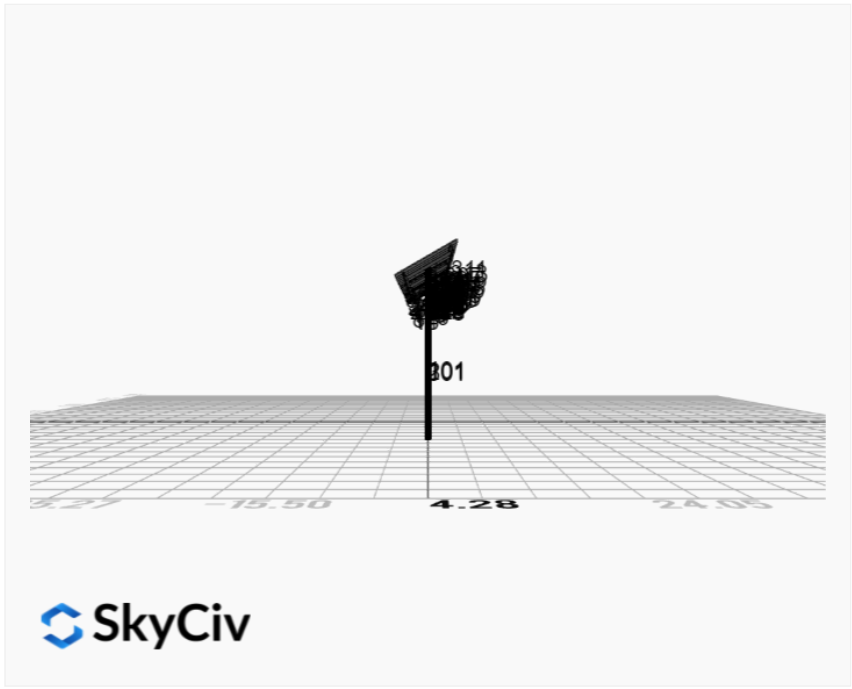
AutoDesigner Input

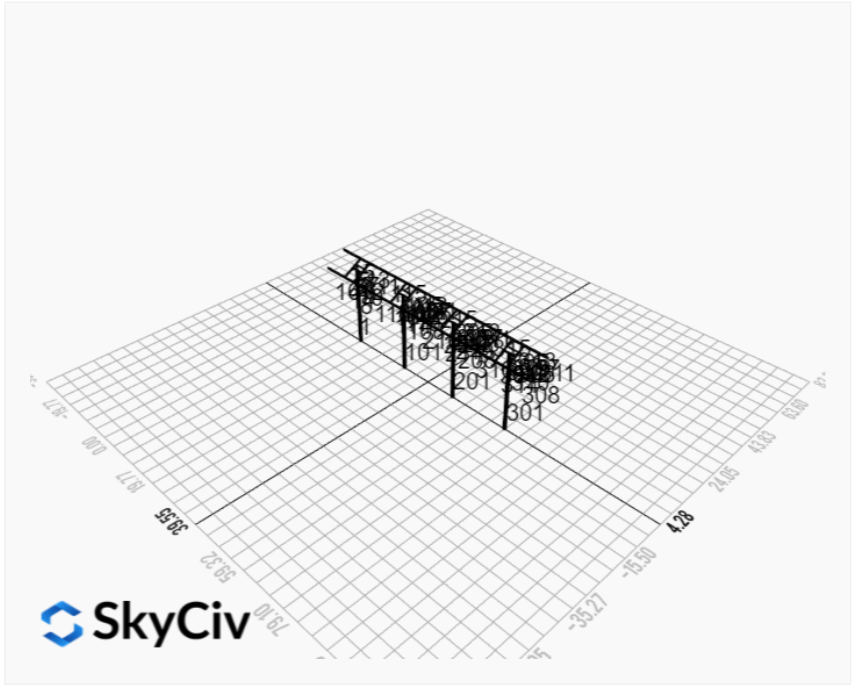
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Design Notes:

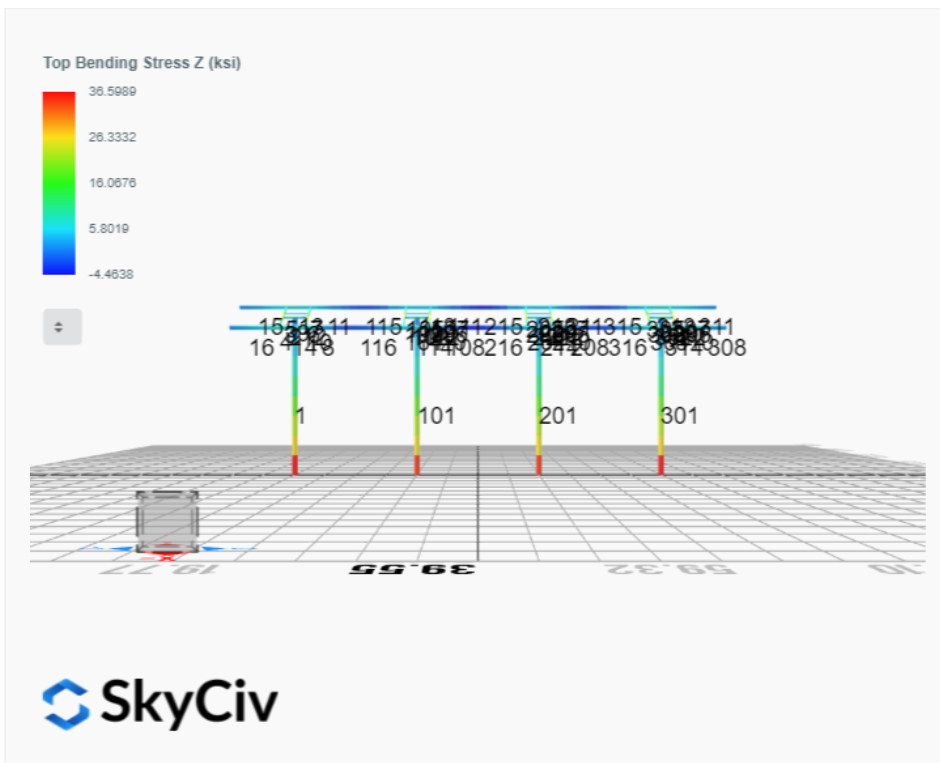
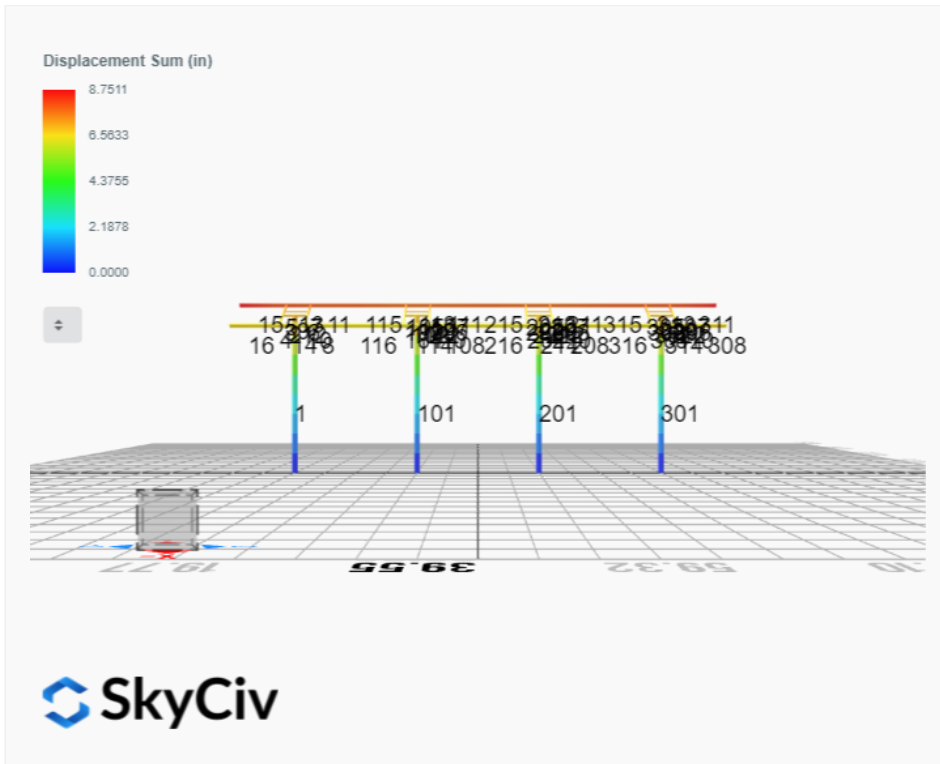
- AISC Deflection checks are set to L/1 due to structure design intent
- Foundation Soil Parameters used in this Autodesgin are all estimates, proper geotechnical reports are required to confirm soil profiles
- Foundation Design and Sizing is approximate only

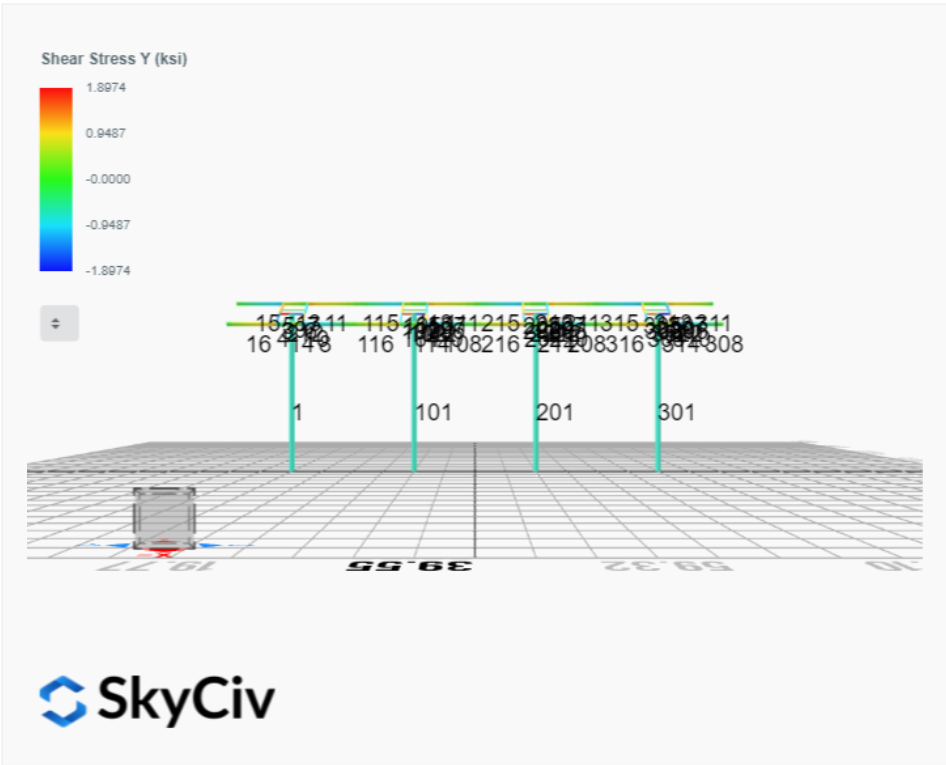
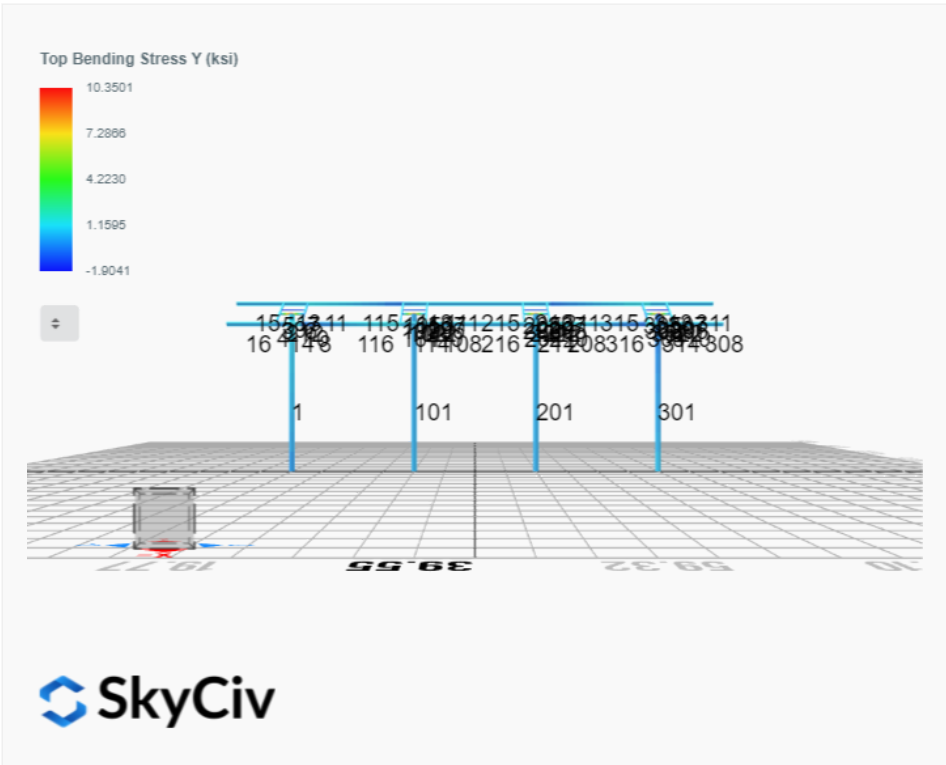


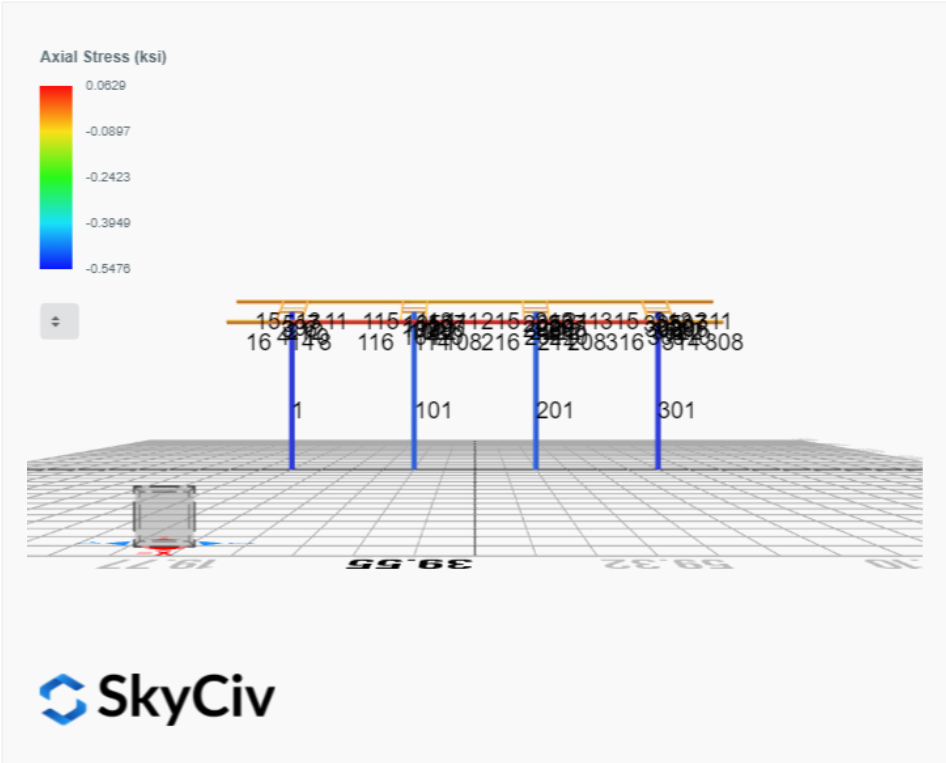




FEM Results (Envelope Worst Case for each member)







Reaction Forces for Foundation 1 (Node ID#1), (kip, kip-ft)

ASD Load Combination Results

Name	Fx	Fy	Fz	Mx	My	Mz
ULS: 1. D	-0.0088	2.6439	-0.0205	-0.1695	0.0761	0.2391
ULS: 2. D + L	-0.0088	2.6439	-0.0205	-0.1695	0.0761	0.2391
ULS: 3. D + (S or Lr or R)	-0.0088	2.6439	-0.0205	-0.1695	0.0761	0.2391
ULS: 3. D + (S or Lr or R)	-0.0088	2.6439	-0.0205	-0.1695	0.0761	0.2391
ULS: 4. D + 0.75L + 0.75(S or Lr or R)	-0.0088	2.6439	-0.0205	-0.1695	0.0761	0.2391
ULS: 4. D + 0.75L + 0.75(S or Lr or R)	-0.0088	2.6439	-0.0205	-0.1695	0.0761	0.2391
ULS: 5b. D + 0.7E	-0.0088	2.6439	-0.0205	-0.1695	0.0761	0.2391
ULS: 6b. D + 0.75L + 0.75(0.7)E + 0.75S	-0.0088	2.6439	-0.0205	-0.1695	0.0761	0.2391
ULS: 8. 0.6D + 0.7E	-0.0053	1.5864	-0.0123	-0.1017	0.0457	0.1435
ULS: 5a. D + 0.6W_Wind downforce Case A only	-2.6178	7.2062	-0.1039	-0.8573	0.4863	70.3152
ULS: 5a. D + 0.6W_Wind downforce Case B only	-2.6178	7.2062	-0.1039	-0.8573	0.4863	70.3152
ULS: 5a. D + 0.6W_Wind uplift Case A only	2.2317	-1.2684	0.0489	0.3985	-0.2647	-54.4836
ULS: 5a. D + 0.6W_Wind uplift Case B only	1.8526	-0.6134	0.0400	0.3260	-0.2239	-54.4433
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind downforce Case A only	-1.9655	6.0656	-0.0831	-0.6853	0.3837	52.7962
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind downforce Case B only	-1.9655	6.0656	-0.0831	-0.6853	0.3837	52.7962
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind uplift Case A only	1.6715	-0.2903	0.0315	0.2565	-0.1795	-40.8029
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind uplift Case B only	1.3872	0.2010	0.0249	0.2021	-0.1489	-40.7727
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind downforce Case A only	-1.9655	6.0656	-0.0831	-0.6853	0.3837	52.7962
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind downforce Case B only	-1.9655	6.0656	-0.0831	-0.6853	0.3837	52.7962
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind uplift Case A only	1.6715	-0.2903	0.0315	0.2565	-0.1795	-40.8029
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind uplift Case B only	1.3872	0.2010	0.0249	0.2021	-0.1489	-40.7727
ULS: 7. 0.6D + 0.6W_Wind downforce Case A only	-2.6142	6.1486	-0.0957	-0.7895	0.4558	70.2196
ULS: 7. 0.6D + 0.6W_Wind downforce Case B only	-2.6142	6.1486	-0.0957	-0.7895	0.4558	70.2196
ULS: 7. 0.6D + 0.6W_Wind uplift Case A only	2.2352	-2.3260	0.0571	0.4664	-0.2952	-54.5793
ULS: 7. 0.6D + 0.6W_Wind uplift Case B only	1.8561	-1.6709	0.0482	0.3938	-0.2543	-54.5389

Worst Case Reactions LRFD

These calculations are taken directly from the FEA via SkyCiv and are used in the Concrete Checks of the Foundation Module.
Note: Worst case values are assumed as downforce wind load cases.

Result	Value (kip, kip-ft)
Axial	10.7759
Shear X	-4.3572
Shear Z	-0.1643
Moment X	-1.3581
Moment Y (Twist)	0.7786
Moment Z	119.8196

Worst Case Reactions ASD

These results are taken from the worst case values in the above table and are used in the Soil Checks in the Foundation Module.
Note: Worst case values are assumed as downforce wind load cases.

Result	Value (kip, kip-ft)
Axial	7.2062
Shear X	-2.6178
Shear Z	-0.1039
Moment X	-0.8573
Moment Y (Twist)	0.4863
Moment Z	70.3152

Reaction Forces for Foundation 2 (Node ID#101), (kip, kip-ft)

ASD Load Combination Results

Name	Fx	Fy	Fz	Mx	My	Mz
ULS: 1. D	0.0088	2.6014	0.0016	0.0136	-0.0038	-0.1863
ULS: 2. D + L	0.0088	2.6014	0.0016	0.0136	-0.0038	-0.1863
ULS: 3. D + (S or Lr or R)	0.0088	2.6014	0.0016	0.0136	-0.0038	-0.1863
ULS: 3. D + (S or Lr or R)	0.0088	2.6014	0.0016	0.0136	-0.0038	-0.1863
ULS: 4. D + 0.75L + 0.75(S or Lr or R)	0.0088	2.6014	0.0016	0.0136	-0.0038	-0.1863
ULS: 4. D + 0.75L + 0.75(S or Lr or R)	0.0088	2.6014	0.0016	0.0136	-0.0038	-0.1863
ULS: 5b. D + 0.7E	0.0088	2.6014	0.0016	0.0136	-0.0038	-0.1863

Name	Fx	Fy	Fz	Mx	My	Mz
ULS: 6b. D + 0.75L + 0.75(0.7)E + 0.75S	0.0088	2.6014	0.0016	0.0136	-0.0038	-0.1863
ULS: 8. 0.6D + 0.7E	0.0053	1.5608	0.0010	0.0081	-0.0023	-0.1118
ULS: 5a. D + 0.6W_Wind downforce Case A only	-2.5369	6.9673	0.0091	0.0767	-0.0166	68.1492
ULS: 5a. D + 0.6W_Wind downforce Case B only	-2.5369	6.9673	0.0091	0.0767	-0.0166	68.1492
ULS: 5a. D + 0.6W_Wind uplift Case A only	2.1866	-1.1390	-0.0060	-0.0496	0.0153	-53.5523
ULS: 5a. D + 0.6W_Wind uplift Case B only	1.8294	-0.5186	-0.0034	-0.0283	0.0026	-53.6564
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind downforce Case A only	-1.9005	5.8758	0.0072	0.0609	-0.0134	51.0653
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind downforce Case B only	-1.9005	5.8758	0.0072	0.0609	-0.0134	51.0653
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind uplift Case A only	1.6422	-0.2039	-0.0041	-0.0338	0.0106	-40.2108
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind uplift Case B only	1.3742	0.2614	-0.0022	-0.0178	0.0010	-40.2889
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind downforce Case A only	-1.9005	5.8758	0.0072	0.0609	-0.0134	51.0653
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind downforce Case B only	-1.9005	5.8758	0.0072	0.0609	-0.0134	51.0653
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind uplift Case A only	1.6422	-0.2039	-0.0041	-0.0338	0.0106	-40.2108
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind uplift Case B only	1.3742	0.2614	-0.0022	-0.0178	0.0010	-40.2889
ULS: 7. 0.6D + 0.6W_Wind downforce Case A only	-2.5404	5.9267	0.0085	0.0713	-0.0151	68.2237
ULS: 7. 0.6D + 0.6W_Wind downforce Case B only	-2.5404	5.9267	0.0085	0.0713	-0.0151	68.2237
ULS: 7. 0.6D + 0.6W_Wind uplift Case A only	2.1831	-2.1796	-0.0066	-0.0551	0.0168	-53.4778
ULS: 7. 0.6D + 0.6W_Wind uplift Case B only	1.8258	-1.5591	-0.0040	-0.0337	0.0041	-53.5819

Worst Case Reactions LRFD

These calculations are taken directly from the FEA via SkyCiv and are used in the Concrete Checks of the Foundation Module.
Note: Worst case values are assumed as downforce wind load cases.

Result	Value (kip, kip-ft)
Axial	10.3988
Shear X	-4.2429
Shear Z	0.0140
Moment X	0.1181
Moment Y (Twist)	0.0318
Moment Z	116.3527

Worst Case Reactions ASD

These results are taken from the worst case values in the above table and are used in the Soil Checks in the Foundation Module.
Note: Worst case values are assumed as downforce wind load cases.

Result	Value (kip, kip-ft)
Axial	6.9673
Shear X	-2.5404
Shear Z	0.0091
Moment X	0.0767
Moment Y (Twist)	0.0168
Moment Z	68.2237

Reaction Forces for Foundation 3 (Node ID#201), (kip, kip-ft)

ASD Load Combination Results

Name	Fx	Fy	Fz	Mx	My	Mz
ULS: 1. D	0.0088	2.6014	-0.0016	-0.0136	0.0038	-0.1863
ULS: 2. D + L	0.0088	2.6014	-0.0016	-0.0136	0.0038	-0.1863
ULS: 3. D + (S or Lr or R)	0.0088	2.6014	-0.0016	-0.0136	0.0038	-0.1863
ULS: 3. D + (S or Lr or R)	0.0088	2.6014	-0.0016	-0.0136	0.0038	-0.1863
ULS: 4. D + 0.75L + 0.75(S or Lr or R)	0.0088	2.6014	-0.0016	-0.0136	0.0038	-0.1863
ULS: 4. D + 0.75L + 0.75(S or Lr or R)	0.0088	2.6014	-0.0016	-0.0136	0.0038	-0.1863
ULS: 5b. D + 0.7E	0.0088	2.6014	-0.0016	-0.0136	0.0038	-0.1863
ULS: 6b. D + 0.75L + 0.75(0.7)E + 0.75S	0.0088	2.6014	-0.0016	-0.0136	0.0038	-0.1863
ULS: 8. 0.6D + 0.7E	0.0053	1.5608	-0.0010	-0.0081	0.0023	-0.1118
ULS: 5a. D + 0.6W_Wind downforce Case A only	-2.5369	6.9673	-0.0091	-0.0767	0.0166	68.1492
ULS: 5a. D + 0.6W_Wind downforce Case B only	-2.5369	6.9673	-0.0091	-0.0767	0.0166	68.1492
ULS: 5a. D + 0.6W_Wind uplift Case A only	2.1866	-1.1390	0.0060	0.0496	-0.0153	-53.5523
ULS: 5a. D + 0.6W_Wind uplift Case B only	1.8294	-0.5186	0.0034	0.0283	-0.0026	-53.6564
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind downforce Case A only	-1.9005	5.8758	-0.0072	-0.0609	0.0134	51.0653
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind downforce Case B only	-1.9005	5.8758	-0.0072	-0.0609	0.0134	51.0653
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind uplift Case A only	1.6422	-0.2039	0.0041	0.0338	-0.0105	-40.2108
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind uplift Case B only	1.3742	0.2614	0.0022	0.0178	-0.0010	-40.2889

Name	Fx	Fy	Fz	Mx	My	Mz
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind downforce Case A only	-1.9005	5.8758	-0.0072	-0.0609	0.0134	51.0653
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind downforce Case B only	-1.9005	5.8758	-0.0072	-0.0609	0.0134	51.0653
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind uplift Case A only	1.6422	-0.2039	0.0041	0.0338	-0.0105	-40.2108
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind uplift Case B only	1.3742	0.2614	0.0022	0.0178	-0.0010	-40.2889
ULS: 7. 0.6D + 0.6W_Wind downforce Case A only	-2.5404	5.9267	-0.0085	-0.0713	0.0151	68.2237
ULS: 7. 0.6D + 0.6W_Wind downforce Case B only	-2.5404	5.9267	-0.0085	-0.0713	0.0151	68.2237
ULS: 7. 0.6D + 0.6W_Wind uplift Case A only	2.1831	-2.1796	0.0066	0.0551	-0.0168	-53.4778
ULS: 7. 0.6D + 0.6W_Wind uplift Case B only	1.8258	-1.5591	0.0040	0.0337	-0.0041	-53.5819

Worst Case Reactions LRFD

These calculations are taken directly from the FEA via SkyCiv and are used in the Concrete Checks of the Foundation Module.
Note: Worst case values are assumed as downforce wind load cases.

Result	Value (kip, kip-ft)
Axial	10.3988
Shear X	-4.2429
Shear Z	-0.0140
Moment X	-0.1182
Moment Y (Twist)	0.0318
Moment Z	116.3531

Worst Case Reactions ASD

These results are taken from the worst case values in the above table and are used in the Soil Checks in the Foundation Module.
Note: Worst case values are assumed as downforce wind load cases.

Result	Value (kip, kip-ft)
Axial	6.9673
Shear X	-2.5404
Shear Z	-0.0091
Moment X	-0.0767
Moment Y (Twist)	0.0168
Moment Z	68.2237

Reaction Forces for Foundation 4 (Node ID#301), (kip, kip-ft)

ASD Load Combination Results

Name	Fx	Fy	Fz	Mx	My	Mz
ULS: 1. D	-0.0088	2.6439	0.0205	0.1695	-0.0761	0.2391
ULS: 2. D + L	-0.0088	2.6439	0.0205	0.1695	-0.0761	0.2391
ULS: 3. D + (S or Lr or R)	-0.0088	2.6439	0.0205	0.1695	-0.0761	0.2391
ULS: 3. D + (S or Lr or R)	-0.0088	2.6439	0.0205	0.1695	-0.0761	0.2391
ULS: 4. D + 0.75L + 0.75(S or Lr or R)	-0.0088	2.6439	0.0205	0.1695	-0.0761	0.2391
ULS: 4. D + 0.75L + 0.75(S or Lr or R)	-0.0088	2.6439	0.0205	0.1695	-0.0761	0.2391
ULS: 5b. D + 0.7E	-0.0088	2.6439	0.0205	0.1695	-0.0761	0.2391
ULS: 6b. D + 0.75L + 0.75(0.7)E + 0.75S	-0.0088	2.6439	0.0205	0.1695	-0.0761	0.2391
ULS: 8. 0.6D + 0.7E	-0.0053	1.5864	0.0123	0.1017	-0.0457	0.1435
ULS: 5a. D + 0.6W_Wind downforce Case A only	-2.6178	7.2062	0.1039	0.8573	-0.4863	70.3152
ULS: 5a. D + 0.6W_Wind downforce Case B only	-2.6178	7.2062	0.1039	0.8573	-0.4863	70.3152
ULS: 5a. D + 0.6W_Wind uplift Case A only	2.2317	-1.2684	-0.0489	-0.3985	0.2647	-54.4836
ULS: 5a. D + 0.6W_Wind uplift Case B only	1.8526	-0.6134	-0.0400	-0.3260	0.2239	-54.4433
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind downforce Case A only	-1.9655	6.0656	0.0831	0.6853	-0.3837	52.7962
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind downforce Case B only	-1.9655	6.0656	0.0831	0.6853	-0.3837	52.7962
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind uplift Case A only	1.6715	-0.2903	-0.0315	-0.2565	0.1795	-40.8029
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind uplift Case B only	1.3872	0.2010	-0.0249	-0.2021	0.1489	-40.7727
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind downforce Case A only	-1.9655	6.0656	0.0831	0.6853	-0.3837	52.7962
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind downforce Case B only	-1.9655	6.0656	0.0831	0.6853	-0.3837	52.7962
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind uplift Case A only	1.6715	-0.2903	-0.0315	-0.2565	0.1795	-40.8029
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind uplift Case B only	1.3872	0.2010	-0.0249	-0.2021	0.1489	-40.7727
ULS: 7. 0.6D + 0.6W_Wind downforce Case A only	-2.6142	6.1486	0.0957	0.7895	-0.4558	70.2196
ULS: 7. 0.6D + 0.6W_Wind downforce Case B only	-2.6142	6.1486	0.0957	0.7895	-0.4558	70.2196
ULS: 7. 0.6D + 0.6W_Wind uplift Case A only	2.2352	-2.3260	-0.0571	-0.4663	0.2952	-54.5793
ULS: 7. 0.6D + 0.6W_Wind uplift Case B only	1.8561	-1.6709	-0.0482	-0.3938	0.2543	-54.5389

Worst Case Reactions LRFD

Worst Case Reactions ASD

These calculations are taken directly from the FEA via SkyCiv and are used in the Concrete Checks of the Foundation Module. Note: Worst case values are assumed as downforce wind load cases.

Result	Value (kip, kip-ft)
Axial	10.7759
Shear X	-4.3572
Shear Z	0.1643
Moment X	1.3579
Moment Y (Twist)	0.7789
Moment Z	119.8202

These results are taken from the worst case values in the above table and are used in the Soil Checks in the Foundation Module. Note: Worst case values are assumed as downforce wind load cases.

Result	Value (kip, kip-ft)
Axial	7.2062
Shear X	-2.6178
Shear Z	0.1039
Moment X	0.8573
Moment Y (Twist)	0.4863
Moment Z	70.3152

Project Details

Design Code: AISC 360-16 LRFD
 Provision: LRFD
 Country: United States

User Name: sales@mtsolar.us
 Project Name: MTSOLAR_32GD72009EB65
 Unit System: imperial



Design Input Information

Design Factors			
Φ_t	Φ_c	Φ_b	Φ_v
0.9	0.9	0.9	0.9

Design Materials			
ID	E (ksi)	F _y (ksi)	F _u (ksi)
1	29000	50	65

Section Dimensions			

ID	Name	d (in)	t _w (in)				
2	2in Pipe Sch 80	2.38	0.22				
5	4in Pipe Sch 80	4.50	0.34				
11	10in Pipe Sch 40	10.75	0.36				

Section Dimensions			

ID	Name	d (in)	b (in)	t _w (in)	t _b (in)	r (in)	
16	HSS5x3x3/16	5.00	3.00	0.17	0.17	0.17	

Section Dimensions			

ID	Name	d (in)	t _w (in)	b _t (in)	b _b (in)	t _t (in)	t _b (in)	r (in)
19	W8x10	7.89	0.17	3.94	3.94	0.20	0.20	0.30

Section Properties								
ID	Name	A (in ²)	J (in ⁴)	I _{yp} (in ⁴)	I _{zp} (in ⁴)	I _w (in ⁶)	S _{yp} (in ³)	S _{zp} (in ³)
2	2in Pipe Sch 80	1.48	1.74	0.87	0.87	0.00	1.02	1.02
5	4in Pipe Sch 80	4.41	19.22	9.61	9.61	0.00	5.85	5.85

11	10in Pipe Sch 40	11.91	321.47	160.73	160.73	0.00	39.38	39.38
16	HSS5x3x3/16	2.58	8.64	3.85	8.53	0.73	2.96	4.21
19	W8x10	2.96	0.04	2.09	30.80	30.90	1.66	8.87

Member Properties								
Member ID	Section ID	K _z L (ft)	K _y L (ft)	L _b (ft)	C _b	L S T	L S C	L D
1	11	53.55	53.55	25.50	-	300	200	1
2	5	1.30	1.30	2.00	-	300	200	1
3	16	0.92	0.92	1.42	1.19,1.19,1.19,1.19,1.19,1.19,1.18,1.18,1.18,1.18,1.18,1.18,1.18,1.18,1.17,1.18,1.18,1.18,1.17,1.18,1.18	300	200	1
4	16	2.44	2.44	3.75	1.69,1.69,1.69,1.69,1.69,1.69,1.67,1.67,1.66,1.63,1.67,1.67,1.66,1.63,1.67,1.67,1.66,1.63,1.67,1.67,1.65,1.76,1.67,1.67,1.65,1.76,1.67,1.67,1.66,1.65	300	200	1
5	16	1.52	1.52	2.33	1.68,1.68,1.68,1.68,1.68,1.68,1.67,1.67,1.66,1.66,1.67,1.67,1.66,1.66,1.67,1.67,1.66,1.66,1.67,1.67,1.66,1.66,1.67,1.67,1.66,1.66	300	200	1
6	16	0.92	0.92	1.42	1.19,1.19,1.19,1.19,1.19,1.19,1.18,1.18,1.17,1.17,1.18,1.18,1.17,1.17,1.18,1.18,1.17,1.17,1.18,1.18,1.17,1.17,1.18,1.18,1.17,1.17	300	200	1
7	16	1.52	1.52	2.33	1.68,1.68,1.68,1.68,1.68,1.68,1.67,1.67,1.66,1.66,1.67,1.67,1.66,1.66,1.67,1.67,1.66,1.66,1.67,1.67,1.66,1.66,1.67,1.67,1.66,1.66	300	200	1
8	19	1.33	1.33	2.05	1.90,1.90,1.90,1.90,1.90,1.90,1.88,1.88,1.87,2.11,1.88,1.88,1.87,2.11,1.88,1.88,1.86,1.79,1.88,1.88,1.86,1.79,1.88,1.88,1.87,2.02	300	200	1
9	2	2.60	2.60	4.00	-	300	200	1
10	16	2.44	2.44	3.75	1.69,1.69,1.69,1.69,1.69,1.69,1.67,1.67,1.66,1.57,1.67,1.67,1.66,1.57,1.67,1.67,1.66,1.57,1.67,1.67,1.65,1.73,1.67,1.67,1.65,1.73,1.67,1.67,1.66,1.63	300	200	1
11	19	1.33	1.33	2.05	1.96,1.96,1.96,1.96,1.96,1.96,1.94,1.94,1.92,1.90,1.94,1.94,1.92,1.90,1.94,1.94,1.91,1.90,1.94,1.94,1.91,1.90,1.94,1.94,1.92,1.90	300	200	1
12	5	1.30	1.30	2.00	-	300	200	1
13	19	4.88	4.00	7.50	1.10,1.10,1.10,1.10,1.10,1.10,1.10,1.10,1.10,1.13,1.10,1.10,1.10,1.13,1.10,1.10,1.10,1.14,1.10,1.10,1.10,1.14,1.10,1.10,1.10,1.13	300	200	1
14	19	4.88	4.00	7.50	1.10,1.10,1.10,1.10,1.10,1.10,1.10,1.10,1.09,1.19,1.10,1.10,1.09,1.19,1.10,1.10,1.09,1.17,1.10,1.10,1.09,1.17,1.10,1.10,1.09,1.16	300	200	1
15	19	12.60	12.60	6.00	2.33,2.33	300	200	1
16	19	12.60	12.60	6.00	2.33,2.33	300	200	1
101	11	53.55	53.55	25.50	-	300	200	1
102	5	1.30	1.30	2.00	-	300	200	1
103	16	0.92	0.92	1.42	1.19,1.19,1.19,1.19,1.19,1.19,1.18,1.18,1.17,1.18,1.18,1.18,1.17,1.18,1.18,1.18,1.17,1.17,1.18,1.18,1.17,1.17,1.18,1.18,1.17,1.17	300	200	1
104	16	2.44	2.44	3.75	1.69,1.69,1.69,1.69,1.69,1.69,1.67,1.67,1.66,1.61,1.67,1.67,1.66,1.61,1.67,1.67,1.66,1.61,1.67,1.67,1.65,1.74,1.67,1.67,1.65,1.74,1.67,1.67,1.66,1.64	300	200	1
105	16	1.52	1.52	2.33	1.68,1.68,1.68,1.68,1.68,1.68,1.67,1.67,1.66,1.66,1.67,1.67,1.66,1.66,1.67,1.67,1.66,1.66,1.67,1.67,1.66,1.66,1.67,1.67,1.66,1.66	300	200	1
106	16	0.92	0.92	1.42	1.19,1.19,1.19,1.19,1.19,1.19,1.18,1.18,1.18,1.18,1.18,1.18,1.18,1.18,1.17,1.18,1.18,1.18,1.17,1.17,1.18,1.18,1.17,1.17	300	200	1
107	16	1.52	1.52	2.33	1.68,1.68,1.68,1.68,1.68,1.68,1.67,1.67,1.66,1.66,1.67,1.67,1.66,1.66,1.67,1.67,1.66,1.66,1.67,1.67,1.66,1.66,1.67,1.67,1.66,1.66	300	200	1

103	116.10	115.41	15.79	11.10	42.08	23.28
104	116.10	111.33	15.79	11.10	42.08	23.28
105	116.10	114.23	15.79	11.10	42.08	23.28
106	116.10	115.41	15.79	11.10	42.08	23.28
107	116.10	114.23	15.79	11.10	42.08	23.28
108	133.20	126.01	32.87	6.12	40.24	43.62
109	66.48	58.89	3.82	3.82	19.94	19.94
110	116.10	111.33	15.79	11.10	42.08	23.28
111	133.20	126.01	32.87	6.12	40.24	43.62
112	198.33	196.72	21.95	21.95	59.50	59.50
113	133.20	104.94	24.06	6.12	40.24	43.62
114	133.20	104.94	23.37	6.12	40.24	43.62
115	133.20	69.16	17.95	6.12	40.24	43.62
116	133.20	69.16	17.64	6.12	40.24	43.62
201	535.87	87.94	147.68	147.68	160.76	160.76
202	198.33	196.72	21.95	21.95	59.50	59.50
203	116.10	115.41	15.79	11.10	42.08	23.28
204	116.10	111.33	15.79	11.10	42.08	23.28
205	116.10	114.23	15.79	11.10	42.08	23.28
206	116.10	115.41	15.79	11.10	42.08	23.28
207	116.10	114.23	15.79	11.10	42.08	23.28
208	133.20	126.01	32.87	6.12	40.24	43.62
209	66.48	58.89	3.82	3.82	19.94	19.94
210	116.10	111.33	15.79	11.10	42.08	23.28
211	133.20	126.01	32.87	6.12	40.24	43.62
212	198.33	196.72	21.95	21.95	59.50	59.50
213	133.20	104.94	24.06	6.12	40.24	43.62
214	133.20	104.94	23.37	6.12	40.24	43.62
215	133.20	69.16	17.80	6.12	40.24	43.62
216	133.20	69.16	17.33	6.12	40.24	43.62
301	535.87	87.94	147.68	147.68	160.76	160.76
302	198.33	196.72	21.95	21.95	59.50	59.50
303	116.10	115.41	15.79	11.10	42.08	23.28
304	116.10	111.33	15.79	11.10	42.08	23.28
305	116.10	114.23	15.79	11.10	42.08	23.28
306	116.10	115.41	15.79	11.10	42.08	23.28
307	116.10	114.23	15.79	11.10	42.08	23.28
308	133.20	20.65	32.87	6.12	40.24	43.62
309	66.48	58.89	3.82	3.82	19.94	19.94
310	116.10	111.33	15.79	11.10	42.08	23.28
311	133.20	20.65	32.87	6.12	40.24	43.62
312	198.33	196.72	21.95	21.95	59.50	59.50
313	133.20	104.94	25.21	6.12	40.24	43.62
314	133.20	104.94	24.98	6.12	40.24	43.62
315	133.20	69.16	19.50	6.12	40.24	43.62
316	133.20	69.16	19.19	6.12	40.24	43.62

Design Ratio

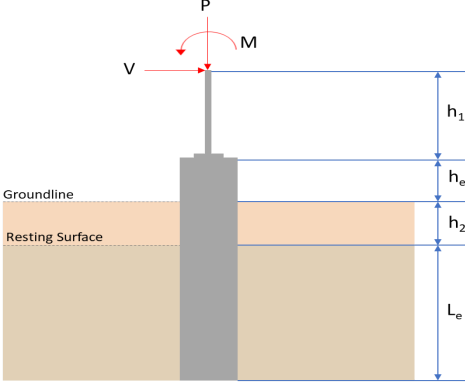
Member ID	P	M _z	M _y	V _y	V _z	(P,M _z ,M _y)	Worst LC	KL/r	δ	Status
1	0.123	0.811	0.019	0.027	0.001	0.882	#13	0.875	Not Required	Pass
2	0.001	0.450	0.210	0.089	0.040	0.660	#13	0.035	Not Required	Pass
3	0.003	0.676	0.015	0.069	0.003	0.688	#13	0.045	Not Required	Pass

4	0.003	0.674	0.049	0.068	0.011	0.684	#13	0.080	Not Required	Pass
5	0.002	0.418	0.050	0.067	0.012	0.430	#13	0.074	Not Required	Pass
6	0.002	0.550	0.011	0.054	0.001	0.560	#13	0.045	Not Required	Pass
7	0.002	0.341	0.045	0.055	0.012	0.354	#13	0.074	Not Required	Pass
8	0.001	0.082	0.048	0.042	0.004	0.131	#13	0.095	Not Required	Pass
9	0.005	0.089	0.045	0.003	0.001	0.136	#13	0.204	Not Required	Pass
10	0.002	0.556	0.055	0.056	0.013	0.600	#13	0.080	Not Required	Pass
11	0.001	0.077	0.047	0.041	0.004	0.124	#13	0.095	Not Required	Pass
12	0.001	0.321	0.174	0.071	0.033	0.496	#13	0.035	Not Required	Pass
13	0.002	0.305	0.120	0.052	0.005	0.406	#13	0.286	Not Required	Pass
14	0.002	0.313	0.120	0.053	0.005	0.406	#13	0.190	Not Required	Pass
15	0.000	0.139	0.072	0.038	0.003	0.201	#13	Not Required	Not Required	Pass
16	0.000	0.139	0.072	0.038	0.003	0.201	#13	Not Required	Not Required	Pass
101	0.118	0.788	0.002	0.026	0.000	0.848	#13	0.875	Not Required	Pass
102	0.001	0.358	0.180	0.076	0.036	0.539	#13	0.035	Not Required	Pass
103	0.002	0.589	0.015	0.059	0.003	0.601	#13	0.045	Not Required	Pass
104	0.002	0.581	0.034	0.058	0.007	0.597	#13	0.080	Not Required	Pass
105	0.002	0.365	0.035	0.059	0.009	0.370	#13	0.074	Not Required	Pass
106	0.002	0.597	0.017	0.060	0.004	0.615	#13	0.045	Not Required	Pass
107	0.002	0.370	0.034	0.059	0.008	0.375	#13	0.074	Not Required	Pass
108	0.002	0.056	0.030	0.039	0.003	0.066	#13	0.095	Not Required	Pass
109	0.002	0.055	0.035	0.001	0.000	0.091	#13	0.204	Not Required	Pass
110	0.002	0.594	0.033	0.060	0.007	0.614	#13	0.080	Not Required	Pass
111	0.001	0.050	0.031	0.039	0.003	0.060	#13	0.095	Not Required	Pass
112	0.001	0.369	0.181	0.078	0.035	0.550	#13	0.035	Not Required	Pass
113	0.002	0.194	0.082	0.050	0.004	0.240	#13	0.286	Not Required	Pass
114	0.003	0.189	0.083	0.050	0.004	0.233	#13	0.286	Not Required	Pass
115	0.001	0.154	0.044	0.036	0.003	0.195	#13	0.473	Not Required	Pass
116	0.003	0.159	0.045	0.036	0.003	0.200	#13	0.473	Not Required	Pass
201	0.118	0.788	0.002	0.026	0.000	0.848	#13	0.875	Not Required	Pass
202	0.001	0.369	0.181	0.078	0.035	0.550	#13	0.035	Not Required	Pass
203	0.002	0.597	0.017	0.060	0.004	0.615	#13	0.045	Not Required	Pass
204	0.002	0.594	0.033	0.060	0.007	0.614	#13	0.080	Not Required	Pass
205	0.002	0.370	0.034	0.059	0.008	0.375	#13	0.074	Not Required	Pass
206	0.002	0.589	0.015	0.059	0.003	0.601	#13	0.045	Not Required	Pass
207	0.002	0.365	0.035	0.059	0.009	0.370	#13	0.074	Not Required	Pass
208	0.001	0.039	0.037	0.036	0.003	0.064	#13	0.095	Not Required	Pass
209	0.002	0.055	0.035	0.001	0.000	0.091	#13	0.204	Not Required	Pass
210	0.002	0.581	0.034	0.058	0.007	0.597	#13	0.080	Not Required	Pass
211	0.001	0.041	0.037	0.036	0.003	0.073	#16	0.095	Not Required	Pass
212	0.001	0.358	0.180	0.076	0.036	0.539	#13	0.035	Not Required	Pass
213	0.002	0.194	0.082	0.050	0.004	0.241	#13	0.286	Not Required	Pass
214	0.003	0.189	0.083	0.050	0.004	0.233	#13	0.286	Not Required	Pass
215	0.001	0.211	0.044	0.039	0.003	0.249	#13	0.473	Not Required	Pass
216	0.003	0.223	0.045	0.039	0.003	0.262	#13	0.473	Not Required	Pass
301	0.123	0.811	0.019	0.027	0.001	0.882	#13	0.875	Not Required	Pass
302	0.001	0.321	0.174	0.071	0.033	0.496	#13	0.035	Not Required	Pass
303	0.002	0.550	0.011	0.054	0.001	0.560	#13	0.045	Not Required	Pass
304	0.002	0.556	0.055	0.056	0.013	0.600	#13	0.080	Not Required	Pass
305	0.002	0.341	0.045	0.055	0.012	0.354	#13	0.074	Not Required	Pass
306	0.003	0.676	0.015	0.069	0.003	0.688	#13	0.045	Not Required	Pass
307	0.002	0.418	0.050	0.067	0.012	0.430	#13	0.074	Not Required	Pass
308	0.000	0.139	0.072	0.038	0.003	0.201	#13	Not Required	Not Required	Pass
309	0.005	0.089	0.045	0.003	0.001	0.136	#13	0.204	Not Required	Pass

309	0.003	0.009	0.049	0.003	0.001	0.130	#13	0.204	Not Required	Pass
310	0.003	0.674	0.049	0.068	0.011	0.683	#13	0.080	Not Required	Pass
311	0.000	0.139	0.072	0.038	0.003	0.201	#13	Not Required	Not Required	Pass
312	0.001	0.450	0.210	0.089	0.040	0.660	#13	0.035	Not Required	Pass
313	0.002	0.305	0.120	0.052	0.005	0.406	#13	0.190	Not Required	Pass
314	0.002	0.313	0.120	0.053	0.005	0.406	#13	0.286	Not Required	Pass
315	0.001	0.146	0.047	0.041	0.004	0.184	#13	0.473	Not Required	Pass
316	0.003	0.147	0.048	0.042	0.004	0.186	#13	0.473	Not Required	Pass

Definitions

Φ_t	Safety factor for tensile
Φ_c	Safety factor for compression
Φ_b	Safety factor for flexure
Φ_v	Safety factor for shear
E	Modulus of elasticity
F_y	Specified minimum yield stress
F_u	Specified minimum tensile strength
A	Cross-sectional area
J	Torsional constant
I_{yp}	Moment of inertia about the Y axes
I_{zp}	Moment of inertia about the Z axes
I_w	Warping constant
S_{yp}	Plastic section modulus about the Y axis
S_{zp}	Plastic section modulus about the Z axis
KL	Effective length
C_b	Buckling modification factor (from all load combinations)
L_b	Length between braced points
LST	Limited slenderness for tension
LSC	Limited slenderness for compression
LD	Limited deflection
P_n	Nominal axial strength (tension/compression)
M_n	Nominal flexural strength (about Z/Y axis)
V_n	Nominal shear strength (along Z/Y axis)
P	Design ratio in case of axial force
M_z	Design ratio in case of bending about Z axis
M_y	Design ratio in case of bending about Y axis
V_y	Design ratio in case of shear along Y axis
V_z	Design ratio in case of shear along Z axis
(P, M_z, M_y)	Design ratio in case of axial force and bending action
KL/r	Design ratio in case of section slenderness
δ	Design ratio in case of member deflection
OK	Capacity is provided
NG	Capacity is not provided

REFERENCES	CALCULATIONS	RESULTS																										
	<p>SkyCiv Foundation Design Pile Foundation</p> <p>Design Information : Design code : IBC 2021 (International Building Code) Unit System : Imperial</p>																											
	<p>Pile Input</p>  <p>Geometry Pile shape: rectangular $b = 48$ in - Pile width $D = 48$ in - Pile depth $L = 9$ ft - Total pile length $h_1 = 0$ ft - Lateral load height from the top of the pile, $h_2 = 0$ ft - Depth to resting surface $h_e = 0$ ft - Length of pile above the ground</p> <p>Tabulation of Soil Parameters</p> <table border="1" data-bbox="416 1102 1193 1191"> <thead> <tr> <th>Layer</th> <th>Label</th> <th>Allowable Bearing Pressure (q_a) (psf)</th> <th>Allowable Lateral Pressure (R) (psf/ft)</th> </tr> </thead> <tbody> <tr> <td>1</td> <td>Sand, silty sand, clayey sand, silty gravel & clayey gravel</td> <td>2000.000</td> <td>150.000</td> </tr> </tbody> </table> <p>Tabulation of Loads</p> <table border="1" data-bbox="675 1288 936 1458"> <thead> <tr> <th>Load Component</th> <th>ASD</th> <th>LRFD</th> </tr> </thead> <tbody> <tr> <td>P (kip)</td> <td>6.967</td> <td>10.399</td> </tr> <tr> <td>V_x (kip)</td> <td>-2.540</td> <td>-4.243</td> </tr> <tr> <td>V_z (kip)</td> <td>0.009</td> <td>0.014</td> </tr> <tr> <td>M_x (kipft)</td> <td>0.077</td> <td>0.118</td> </tr> <tr> <td>M_z (kipft)</td> <td>68.224</td> <td>116.353</td> </tr> </tbody> </table> <p>Material Properties $f'_{ck} = 2.5$ ksi - Concrete strength,</p>	Layer	Label	Allowable Bearing Pressure (q_a) (psf)	Allowable Lateral Pressure (R) (psf/ft)	1	Sand, silty sand, clayey sand, silty gravel & clayey gravel	2000.000	150.000	Load Component	ASD	LRFD	P (kip)	6.967	10.399	V_x (kip)	-2.540	-4.243	V_z (kip)	0.009	0.014	M_x (kipft)	0.077	0.118	M_z (kipft)	68.224	116.353	
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	<p>Required depth to resist lateral loads (ASD) H - Point of application of the lateral load</p> $H = h_1 + h_2 + h_e$ $H = (0 \text{ ft}) + (0 \text{ ft}) + (0 \text{ ft})$ $H = 0 \text{ ft}$ <p>Considering x-direction: H_o - Lateral force per length of pile,</p> $H_o = \frac{V_x}{1.57 D}$ $H_o = \frac{(-2.54 \text{ kip})}{1.57 \times (48 \text{ in})}$ $H_o = -0.40446 \text{ kip/ft}$ <p>M_o - Moment per length of pile,</p> $M_o = \frac{M_x + (V_x H)}{1.57 D}$																											

$$M_o = \frac{(68.224 \text{ kipft}) + ((-2.54 \text{ kip}) \times (0 \text{ ft}))}{1.57 \times (48 \text{ in})}$$

$$M_o = 10.864 \text{ kipft/ft}$$

Required depth of embedment in earth:

$$L_x^3 - \left(14.14 \times \frac{H_o \times L_x}{R}\right) - \left(18.85 \times \frac{M_o}{R}\right) = 0$$

Solving the cubic equation:

$L_{e,x} = 8.6979 \text{ ft}$ - Required depth in x-direction,

Considering z-direction:

H_o - Lateral force per length of pile,

$$H_o = \frac{V_z}{1.57 b}$$

$$H_o = \frac{(0.009 \text{ kip})}{1.57 \times (48 \text{ in})}$$

$$H_o = 0.0014331 \text{ kip/ft}$$

M_o - Moment per length of pile,

$$M_o = \frac{M_x + (V_z H)}{1.57 b}$$

$$M_o = \frac{(0.077 \text{ kipft}) + ((0.009 \text{ kip}) \times (0 \text{ ft}))}{1.57 \times (48 \text{ in})}$$

$$M_o = 0.012261 \text{ kipft/ft}$$

Required depth of embedment in earth:

$$L_z^3 - \left(14.14 \times \frac{H_o \times L_z}{R}\right) - \left(18.85 \times \frac{M_o}{R}\right) = 0$$

Solving the cubic equation:

$L_{e,z} = 1.0223 \text{ ft}$ - Required depth in z-direction,

Minimum embedded depth required:

$L_{e,req}$ - Depth of pile required,

$$L_{e,req} = \text{MAX}[L_{e,x}, L_{e,z}]$$

$$L_{e,req} = \text{MAX}[(8.6979 \text{ ft}), (1.0223 \text{ ft})]$$

$$L_{e,req} = 8.698 \text{ ft}$$

L_e - Actual embedded length of pile,

$$L_e = L - h_c - h_2$$

$$L_e = (9 \text{ ft}) - (0 \text{ ft}) - (0 \text{ ft})$$

$$L_e = 9 \text{ ft}$$

Ratio - Embedded depth

$$\text{Ratio} = \frac{L_{e,req}}{L_e}$$

$$\text{Ratio} = \frac{(8.698 \text{ ft})}{(9 \text{ ft})}$$

$$\text{Ratio} = 0.96644$$

Status: **PASS**
Ratio: **0.970**

End-bearing Capacity (ASD)

A - Pile cross-section area

$$A = b D$$

$$A = (48 \text{ in}) \times (48 \text{ in})$$

$$A = 16 \text{ ft}^2$$

q - End-bearing pressure

$$q = \frac{P_c}{A}$$

$$q = \frac{(6.967 \text{ kip})}{(16 \text{ ft}^2)}$$

$$q = 0.43544 \text{ kip/ft}^2$$

$$q = 0.43544 \text{ kip/ft}^2$$

Check bearing capacity ratio:

Ratio - Capacity

$$\text{Ratio} = \frac{q}{q_a}$$

$$\text{Ratio} = \frac{(0.43544 \text{ kip/ft}^2)}{(2000 \text{ psf})}$$

$$\text{Ratio} = 0.21772$$

Status: **PASS**
Ratio: **0.220**

Czerniak

Lateral Soil Pressure (ASD):

L/D - Length to least lateral dimension ratio,

$$L/D = \frac{L}{D}$$

$$L/D = \frac{(9 \text{ ft})}{(48 \text{ in})}$$

$$L/D = 2.25$$

Since $L/D \leq 10$,

Pile is short.

Considering x-direction:

$H_o = -0.40446 \text{ kip/ft}$ - Lateral force per length of pile,

$M_o = 10.864 \text{ kipft/ft}$ - Overturning moment per length of pile,

a - Distance from resting surface to pivot point,

$$a = \frac{(4 M_o L_e) + (3 H_o L_e^2)}{(6 M_o) + (4 H_o L_e)}$$

$$a = \frac{(4 \times (10.864 \text{ kipft/ft}) \times (9 \text{ ft})) + (3 \times (-0.40446 \text{ kip/ft}) \times (9 \text{ ft})^2)}{(6 \times (10.864 \text{ kipft/ft})) + (4 \times (-0.40446 \text{ kip/ft}) \times (9 \text{ ft}))}$$

$$a = 6.1369 \text{ ft}$$

p - Earth pressure against the pile at distance $a/2$ from resting surface,

$$p = \frac{0.75 [(4 M_o) + (3 H_o L_e)]^2}{L_e^2 [(3 M_o) + (2 H_o L_e)]}$$

$$p = \frac{0.75 \times [(4 \times (10.864 \text{ kipft/ft})) + (3 \times (-0.40446 \text{ kip/ft}) \times (9 \text{ ft}))]^2}{(9 \text{ ft})^2 \times [(3 \times (10.864 \text{ kipft/ft})) + (2 \times (-0.40446 \text{ kip/ft}) \times (9 \text{ ft}))]}$$

$$p = 0.38722 \text{ kip/ft}^2$$

s - Earth pressure against the pile at distance L_e ,

$$s = \frac{6 [(2 M_o) + (H_o L_e)]}{L_e^2}$$

$$s = \frac{6 \times [(2 \times (10.864 \text{ kipft/ft})) + ((-0.40446 \text{ kip/ft}) \times (9 \text{ ft}))]}{(9 \text{ ft})^2}$$

$$s = 1.3398 \text{ kip/ft}^2$$

Check lateral soil pressure capacity:

p_a - Allowable lateral soil pressure at depth $a/2$,

$$p_a = R \frac{a}{2}$$

$$p_a = (150 \text{ psf/ft}) \times \frac{(6.1369 \text{ ft})}{2}$$

$$p_a = 0.46027 \text{ kip/ft}^2$$

Ratio - Lateral soil capacity

$$\text{Ratio} = \frac{p}{p_a}$$

$$\text{Ratio} = \frac{(0.38722 \text{ kip/ft}^2)}{(0.46027 \text{ kip/ft}^2)}$$

$$\text{Ratio} = 0.84128$$

p_a - Allowable lateral soil pressure at depth L_e ,

Status: **PASS**
Ratio: **0.840**

$$p_s = R L_e$$

$$p_s = (150 \text{ psf/ft}) \times (9 \text{ ft})$$

$$p_s = 1.35 \text{ kip/ft}^2$$

Ratio - Lateral soil capacity

$$\text{Ratio} = \frac{s}{p_s}$$

$$\text{Ratio} = \frac{(1.3398 \text{ kip/ft}^2)}{(1.35 \text{ kip/ft}^2)}$$

$$\text{Ratio} = 0.99244$$

Status: **PASS**
Ratio: **0.990**

Considering z-direction:

$H_o = 0.0014331 \text{ kip/ft}$ - Lateral force per length of pile,

$M_o = 0.012261 \text{ kipft/ft}$ - Overturning moment per length of pile,

a - Distance from resting surface to pivot point,

$$a = \frac{(4 M_o L_e) + (3 H_o L_e^2)}{(6 M_o) + (4 H_o L_e)}$$

$$a = \frac{(4 \times (0.012261 \text{ kipft/ft}) \times (9 \text{ ft})) + (3 \times (0.0014331 \text{ kip/ft}) \times (9 \text{ ft})^2)}{(6 \times (0.012261 \text{ kipft/ft})) + (4 \times (0.0014331 \text{ kip/ft}) \times (9 \text{ ft}))}$$

$$a = 6.3092 \text{ ft}$$

p - Earth pressure against the pile at distance $a/2$ from resting surface,

$$p = \frac{0.75 [(4 M_o) + (3 H_o L_e)]^2}{L_e^2 [(3 M_o) + (2 H_o L_e)]}$$

$$p = \frac{0.75 \times [(4 \times (0.012261 \text{ kipft/ft})) + (3 \times (0.0014331 \text{ kip/ft}) \times (9 \text{ ft}))]^2}{(9 \text{ ft})^2 \times [(3 \times (0.012261 \text{ kipft/ft})) + (2 \times (0.0014331 \text{ kip/ft}) \times (9 \text{ ft}))]}$$

$$p = 0.001139 \text{ kip/ft}^2$$

s - Earth pressure against the pile at distance L_e ,

$$s = \frac{6 [(2 M_o) + (H_o L_e)]}{L_e^2}$$

$$s = \frac{6 \times [(2 \times (0.012261 \text{ kipft/ft})) + ((0.0014331 \text{ kip/ft}) \times (9 \text{ ft}))]}{(9 \text{ ft})^2}$$

$$s = 0.0027719 \text{ kip/ft}^2$$

Check lateral soil pressure capacity:

p_a - Allowable lateral soil pressure at depth $a/2$,

$$p_a = R \frac{a}{2}$$

$$p_a = (150 \text{ psf/ft}) \times \frac{(6.3092 \text{ ft})}{2}$$

$$p_a = 0.47319 \text{ kip/ft}^2$$

Ratio - Lateral soil capacity

$$\text{Ratio} = \frac{p}{p_a}$$

$$\text{Ratio} = \frac{(0.001139 \text{ kip/ft}^2)}{(0.47319 \text{ kip/ft}^2)}$$

$$\text{Ratio} = 0.0024071$$

p_s - Allowable lateral soil pressure at depth L_e ,

$$p_s = R L_e$$

$$p_s = (150 \text{ psf/ft}) \times (9 \text{ ft})$$

$$p_s = 1.35 \text{ kip/ft}^2$$

Ratio - Lateral soil capacity

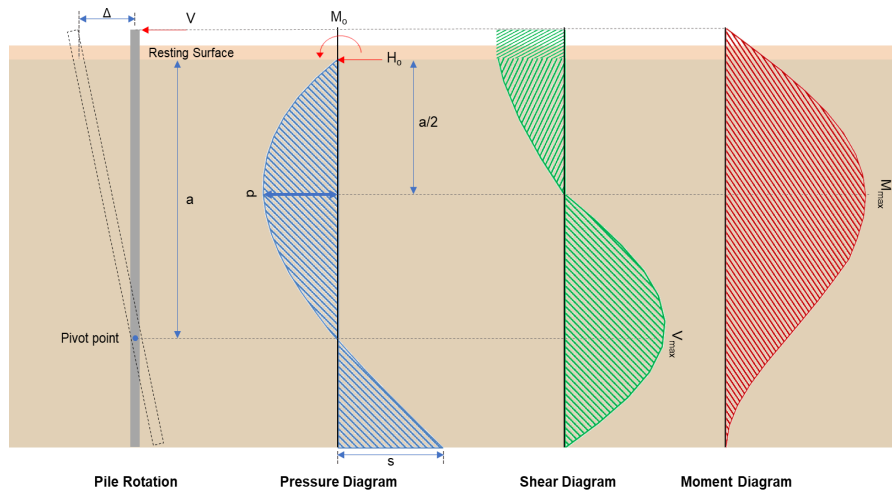
$$\text{Ratio} = \frac{s}{p_s}$$

Status: **PASS**
Ratio: **0.000**

$$Ratio = \frac{(0.0027719 \text{ kip/ft}^2)}{(1.35 \text{ kip/ft}^2)}$$

$$Ratio = 0.0020532$$

Status: **PASS**
Ratio: **0.000**



Shear force and Bending moment (x-direction, LRFD)

H_o - Lateral force per length of pile,

$$H_o = \frac{V_e}{1.57 D}$$

$$H_o = \frac{(-4.243 \text{ kip})}{1.57 \times (48 \text{ in})}$$

$$H_o = -0.67564 \text{ kip/ft}$$

M_o - Moment per length of pile,

$$M_o = \frac{M_z + (V_x H)}{1.57 D}$$

$$M_o = \frac{(116.35 \text{ kipft}) + ((-4.243 \text{ kip}) \times (0 \text{ ft}))}{1.57 \times (48 \text{ in})}$$

$$M_o = 18.528 \text{ kipft/ft}$$

E - Distance from lateral load to resisting surface,

$$E = \frac{M_o}{H_o}$$

$$E = \frac{(18.528 \text{ kipft/ft})}{(-0.67564 \text{ kip/ft})}$$

$$E = 27.422 \text{ ft}$$

a - Distance from resting surface to pivot point,

$$a = \frac{(4 M_o L_e) + (3 H_o L_e^2)}{(6 M_o) + (4 H_o L_e)}$$

$$a = \frac{(4 \times (18.528 \text{ kipft/ft}) \times (9 \text{ ft})) + (3 \times (-0.67564 \text{ kip/ft}) \times (9 \text{ ft})^2)}{(6 \times (18.528 \text{ kipft/ft})) + (4 \times (-0.67564 \text{ kip/ft}) \times (9 \text{ ft}))}$$

$$a = 6.1346 \text{ ft}$$

V_{max} - Max shear force located at depth a ,

$$V_{max} = (H_o D) \left[1 - \left[3 \left(\frac{4 E}{L_e} + 3 \right) \left(\frac{a}{L_e} \right)^2 \right] + \left[4 \left(\frac{3 E}{L_e} + 2 \right) \left(\frac{a}{L_e} \right)^3 \right] \right]$$

$$V_{max} = ((-0.67564 \text{ kip/ft}) \times (48 \text{ in})) \times \left[1 - \left[3 \times \left(\frac{4 \times (27.422 \text{ ft})}{(9 \text{ ft})} + 3 \right) \times \left(\frac{(6.1346 \text{ ft})}{(9 \text{ ft})} \right)^2 \right] + \left[4 \times \left(\frac{3 \times (27.422 \text{ ft})}{(9 \text{ ft})} + 2 \right) \times \left(\frac{(6.1346 \text{ ft})}{(9 \text{ ft})} \right)^3 \right] \right]$$

$$V_{max} = 16.368 \text{ kip}$$

M_{max} - Max bending moment located at depth $a/2$,

$$M_{max} = (H_o D L_e) \left[\left(\frac{E}{L_e} + \frac{a}{2 L_e} \right) - \left[\left(\frac{4 E}{L_e} + 3 \right) \left(\frac{a}{2 L_e} \right)^3 \right] + \left[\left(\frac{3 E}{L_e} + 2 \right) \left(\frac{a}{2 L_e} \right)^4 \right] \right]$$

$$M_{max} = ((-0.67564 \text{ kip/ft}) \times (48 \text{ in}) \times (9 \text{ ft})) \times \left[\left(\frac{(27.422 \text{ ft})}{(9 \text{ ft})} + \frac{(6.1346 \text{ ft})}{2 \times (9 \text{ ft})} \right) - \left[\left(\frac{4 \times (27.422 \text{ ft})}{(9 \text{ ft})} + 3 \right) \times \left(\frac{(6.1346 \text{ ft})}{2 \times (9 \text{ ft})} \right)^3 \right] + \left[\left(\frac{3 \times (27.422 \text{ ft})}{(9 \text{ ft})} + 2 \right) \times \left(\frac{(6.1346 \text{ ft})}{2 \times (9 \text{ ft})} \right)^4 \right] \right]$$

$$M_{max} = 71.432 \text{ kipft}$$

Shear force and Bending moment (z-direction, LRFD)

H_o - Lateral force per length of pile,

$$H_o = \frac{V_z}{1.57 b}$$

$$H_o = \frac{(0.014 \text{ kip})}{1.57 \times (48 \text{ in})}$$

$$H_o = 0.0022293 \text{ kip/ft}$$

M_o - Moment per length of pile,

$$M_o = \frac{M_x + (V_z H)}{1.57 b}$$

$$M_o = \frac{(0.118 \text{ kipft}) + ((0.014 \text{ kip}) \times (0 \text{ ft}))}{1.57 \times (48 \text{ in})}$$

$$M_o = 0.01879 \text{ kipft/ft}$$

E - Distance from lateral load to resisting surface,

$$E = \frac{M_o}{H_o}$$

$$E = \frac{(0.01879 \text{ kipft/ft})}{(0.0022293 \text{ kip/ft})}$$

$$E = 8.4286 \text{ ft}$$

a - Distance from resting surface to pivot point,

$$a = \frac{(4 M_o L_e) + (3 H_o L_e^2)}{(6 M_o) + (4 H_o L_e)}$$

$$a = \frac{(4 \times (0.01879 \text{ kipft/ft}) \times (9 \text{ ft})) + (3 \times (0.0022293 \text{ kip/ft}) \times (9 \text{ ft})^2)}{(6 \times (0.01879 \text{ kipft/ft})) + (4 \times (0.0022293 \text{ kip/ft}) \times (9 \text{ ft}))}$$

$$a = 6.3119 \text{ ft}$$

V_{max} - Max shear force located at depth a ,

$$V_{max} = (H_o b) \left[1 - \left[3 \left(\frac{4 E}{L_e} + 3 \right) \left(\frac{a}{L_e} \right)^2 \right] + \left[4 \left(\frac{3 E}{L_e} + 2 \right) \left(\frac{a}{L_e} \right)^3 \right] \right]$$

$$V_{max} = ((0.0022293 \text{ kip/ft}) \times (48 \text{ in})) \times \left[1 - \left[3 \times \left(\frac{4 \times (8.4286 \text{ ft})}{(9 \text{ ft})} + 3 \right) \times \left(\frac{(6.3119 \text{ ft})}{(9 \text{ ft})} \right)^2 \right] + \left[4 \times \left(\frac{3 \times (8.4286 \text{ ft})}{(9 \text{ ft})} + 2 \right) \times \left(\frac{(6.3119 \text{ ft})}{(9 \text{ ft})} \right)^3 \right] \right]$$

$$V_{max} = 0.02067 \text{ kip}$$

M_{max} - Max bending moment located at depth $a/2$,

$$M_{max} = (H_o b L_e) \left[\left(\frac{E}{L_e} + \frac{a}{2 L_e} \right) - \left[\left(\frac{4 E}{L_e} + 3 \right) \left(\frac{a}{2 L_e} \right)^3 \right] + \left[\left(\frac{3 E}{L_e} + 2 \right) \left(\frac{a}{2 L_e} \right)^4 \right] \right]$$

$$M_{max} = ((0.0022293 \text{ kip/ft}) \times (48 \text{ in}) \times (9 \text{ ft})) \times \left[\left(\frac{(8.4286 \text{ ft})}{(9 \text{ ft})} + \frac{(6.3119 \text{ ft})}{2 \times (9 \text{ ft})} \right) - \left[\left(\frac{4 \times (8.4286 \text{ ft})}{(9 \text{ ft})} + 3 \right) \times \left(\frac{(6.3119 \text{ ft})}{2 \times (9 \text{ ft})} \right)^3 \right] + \left[\left(\frac{3 \times (8.4286 \text{ ft})}{(9 \text{ ft})} + 2 \right) \times \left(\frac{(6.3119 \text{ ft})}{2 \times (9 \text{ ft})} \right)^4 \right] \right]$$

$$M_{max} = 0.085793 \text{ kipft}$$

Minimum Reinforcement Check (LRFD)

Parameters:

$f'_{ck} = 2.5 \text{ ksi}$ - Concrete strength,
 $f_{yk} = 60 \text{ ksi}$ - Longitudinal reinforcement strength,
 $\phi = 0.65$ - Reduction factor for axial strength,
 $\alpha = 0.8$ - Alpha factor for axial strength,
 $A_g = 2304 \text{ in}^2$ - Gross area of concrete,

Table 22.4.2.1

Longitudinal reinforcement:

Required reinforcement due to axial load, $A_{st,required}$

22.4.2.2, 10.6.1.1

$A_{st,required}$

$$A_{st,required} = \text{Min} \left[\frac{\frac{P}{\phi \alpha} - (0.85 f'_{ck} A_g)}{f_{yk} - (0.85 f'_{ck})}, (0.08 A_g) \right]$$

$$A_{st,required} = \text{Min} \left[\frac{\frac{(10.399 \text{ kip})}{(0.65) \times (0.8)} - (0.85 \times (2.5 \text{ ksi}) \times (2304 \text{ in}^2))}{(60 \text{ ksi}) - (0.85 \times (2.5 \text{ ksi}))}, (0.08 \times (2304 \text{ in}^2)) \right]$$

$$A_{st,required} = -84.251 \text{ in}^2$$

A_{min} - Governing minimum reinforcement area,

$$A_{min} = \text{Max} [A_{st,required}, (0.0018 A_g)]$$

$$A_{min} = \text{Max} [(-84.251 \text{ in}^2), (0.0018 \times (2304 \text{ in}^2))]$$

$$A_{min} = 4.1472 \text{ in}^2$$

n_{rebar} - Required number of reinforcement,

$$n_{rebar} = \frac{A_{min}}{A_{rebar}}$$

$$n_{rebar} = \frac{(4.1472 \text{ in}^2)}{(0.3068 \text{ in}^2)}$$

$$n_{rebar} = 14$$

A_{st} - Actual total reinforcement area,

$$A_{st} = n_{rebar} \frac{\pi d_{bar}^2}{4}$$

$$A_{st} = (14) \times \frac{\pi \times (0.625 \text{ in})^2}{4}$$

$$A_{st} = 4.2951 \text{ in}^2$$

Ratio - Capacity

$$\text{Ratio} = \frac{A_{min}}{A_{st}}$$

$$\text{Ratio} = \frac{(4.1472 \text{ in}^2)}{(4.2951 \text{ in}^2)}$$

$$\text{Ratio} = 0.96556$$

Status: **PASS**
Ratio: **0.970**

25.2.3

s_{rebar} - Minimum spacing of reinforcement,

$$s_{rebar} = \text{Max} [1.5, (1.5 d_{bar})]$$

$$s_{rebar} = \text{Max} [1.5, (1.5 \times (0.625 \text{ in}))]$$

$$s_{rebar} = 1.5 \text{ in}$$

Ties:

25.7.2.2

Since longitudinal reinforcement is \leq No. 10: Use #3(0.375 in)

25.7.2.1

s_{ties} - Maximum spacing of ties,

$$s_{ties} = \text{Min} [(16 d_{bar}), (48 d_{ties}), \text{Min} (D, b)]$$

$$s_{ties} = \text{Min} [(16 \times (0.625 \text{ in})), (48 \times (0.375 \text{ in})), \text{Min} ((48 \text{ in}), (48 \text{ in}))]$$

$$s_{ties} = 10 \text{ in}$$

Summary:

Main reinforcement: **14 - #5 (0.625 in)**

Ties: #3(0.375 in) - 10 in

Axial Compression Strength (ACI 318-19, LRFD)

22.4.2.2

ϕP_N - Allowable axial compressive strength

$$\phi P_N = \phi 0.80 [(0.85 f'_{ck} [A_g - A_{st}]) + (f_{yk} A_{st})]$$

$$\phi P_N = (0.65) \times 0.80 \times [(0.85 \times (2.5 \text{ ksi}) \times [(2304 \text{ in}^2) - (4.2951 \text{ in}^2)]) + ((60 \text{ ksi}) \times (4.2951 \text{ in}^2))]$$

$$\phi P_N = 2675.2 \text{ kip}$$

Ratio - Capacity

$$\text{Ratio} = \frac{P}{\phi P_N}$$

$$\text{Ratio} = \frac{(10.399 \text{ kip})}{(2675.2 \text{ kip})}$$

$$\text{Ratio} = 0.0038872$$

Status: **PASS**
Ratio: **0.000**

Shear Strength (ACI 318-19, LRFD)

Parameters:

22.5.2.2

$b_w = 48 \text{ in}$ - Effective width,
 d - Effective depth

$$d = 0.80 D$$

$$d = 0.80 \times (48 \text{ in})$$

$$d = 38.4 \text{ in}$$

22.5.5.1.3

λ_s - size effect modification factor

$$\lambda_s = \text{MIN} \left[\sqrt{\frac{2}{1 + \frac{d}{10}}}, 1 \right]$$

$$\lambda_s = \text{MIN} \left[\sqrt{\frac{2}{1 + \frac{(38.4 \text{ in})}{10}}}, 1 \right]$$

$$\lambda_s = 0.64282$$

22.5.5.1.1

The following variables were converted to be consistent with empirical formula $f'_{ck} = 2.5 \text{ ksi} \rightarrow 2500 \text{ psi}$,
 $V_{c,max}$ - Max shear strength of concrete

$$V_{c,max} = 5 \lambda_s \sqrt{f'_{ck}} b_w d$$

$$V_{c,max} = 5 \times (0.64282) \times \sqrt{(2500 \text{ psi})} \times (48 \text{ in}) \times (38.4 \text{ in})$$

$$V_{c,max} = 296.21 \text{ kip}$$

22.5.5.1.1(a)

The following variables were converted to be consistent with empirical formula $f'_{ck} = 2.5 \text{ ksi} \rightarrow 2500 \text{ psi}$, $P = 10.399 \text{ kip} \rightarrow 10399 \text{ lbf}$,
 $V_{c,a}$ - Shear strength of concrete (a)

$$V_{c,a} = \left[2 \lambda_s \sqrt{f'_{ck}} + \frac{P}{6 A_g} \right] b_w d$$

$$V_{c,a} = \left[2 \times (0.64282) \times \sqrt{(2500 \text{ psi})} + \frac{(10399 \text{ lbf})}{6 \times (2304 \text{ in}^2)} \right] \times (48 \text{ in}) \times (38.4 \text{ in})$$

$$V_{c,a} = 119.87 \text{ kip}$$

22.5.5.1.2

The following variables were converted to be consistent with empirical formula $f'_{ck} = 2.5 \text{ ksi} \rightarrow 2500 \text{ psi}$,
 $V_{c,b}$ - Shear strength of concrete (b)

$$V_{c,b} = \left[2 \lambda_s \sqrt{f'_{ck}} + (0.05 f'_{ck}) \right] b_w d$$

$$V_{c,b} = \left[2 \times (0.64282) \times \sqrt{(2500 \text{ psi})} + (0.05 \times (2500 \text{ psi})) \right] \times (48 \text{ in}) \times (38.4 \text{ in})$$

$$V_{c,b} = 348.89 \text{ kip}$$

V_c - Governing shear strength of concrete

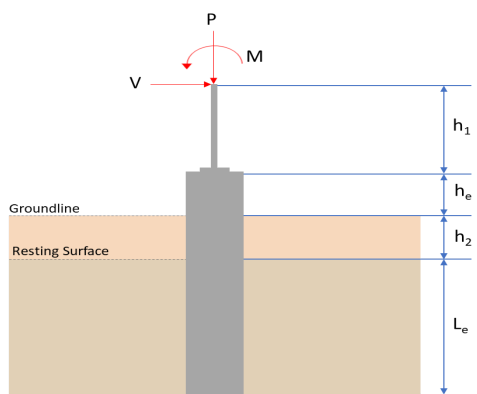
$$V_c = \text{Min}[V_{c,max}, V_{c,a}, V_{c,b}]$$

$$V_c = \text{Min}[(296.21 \text{ kip}), (119.87 \text{ kip}), (348.89 \text{ kip})]$$

$$V_c = 119.87 \text{ kip}$$

<p>22.5.1.2</p>	<p>The following variables were converted to be consistent with empirical formula $f'_{ck} = 2.5 \text{ ksi} \rightarrow 2500 \text{ psi}$.</p> <p>$V_{s,a}$ - Shear strength of steel (a)</p> $V_{s,a} = 8 \sqrt{f'_{ck}} b_w d$ $V_{s,a} = 8 \times \sqrt{(2500 \text{ psi})} \times (48 \text{ in}) \times (38.4 \text{ in})$ $V_{s,a} = 737.28 \text{ kip}$ <p>A_v - Ties rebar area,</p> $A_v = \frac{\pi d_{ties}^2}{4}$ $A_v = \frac{\pi \times (0.375 \text{ in})^2}{4}$ $A_v = 0.11045 \text{ in}^2$ <p>22.5.8.5.3 $V_{s,b}$ - Shear strength of steel (b)</p> $V_{s,b} = \frac{2 A_v f_{yt} d}{s_{ties}}$ $V_{s,b} = \frac{2 \times (0.11045 \text{ in}^2) \times (60 \text{ ksi}) \times (38.4 \text{ in})}{(10 \text{ in})}$ $V_{s,b} = 50.894 \text{ kip}$ <p>V_s - Governing shear strength of steel</p> $V_s = \text{MIN}[V_{s,a}, V_{s,b}]$ $V_s = \text{MIN}[(737.28 \text{ kip}), (50.894 \text{ kip})]$ $V_s = 50.894 \text{ kip}$ <p>22.5.1.1 ϕV_n - Allowable shear strength</p> $\phi V_n = \phi (V_c + V_s)$ $\phi V_n = (0.65) \times ((119.87 \text{ kip}) + (50.894 \text{ kip}))$ $\phi V_n = 111 \text{ kip}$ <p>Considering x-direction:</p> <p>$V_{max} = 16.368 \text{ kip}$ - Maximum shear force in the x-direction, Ratio - Capacity</p> $\text{Ratio} = \frac{V_{max}}{\phi V_n}$ $\text{Ratio} = \frac{(16.368 \text{ kip})}{(111 \text{ kip})}$ $\text{Ratio} = 0.14746$ <p>Considering z-direction:</p> <p>$V_{max} = 0.02067 \text{ kip}$ - Maximum shear force in the z-direction, Ratio - Capacity</p> $\text{Ratio} = \frac{V_{max}}{\phi V_n}$ $\text{Ratio} = \frac{(0.02067 \text{ kip})}{(111 \text{ kip})}$ $\text{Ratio} = 0.00018622$	<p>Status: PASS Ratio: 0.150</p> <p>Status: PASS Ratio: 0.000</p>
	<p>Flexural Strength (ACI 318-19, LFRD)</p> <p>S_m - Section modulus</p> $S_m = \frac{b D^2}{6}$ $S_m = \frac{(48 \text{ in}) \times (48 \text{ in})^2}{6}$ $S_m = 18432 \text{ in}^3$	

<p>14.5.2.1b</p>	<p>$\lambda = 1$ - Concrete modification factor (Normal concrete), Allowable flexural strength: M_n shall be the lesser of: $\phi M_{n,1}$</p> $\phi M_{n,1} = \phi \times 5 \times \lambda \times \sqrt{f'_c} \times S_m$ $\phi M_{n,1} = 0.65 \times 5 \times 1 \times \sqrt{2.5 \text{ksi}} \times 18432.001 \text{in}^3$ $\phi M_{n,1} = 249.600 \text{kipft}$ <p>$\phi M_{n,2}$</p> $\phi M_{n,2} = \phi \times 0.85 \times f'_c \times S_m$ $\phi M_{n,2} = (0.65) \times 0.85 \times (2.5 \text{ksi}) \times (18432 \text{in}^3)$ $\phi M_{n,2} = 2121.6 \text{kipft}$ <p>Therefore, ϕM_n - Allowable flexural strength,</p> $\phi M_n = \text{MIN}[\phi M_{n,1}, \phi M_{n,2}]$ $\phi M_n = \text{MIN}[(249.6 \text{kipft}), (2121.6 \text{kipft})]$ $\phi M_n = 249.6 \text{kipft}$ <p>Considering x-direction: $M_{max} = 71.432 \text{kipft}$ - Maximum moment in the x-direction, Ratio - Capacity</p> $\text{Ratio} = \frac{M_{max}}{\phi M_n}$ $\text{Ratio} = \frac{(71.432 \text{kipft})}{(249.6 \text{kipft})}$ $\text{Ratio} = 0.28619$	<p>Status: PASS Ratio: 0.290</p>
	<p>Considering z-direction: $M_{max} = 0.085793 \text{kipft}$ - Maximum moment in the z-direction, Ratio - Capacity</p> $\text{Ratio} = \frac{M_{max}}{\phi M_n}$ $\text{Ratio} = \frac{(0.085793 \text{kipft})}{(249.6 \text{kipft})}$ $\text{Ratio} = 0.00034372$	<p>Status: PASS Ratio: 0.000</p>

REFERENCES	CALCULATIONS	RESULTS																										
	<p>SkyCiv Foundation Design Pile Foundation</p> <p>Design Information : Design code : IBC 2021 (International Building Code) Unit System : Imperial</p>																											
	<p>Pile Input</p>  <p>Geometry Pile shape: rectangular $b = 48$ in - Pile width $D = 48$ in - Pile depth $L = 9$ ft - Total pile length $h_1 = 0$ ft - Lateral load height from the top of the pile, $h_2 = 0$ ft - Depth to resting surface $h_e = 0$ ft - Length of pile above the ground</p> <p>Tabulation of Soil Parameters</p> <table border="1" data-bbox="414 1097 1189 1198"> <thead> <tr> <th>Layer</th> <th>Label</th> <th>Allowable Bearing Pressure (q_n) (psf)</th> <th>Allowable Lateral Pressure (R) (psf/ft)</th> </tr> </thead> <tbody> <tr> <td>1</td> <td>Sand, silty sand, clayey sand, silty gravel & clayey gravel</td> <td>2000.000</td> <td>150.000</td> </tr> </tbody> </table> <p>Tabulation of Loads</p> <table border="1" data-bbox="670 1288 933 1456"> <thead> <tr> <th>Load Component</th> <th>ASD</th> <th>LRFD</th> </tr> </thead> <tbody> <tr> <td>P (kip)</td> <td>6.967</td> <td>10.399</td> </tr> <tr> <td>V_x (kip)</td> <td>-2.540</td> <td>-4.243</td> </tr> <tr> <td>V_z (kip)</td> <td>-0.009</td> <td>-0.014</td> </tr> <tr> <td>M_x (kipft)</td> <td>-0.077</td> <td>-0.118</td> </tr> <tr> <td>M_z (kipft)</td> <td>68.224</td> <td>116.353</td> </tr> </tbody> </table> <p>Material Properties $f'_{ck} = 2.5$ ksi - Concrete strength,</p>	Layer	Label	Allowable Bearing Pressure (q_n) (psf)	Allowable Lateral Pressure (R) (psf/ft)	1	Sand, silty sand, clayey sand, silty gravel & clayey gravel	2000.000	150.000	Load Component	ASD	LRFD	P (kip)	6.967	10.399	V_x (kip)	-2.540	-4.243	V_z (kip)	-0.009	-0.014	M_x (kipft)	-0.077	-0.118	M_z (kipft)	68.224	116.353	
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	<p>Required depth to resist lateral loads (ASD) H - Point of application of the lateral load</p> $H = h_1 + h_2 + h_e$ $H = (0 \text{ ft}) + (0 \text{ ft}) + (0 \text{ ft})$ $H = 0 \text{ ft}$ <p>Considering x-direction: H_o - Lateral force per length of pile,</p> $H_o = \frac{V_x}{1.57 D}$ $H_o = \frac{(-2.54 \text{ kip})}{1.57 \times (48 \text{ in})}$ $H_o = -0.40446 \text{ kip/ft}$ <p>M_o - Moment per length of pile,</p> $M_o = \frac{M_z + (V_x H)}{1.57 D}$																											

$$M_o = \frac{(68.224 \text{ kipft}) + ((-2.54 \text{ kip}) \times (0 \text{ ft}))}{1.57 \times (48 \text{ in})}$$

$$M_o = 10.864 \text{ kipft/ft}$$

Required depth of embedment in earth:

$$L_x^3 - \left(14.14 \times \frac{H_o \times L_x}{R}\right) - \left(18.85 \times \frac{M_o}{R}\right) = 0$$

Solving the cubic equation:

$L_{e,x} = 8.6979 \text{ ft}$ - Required depth in x-direction,

Considering z-direction:

H_o - Lateral force per length of pile,

$$H_o = \frac{V_z}{1.57 b}$$

$$H_o = \frac{(-0.009 \text{ kip})}{1.57 \times (48 \text{ in})}$$

$$H_o = -0.0014331 \text{ kip/ft}$$

M_o - Moment per length of pile,

$$M_o = \frac{M_x + (V_z H)}{1.57 b}$$

$$M_o = \frac{(0.077 \text{ kipft}) + ((-0.009 \text{ kip}) \times (0 \text{ ft}))}{1.57 \times (48 \text{ in})}$$

$$M_o = 0.012261 \text{ kipft/ft}$$

Required depth of embedment in earth:

$$L_z^3 - \left(14.14 \times \frac{H_o \times L_z}{R}\right) - \left(18.85 \times \frac{M_o}{R}\right) = 0$$

Solving the cubic equation:

$L_{e,z} = 0.96478 \text{ ft}$ - Required depth in z-direction,

Minimum embedded depth required:

$L_{e,req}$ - Depth of pile required,

$$L_{e,req} = \text{MAX}[L_{e,x}, L_{e,z}]$$

$$L_{e,req} = \text{MAX}[(8.6979 \text{ ft}), (0.96478 \text{ ft})]$$

$$L_{e,req} = 8.698 \text{ ft}$$

L_e - Actual embedded length of pile,

$$L_e = L - h_c - h_2$$

$$L_e = (9 \text{ ft}) - (0 \text{ ft}) - (0 \text{ ft})$$

$$L_e = 9 \text{ ft}$$

Ratio - Embedded depth

$$\text{Ratio} = \frac{L_{e,req}}{L_e}$$

$$\text{Ratio} = \frac{(8.698 \text{ ft})}{(9 \text{ ft})}$$

$$\text{Ratio} = 0.96644$$

Status: **PASS**
Ratio: **0.970**

End-bearing Capacity (ASD)

A - Pile cross-section area

$$A = b D$$

$$A = (48 \text{ in}) \times (48 \text{ in})$$

$$A = 16 \text{ ft}^2$$

q - End-bearing pressure

$$q = \frac{P_c}{A}$$

$$q = \frac{(6.967 \text{ kip})}{(16 \text{ ft}^2)}$$

$$q = 0.43544 \text{ kip/ft}^2$$

$$q = 0.43544 \text{ kip/ft}^2$$

Check bearing capacity ratio:

Ratio - Capacity

$$\text{Ratio} = \frac{q}{q_a}$$

$$\text{Ratio} = \frac{(0.43544 \text{ kip/ft}^2)}{(2000 \text{ psf})}$$

$$\text{Ratio} = 0.21772$$

Status: **PASS**
Ratio: **0.220**

Czerniak

Lateral Soil Pressure (ASD):

L/D - Length to least lateral dimension ratio,

$$L/D = \frac{L}{D}$$

$$L/D = \frac{(9 \text{ ft})}{(48 \text{ in})}$$

$$L/D = 2.25$$

Since $L/D \leq 10$,

Pile is short.

Considering x-direction:

$H_o = -0.40446 \text{ kip/ft}$ - Lateral force per length of pile,

$M_o = 10.864 \text{ kipft/ft}$ - Overturning moment per length of pile,

a - Distance from resting surface to pivot point,

$$a = \frac{(4 M_o L_e) + (3 H_o L_e^2)}{(6 M_o) + (4 H_o L_e)}$$

$$a = \frac{(4 \times (10.864 \text{ kipft/ft}) \times (9 \text{ ft})) + (3 \times (-0.40446 \text{ kip/ft}) \times (9 \text{ ft})^2)}{(6 \times (10.864 \text{ kipft/ft})) + (4 \times (-0.40446 \text{ kip/ft}) \times (9 \text{ ft}))}$$

$$a = 6.1369 \text{ ft}$$

p - Earth pressure against the pile at distance $a/2$ from resting surface,

$$p = \frac{0.75 [(4 M_o) + (3 H_o L_e)]^2}{L_e^2 [(3 M_o) + (2 H_o L_e)]}$$

$$p = \frac{0.75 \times [(4 \times (10.864 \text{ kipft/ft})) + (3 \times (-0.40446 \text{ kip/ft}) \times (9 \text{ ft}))]^2}{(9 \text{ ft})^2 \times [(3 \times (10.864 \text{ kipft/ft})) + (2 \times (-0.40446 \text{ kip/ft}) \times (9 \text{ ft}))]}$$

$$p = 0.38722 \text{ kip/ft}^2$$

s - Earth pressure against the pile at distance L_e ,

$$s = \frac{6 [(2 M_o) + (H_o L_e)]}{L_e^2}$$

$$s = \frac{6 \times [(2 \times (10.864 \text{ kipft/ft})) + ((-0.40446 \text{ kip/ft}) \times (9 \text{ ft}))]}{(9 \text{ ft})^2}$$

$$s = 1.3398 \text{ kip/ft}^2$$

Check lateral soil pressure capacity:

p_a - Allowable lateral soil pressure at depth $a/2$,

$$p_a = R \frac{a}{2}$$

$$p_a = (150 \text{ psf/ft}) \times \frac{(6.1369 \text{ ft})}{2}$$

$$p_a = 0.46027 \text{ kip/ft}^2$$

Ratio - Lateral soil capacity

$$\text{Ratio} = \frac{p}{p_a}$$

$$\text{Ratio} = \frac{(0.38722 \text{ kip/ft}^2)}{(0.46027 \text{ kip/ft}^2)}$$

$$\text{Ratio} = 0.84128$$

p_a - Allowable lateral soil pressure at depth L_e ,

Status: **PASS**
Ratio: **0.840**

$$p_s = R L_e$$

$$p_s = (150 \text{ psf/ft}) \times (9 \text{ ft})$$

$$p_s = 1.35 \text{ kip/ft}^2$$

Ratio - Lateral soil capacity

$$\text{Ratio} = \frac{s}{p_s}$$

$$\text{Ratio} = \frac{(1.3398 \text{ kip/ft}^2)}{(1.35 \text{ kip/ft}^2)}$$

$$\text{Ratio} = 0.99244$$

Status: **PASS**
Ratio: **0.990**

Considering z-direction:

$H_o = -0.0014331 \text{ kip/ft}$ - Lateral force per length of pile,

$M_o = 0.012261 \text{ kipft/ft}$ - Overturning moment per length of pile,

a - Distance from resting surface to pivot point,

$$a = \frac{(4 M_o L_e) + (3 H_o L_e^2)}{(6 M_o) + (4 H_o L_e)}$$

$$a = \frac{(4 \times (0.012261 \text{ kipft/ft}) \times (9 \text{ ft})) + (3 \times (-0.0014331 \text{ kip/ft}) \times (9 \text{ ft})^2)}{(6 \times (0.012261 \text{ kipft/ft})) + (4 \times (-0.0014331 \text{ kip/ft}) \times (9 \text{ ft}))}$$

$$a = 6.3092 \text{ ft}$$

p - Earth pressure against the pile at distance $a/2$ from resting surface,

$$p = \frac{0.75 [(4 M_o) + (3 H_o L_e)]^2}{L_e^2 [(3 M_o) + (2 H_o L_e)]}$$

$$p = \frac{0.75 \times [(4 \times (0.012261 \text{ kipft/ft})) + (3 \times (-0.0014331 \text{ kip/ft}) \times (9 \text{ ft}))]^2}{(9 \text{ ft})^2 \times [(3 \times (0.012261 \text{ kipft/ft})) + (2 \times (-0.0014331 \text{ kip/ft}) \times (9 \text{ ft}))]}$$

$$p = 0.000090281 \text{ kip/ft}^2$$

s - Earth pressure against the pile at distance L_e ,

$$s = \frac{6 [(2 M_o) + (H_o L_e)]}{L_e^2}$$

$$s = \frac{6 \times [(2 \times (0.012261 \text{ kipft/ft})) + ((-0.0014331 \text{ kip/ft}) \times (9 \text{ ft}))]}{(9 \text{ ft})^2}$$

$$s = 0.00086105 \text{ kip/ft}^2$$

Check lateral soil pressure capacity:

p_a - Allowable lateral soil pressure at depth $a/2$,

$$p_a = R \frac{a}{2}$$

$$p_a = (150 \text{ psf/ft}) \times \frac{(6.3092 \text{ ft})}{2}$$

$$p_a = 0.47319 \text{ kip/ft}^2$$

Ratio - Lateral soil capacity

$$\text{Ratio} = \frac{p}{p_a}$$

$$\text{Ratio} = \frac{(0.000090281 \text{ kip/ft}^2)}{(0.47319 \text{ kip/ft}^2)}$$

$$\text{Ratio} = 0.00019079$$

p_s - Allowable lateral soil pressure at depth L_e ,

$$p_s = R L_e$$

$$p_s = (150 \text{ psf/ft}) \times (9 \text{ ft})$$

$$p_s = 1.35 \text{ kip/ft}^2$$

Ratio - Lateral soil capacity

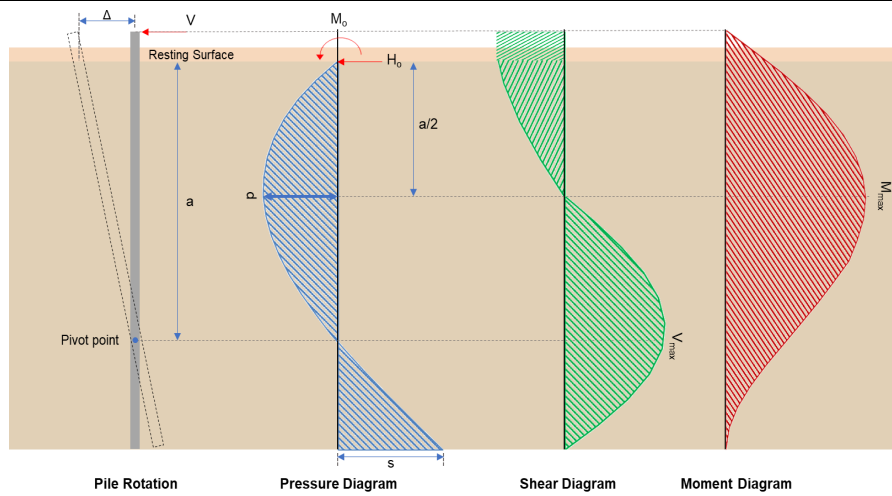
$$\text{Ratio} = \frac{s}{p_s}$$

Status: **PASS**
Ratio: **0.000**

$$\text{Ratio} = \frac{(0.00086105 \text{ kip/ft}^2)}{(1.35 \text{ kip/ft}^2)}$$

$$\text{Ratio} = 0.00063782$$

Status: **PASS**
Ratio: **0.000**



Shear force and Bending moment (x-direction, LRFD)

H_o - Lateral force per length of pile,

$$H_o = \frac{V_x}{1.57 D}$$

$$H_o = \frac{(-4.243 \text{ kip})}{1.57 \times (48 \text{ in})}$$

$$H_o = -0.67564 \text{ kip/ft}$$

M_o - Moment per length of pile,

$$M_o = \frac{M_z + (V_x H)}{1.57 D}$$

$$M_o = \frac{(116.35 \text{ kipft}) + ((-4.243 \text{ kip}) \times (0 \text{ ft}))}{1.57 \times (48 \text{ in})}$$

$$M_o = 18.528 \text{ kipft/ft}$$

E - Distance from lateral load to resisting surface,

$$E = \frac{M_o}{H_o}$$

$$E = \frac{(18.528 \text{ kipft/ft})}{(-0.67564 \text{ kip/ft})}$$

$$E = 27.422 \text{ ft}$$

a - Distance from resting surface to pivot point,

$$a = \frac{(4 M_o L_c) + (3 H_o L_c^2)}{(6 M_o) + (4 H_o L_c)}$$

$$a = \frac{(4 \times (18.528 \text{ kipft/ft}) \times (9 \text{ ft})) + (3 \times (-0.67564 \text{ kip/ft}) \times (9 \text{ ft})^2)}{(6 \times (18.528 \text{ kipft/ft})) + (4 \times (-0.67564 \text{ kip/ft}) \times (9 \text{ ft}))}$$

$$a = 6.1346 \text{ ft}$$

V_{max} - Max shear force located at depth a ,

$$V_{max} = (H_o D) \left[1 - \left[3 \left(\frac{4 E}{L_c} + 3 \right) \left(\frac{a}{L_c} \right)^2 \right] + \left[4 \left(\frac{3 E}{L_c} + 2 \right) \left(\frac{a}{L_c} \right)^3 \right] \right]$$

$$V_{max} = ((-0.67564 \text{ kip/ft}) \times (48 \text{ in})) \times \left[1 - \left[3 \times \left(\frac{4 \times (27.422 \text{ ft})}{(9 \text{ ft})} + 3 \right) \times \left(\frac{(6.1346 \text{ ft})}{(9 \text{ ft})} \right)^2 \right] + \left[4 \times \left(\frac{3 \times (27.422 \text{ ft})}{(9 \text{ ft})} + 2 \right) \times \left(\frac{(6.1346 \text{ ft})}{(9 \text{ ft})} \right)^3 \right] \right]$$

$$V_{max} = 16.368 \text{ kip}$$

M_{max} - Max bending moment located at depth $a/2$,

$$M_{max} = (H_o D L_e) \left[\left(\frac{E}{L_e} + \frac{a}{2 L_e} \right) - \left[\left(\frac{4E}{L_e} + 3 \right) \left(\frac{a}{2 L_e} \right)^3 \right] + \left[\left(\frac{3E}{L_e} + 2 \right) \left(\frac{a}{2 L_e} \right)^4 \right] \right]$$

$$M_{max} = ((-0.67564 \text{ kip/ft}) \times (48 \text{ in}) \times (9 \text{ ft})) \times \left[\left(\frac{(27.422 \text{ ft})}{(9 \text{ ft})} + \frac{(6.1346 \text{ ft})}{2 \times (9 \text{ ft})} \right) - \left[\left(\frac{4 \times (27.422 \text{ ft})}{(9 \text{ ft})} + 3 \right) \times \left(\frac{(6.1346 \text{ ft})}{2 \times (9 \text{ ft})} \right)^3 \right] + \left[\left(\frac{3 \times (27.422 \text{ ft})}{(9 \text{ ft})} + 2 \right) \times \left(\frac{(6.1346 \text{ ft})}{2 \times (9 \text{ ft})} \right)^4 \right] \right]$$

$$M_{max} = 71.432 \text{ kipft}$$

Shear force and Bending moment (z-direction, LRFD)

H_o - Lateral force per length of pile,

$$H_o = \frac{V_z}{1.57 b}$$

$$H_o = \frac{(-0.014 \text{ kip})}{1.57 \times (48 \text{ in})}$$

$$H_o = -0.0022293 \text{ kip/ft}$$

M_o - Moment per length of pile,

$$M_o = \frac{M_x + (V_z H)}{1.57 b}$$

$$M_o = \frac{(0.118 \text{ kipft}) + ((-0.014 \text{ kip}) \times (0 \text{ ft}))}{1.57 \times (48 \text{ in})}$$

$$M_o = 0.01879 \text{ kipft/ft}$$

E - Distance from lateral load to resisting surface,

$$E = \frac{M_o}{H_o}$$

$$E = \frac{(0.01879 \text{ kipft/ft})}{(-0.0022293 \text{ kip/ft})}$$

$$E = 8.4286 \text{ ft}$$

a - Distance from resting surface to pivot point,

$$a = \frac{(4 M_o L_e) + (3 H_o L_e^2)}{(6 M_o) + (4 H_o L_e)}$$

$$a = \frac{(4 \times (0.01879 \text{ kipft/ft}) \times (9 \text{ ft})) + (3 \times (-0.0022293 \text{ kip/ft}) \times (9 \text{ ft})^2)}{(6 \times (0.01879 \text{ kipft/ft})) + (4 \times (-0.0022293 \text{ kip/ft}) \times (9 \text{ ft}))}$$

$$a = 6.3119 \text{ ft}$$

V_{max} - Max shear force located at depth a ,

$$V_{max} = (H_o b) \left[1 - \left[3 \left(\frac{4E}{L_e} + 3 \right) \left(\frac{a}{L_e} \right)^2 \right] + \left[4 \left(\frac{3E}{L_e} + 2 \right) \left(\frac{a}{L_e} \right)^3 \right] \right]$$

$$V_{max} = ((-0.0022293 \text{ kip/ft}) \times (48 \text{ in})) \times \left[1 - \left[3 \times \left(\frac{4 \times (8.4286 \text{ ft})}{(9 \text{ ft})} + 3 \right) \times \left(\frac{(6.3119 \text{ ft})}{(9 \text{ ft})} \right)^2 \right] + \left[4 \times \left(\frac{3 \times (8.4286 \text{ ft})}{(9 \text{ ft})} + 2 \right) \times \left(\frac{(6.3119 \text{ ft})}{(9 \text{ ft})} \right)^3 \right] \right]$$

$$V_{max} = 0.02067 \text{ kip}$$

M_{max} - Max bending moment located at depth $a/2$,

$$M_{max} = (H_o b L_e) \left[\left(\frac{E}{L_e} + \frac{a}{2 L_e} \right) - \left[\left(\frac{4E}{L_e} + 3 \right) \left(\frac{a}{2 L_e} \right)^3 \right] + \left[\left(\frac{3E}{L_e} + 2 \right) \left(\frac{a}{2 L_e} \right)^4 \right] \right]$$

$$M_{max} = ((-0.0022293 \text{ kip/ft}) \times (48 \text{ in}) \times (9 \text{ ft})) \times \left[\left(\frac{(8.4286 \text{ ft})}{(9 \text{ ft})} + \frac{(6.3119 \text{ ft})}{2 \times (9 \text{ ft})} \right) - \left[\left(\frac{4 \times (8.4286 \text{ ft})}{(9 \text{ ft})} + 3 \right) \times \left(\frac{(6.3119 \text{ ft})}{2 \times (9 \text{ ft})} \right)^3 \right] + \left[\left(\frac{3 \times (8.4286 \text{ ft})}{(9 \text{ ft})} + 2 \right) \times \left(\frac{(6.3119 \text{ ft})}{2 \times (9 \text{ ft})} \right)^4 \right] \right]$$

$$M_{max} = 0.085793 \text{ kipft}$$

Minimum Reinforcement Check (LRFD)

Parameters:

$f'_{ck} = 2.5 \text{ ksi}$ - Concrete strength,
 $f_{yk} = 60 \text{ ksi}$ - Longitudinal reinforcement strength,
 $\phi = 0.65$ - Reduction factor for axial strength,
 $\alpha = 0.8$ - Alpha factor for axial strength,
 $A_g = 2304 \text{ in}^2$ - Gross area of concrete,

Table 22.4.2.1

Longitudinal reinforcement:

Required reinforcement due to axial load, $A_{st,required}$

22.4.2.2, 10.6.1.1

$A_{st,required}$

$$A_{st,required} = \text{Min} \left[\frac{\frac{P}{\phi \alpha} - (0.85 f'_{ck} A_g)}{f_{yk} - (0.85 f'_{ck})}, (0.08 A_g) \right]$$

$$A_{st,required} = \text{Min} \left[\frac{\frac{(10.399 \text{ kip})}{(0.65)(0.8)} - (0.85 \times (2.5 \text{ ksi}) \times (2304 \text{ in}^2))}{(60 \text{ ksi}) - (0.85 \times (2.5 \text{ ksi}))}, (0.08 \times (2304 \text{ in}^2)) \right]$$

$$A_{st,required} = -84.251 \text{ in}^2$$

A_{min} - Governing minimum reinforcement area,

$$A_{min} = \text{Max} [A_{st,required}, (0.0018 A_g)]$$

$$A_{min} = \text{Max} [(-84.251 \text{ in}^2), (0.0018 \times (2304 \text{ in}^2))]$$

$$A_{min} = 4.1472 \text{ in}^2$$

n_{rebar} - Required number of reinforcement,

$$n_{rebar} = \frac{A_{min}}{A_{rebar}}$$

$$n_{rebar} = \frac{(4.1472 \text{ in}^2)}{(0.3068 \text{ in}^2)}$$

$$n_{rebar} = 14$$

A_{st} - Actual total reinforcement area,

$$A_{st} = n_{rebar} \frac{\pi d_{bar}^2}{4}$$

$$A_{st} = (14) \times \frac{\pi \times (0.625 \text{ in})^2}{4}$$

$$A_{st} = 4.2951 \text{ in}^2$$

Ratio - Capacity

$$\text{Ratio} = \frac{A_{min}}{A_{st}}$$

$$\text{Ratio} = \frac{(4.1472 \text{ in}^2)}{(4.2951 \text{ in}^2)}$$

$$\text{Ratio} = 0.96556$$

Status: **PASS**
Ratio: **0.970**

25.2.3

s_{rebar} - Minimum spacing of reinforcement,

$$s_{rebar} = \text{Max} [1.5, (1.5 d_{bar})]$$

$$s_{rebar} = \text{Max} [1.5, (1.5 \times (0.625 \text{ in}))]$$

$$s_{rebar} = 1.5 \text{ in}$$

Ties:

25.7.2.2 Since longitudinal reinforcement is \leq No. 10: Use #3(0.375 in)

25.7.2.1 s_{ties} - Maximum spacing of ties,

$$s_{ties} = \text{Min} [(16 d_{bar}), (48 d_{ties}), \text{Min} (D, b)]$$

$$s_{ties} = \text{Min} [(16 \times (0.625 \text{ in})), (48 \times (0.375 \text{ in})), \text{Min} ((48 \text{ in}), (48 \text{ in}))]$$

$$s_{ties} = 10 \text{ in}$$

Summary:

Main reinforcement: **14 - #5 (0.625 in)**

Ties: #3(0.375 in) - 10 in

Axial Compression Strength (ACI 318-19, LRFD)

22.4.2.2

ϕP_N - Allowable axial compressive strength

$$\phi P_N = \phi 0.80 [(0.85 f'_{ck} [A_g - A_{st}]) + (f_{yk} A_{st})]$$

$$\phi P_N = (0.65) \times 0.80 \times [(0.85 \times (2.5 \text{ ksi}) \times [(2304 \text{ in}^2) - (4.2951 \text{ in}^2)]) + ((60 \text{ ksi}) \times (4.2951 \text{ in}^2))]$$

$$\phi P_N = 2675.2 \text{ kip}$$

Ratio - Capacity

$$\text{Ratio} = \frac{P}{\phi P_N}$$

$$\text{Ratio} = \frac{(10.399 \text{ kip})}{(2675.2 \text{ kip})}$$

$$\text{Ratio} = 0.0038872$$

Status: **PASS**
Ratio: **0.000**

Shear Strength (ACI 318-19, LRFD)

Parameters:

22.5.2.2

$b_w = 48 \text{ in}$ - Effective width,
 d - Effective depth

$$d = 0.80 D$$

$$d = 0.80 \times (48 \text{ in})$$

$$d = 38.4 \text{ in}$$

22.5.5.1.3

λ_s - size effect modification factor

$$\lambda_s = \text{MIN} \left[\sqrt{\frac{2}{1 + \frac{d}{10}}}, 1 \right]$$

$$\lambda_s = \text{MIN} \left[\sqrt{\frac{2}{1 + \frac{(38.4 \text{ in})}{10}}}, 1 \right]$$

$$\lambda_s = 0.64282$$

22.5.5.1.1

The following variables were converted to be consistent with empirical formula $f'_{ck} = 2.5 \text{ ksi} \rightarrow 2500 \text{ psi}$,
 $V_{c,max}$ - Max shear strength of concrete

$$V_{c,max} = 5 \lambda_s \sqrt{f'_{ck}} b_w d$$

$$V_{c,max} = 5 \times (0.64282) \times \sqrt{(2500 \text{ psi})} \times (48 \text{ in}) \times (38.4 \text{ in})$$

$$V_{c,max} = 296.21 \text{ kip}$$

22.5.5.1.1(a)

The following variables were converted to be consistent with empirical formula $f'_{ck} = 2.5 \text{ ksi} \rightarrow 2500 \text{ psi}$, $P = 10.399 \text{ kip} \rightarrow 10399 \text{ lbf}$,
 $V_{c,a}$ - Shear strength of concrete (a)

$$V_{c,a} = \left[2 \lambda_s \sqrt{f'_{ck}} + \frac{P}{6 A_g} \right] b_w d$$

$$V_{c,a} = \left[2 \times (0.64282) \times \sqrt{(2500 \text{ psi})} + \frac{(10399 \text{ lbf})}{6 \times (2304 \text{ in}^2)} \right] \times (48 \text{ in}) \times (38.4 \text{ in})$$

$$V_{c,a} = 119.87 \text{ kip}$$

22.5.5.1.2

The following variables were converted to be consistent with empirical formula $f'_{ck} = 2.5 \text{ ksi} \rightarrow 2500 \text{ psi}$,
 $V_{c,b}$ - Shear strength of concrete (b)

$$V_{c,b} = \left[2 \lambda_s \sqrt{f'_{ck}} + (0.05 f'_{ck}) \right] b_w d$$

$$V_{c,b} = \left[2 \times (0.64282) \times \sqrt{(2500 \text{ psi})} + (0.05 \times (2500 \text{ psi})) \right] \times (48 \text{ in}) \times (38.4 \text{ in})$$

$$V_{c,b} = 348.89 \text{ kip}$$

V_c - Governing shear strength of concrete

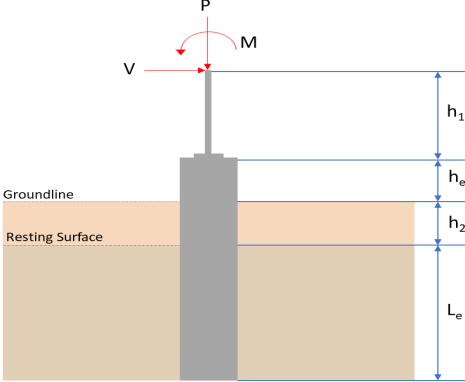
$$V_c = \text{Min}[V_{c,max}, V_{c,a}, V_{c,b}]$$

$$V_c = \text{Min}[(296.21 \text{ kip}), (119.87 \text{ kip}), (348.89 \text{ kip})]$$

$$V_c = 119.87 \text{ kip}$$

<p>22.5.1.2</p>	<p>The following variables were converted to be consistent with empirical formula $f'_{ck} = 2.5 \text{ ksi} \rightarrow 2500 \text{ psi}$.</p> <p>$V_{s,a}$ - Shear strength of steel (a)</p> $V_{s,a} = 8 \sqrt{f'_{ck}} b_w d$ $V_{s,a} = 8 \times \sqrt{(2500 \text{ psi})} \times (48 \text{ in}) \times (38.4 \text{ in})$ $V_{s,a} = 737.28 \text{ kip}$ <p>A_v - Ties rebar area,</p> $A_v = \frac{\pi d_{ties}^2}{4}$ $A_v = \frac{\pi \times (0.375 \text{ in})^2}{4}$ $A_v = 0.11045 \text{ in}^2$ <p>22.5.8.5.3 $V_{s,b}$ - Shear strength of steel (b)</p> $V_{s,b} = \frac{2 A_v f_{yt} d}{s_{ties}}$ $V_{s,b} = \frac{2 \times (0.11045 \text{ in}^2) \times (60 \text{ ksi}) \times (38.4 \text{ in})}{(10 \text{ in})}$ $V_{s,b} = 50.894 \text{ kip}$ <p>V_s - Governing shear strength of steel</p> $V_s = \text{MIN}[V_{s,a}, V_{s,b}]$ $V_s = \text{MIN}[(737.28 \text{ kip}), (50.894 \text{ kip})]$ $V_s = 50.894 \text{ kip}$ <p>22.5.1.1 ϕV_n - Allowable shear strength</p> $\phi V_n = \phi (V_c + V_s)$ $\phi V_n = (0.65) \times ((119.87 \text{ kip}) + (50.894 \text{ kip}))$ $\phi V_n = 111 \text{ kip}$ <p>Considering x-direction:</p> <p>$V_{max} = 16.368 \text{ kip}$ - Maximum shear force in the x-direction, Ratio - Capacity</p> $\text{Ratio} = \frac{V_{max}}{\phi V_n}$ $\text{Ratio} = \frac{(16.368 \text{ kip})}{(111 \text{ kip})}$ $\text{Ratio} = 0.14746$ <p>Considering z-direction:</p> <p>$V_{max} = 0.02067 \text{ kip}$ - Maximum shear force in the z-direction, Ratio - Capacity</p> $\text{Ratio} = \frac{V_{max}}{\phi V_n}$ $\text{Ratio} = \frac{(0.02067 \text{ kip})}{(111 \text{ kip})}$ $\text{Ratio} = 0.00018622$	<p>Status: PASS Ratio: 0.150</p> <p>Status: PASS Ratio: 0.000</p>
	<p>Flexural Strength (ACI 318-19, LRFD)</p> <p>S_m - Section modulus</p> $S_m = \frac{b D^2}{6}$ $S_m = \frac{(48 \text{ in}) \times (48 \text{ in})^2}{6}$ $S_m = 18432 \text{ in}^3$	

<p>14.5.2.1b</p>	<p>$\lambda = 1$ - Concrete modification factor (Normal concrete), Allowable flexural strength: M_n shall be the lesser of: $\phi M_{n,1}$</p> $\phi M_{n,1} = \phi \times 5 \times \lambda \times \sqrt{f'_c} \times S_m$ $\phi M_{n,1} = 0.65 \times 5 \times 1 \times \sqrt{2.5 \text{ksi}} \times 18432.001 \text{in}^3$ $\phi M_{n,1} = 249.600 \text{kipft}$ <p>$\phi M_{n,2}$</p> $\phi M_{n,2} = \phi \times 0.85 \times f'_c \times S_m$ $\phi M_{n,2} = (0.65) \times 0.85 \times (2.5 \text{ksi}) \times (18432 \text{in}^3)$ $\phi M_{n,2} = 2121.6 \text{kipft}$ <p>Therefore, ϕM_n - Allowable flexural strength,</p> $\phi M_n = \text{MIN}[\phi M_{n,1}, \phi M_{n,2}]$ $\phi M_n = \text{MIN}[(249.6 \text{kipft}), (2121.6 \text{kipft})]$ $\phi M_n = 249.6 \text{kipft}$ <p>Considering x-direction: $M_{max} = 71.432 \text{kipft}$ - Maximum moment in the x-direction, Ratio - Capacity</p> $\text{Ratio} = \frac{M_{max}}{\phi M_n}$ $\text{Ratio} = \frac{(71.432 \text{kipft})}{(249.6 \text{kipft})}$ $\text{Ratio} = 0.28619$	<p>Status: PASS Ratio: 0.290</p>
	<p>Considering z-direction: $M_{max} = 0.085793 \text{kipft}$ - Maximum moment in the z-direction, Ratio - Capacity</p> $\text{Ratio} = \frac{M_{max}}{\phi M_n}$ $\text{Ratio} = \frac{(0.085793 \text{kipft})}{(249.6 \text{kipft})}$ $\text{Ratio} = 0.00034372$	<p>Status: PASS Ratio: 0.000</p>

REFERENCES	CALCULATIONS	RESULTS																										
	<p>SkyCiv Foundation Design Pile Foundation</p> <p>Design Information : Design code : IBC 2021 (International Building Code) Unit System : Imperial</p>																											
	<p>Pile Input</p>  <p>Geometry Pile shape: rectangular $b = 48$ in - Pile width $D = 48$ in - Pile depth $L = 9.25$ ft - Total pile length $h_1 = 0$ ft - Lateral load height from the top of the pile, $h_2 = 0$ ft - Depth to resting surface $h_e = 0$ ft - Length of pile above the ground</p> <p>Tabulation of Soil Parameters</p> <table border="1" data-bbox="416 1102 1193 1193"> <thead> <tr> <th>Layer</th> <th>Label</th> <th>Allowable Bearing Pressure (q_a) (psf)</th> <th>Allowable Lateral Pressure (R) (psf/ft)</th> </tr> </thead> <tbody> <tr> <td>1</td> <td>Sand, silty sand, clayey sand, silty gravel & clayey gravel</td> <td>2000.000</td> <td>150.000</td> </tr> </tbody> </table> <p>Tabulation of Loads</p> <table border="1" data-bbox="675 1285 936 1458"> <thead> <tr> <th>Load Component</th> <th>ASD</th> <th>LRFD</th> </tr> </thead> <tbody> <tr> <td>P (kip)</td> <td>7.206</td> <td>10.776</td> </tr> <tr> <td>V_x (kip)</td> <td>-2.618</td> <td>-4.357</td> </tr> <tr> <td>V_z (kip)</td> <td>-0.104</td> <td>-0.164</td> </tr> <tr> <td>M_x (kipft)</td> <td>-0.857</td> <td>-1.358</td> </tr> <tr> <td>M_z (kipft)</td> <td>70.315</td> <td>119.820</td> </tr> </tbody> </table> <p>Material Properties $f'_{ck} = 2.5$ ksi - Concrete strength,</p>	Layer	Label	Allowable Bearing Pressure (q_a) (psf)	Allowable Lateral Pressure (R) (psf/ft)	1	Sand, silty sand, clayey sand, silty gravel & clayey gravel	2000.000	150.000	Load Component	ASD	LRFD	P (kip)	7.206	10.776	V_x (kip)	-2.618	-4.357	V_z (kip)	-0.104	-0.164	M_x (kipft)	-0.857	-1.358	M_z (kipft)	70.315	119.820	
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M_z (kipft)	70.315	119.820																										
	<p>Required depth to resist lateral loads (ASD) H - Point of application of the lateral load</p> $H = h_1 + h_2 + h_e$ $H = (0 \text{ ft}) + (0 \text{ ft}) + (0 \text{ ft})$ $H = 0 \text{ ft}$ <p>Considering x-direction: H_o - Lateral force per length of pile,</p> $H_o = \frac{V_x}{1.57 D}$ $H_o = \frac{(-2.618 \text{ kip})}{1.57 \times (48 \text{ in})}$ $H_o = -0.41688 \text{ kip/ft}$ <p>M_o - Moment per length of pile,</p> $M_o = \frac{M_x + (V_x H)}{1.57 D}$																											

$$M_o = \frac{(70.315 \text{ kipft}) + ((-2.618 \text{ kip}) \times (0 \text{ ft}))}{1.57 \times (48 \text{ in})}$$

$$M_o = 11.197 \text{ kipft/ft}$$

Required depth of embedment in earth:

$$L_x^3 - \left(14.14 \times \frac{H_o \times L_x}{R}\right) - \left(18.85 \times \frac{M_o}{R}\right) = 0$$

Solving the cubic equation:

$L_{e,x} = 8.7772 \text{ ft}$ - Required depth in x-direction,

Considering z-direction:

H_o - Lateral force per length of pile,

$$H_o = \frac{V_z}{1.57 b}$$

$$H_o = \frac{(-0.104 \text{ kip})}{1.57 \times (48 \text{ in})}$$

$$H_o = -0.016561 \text{ kip/ft}$$

M_o - Moment per length of pile,

$$M_o = \frac{M_x + (V_z H)}{1.57 b}$$

$$M_o = \frac{(0.857 \text{ kipft}) + ((-0.104 \text{ kip}) \times (0 \text{ ft}))}{1.57 \times (48 \text{ in})}$$

$$M_o = 0.13646 \text{ kipft/ft}$$

Required depth of embedment in earth:

$$L_z^3 - \left(14.14 \times \frac{H_o \times L_z}{R}\right) - \left(18.85 \times \frac{M_o}{R}\right) = 0$$

Solving the cubic equation:

$L_{e,z} = 2.0693 \text{ ft}$ - Required depth in z-direction,

Minimum embedded depth required:

$L_{e,req}$ - Depth of pile required,

$$L_{e,req} = \text{MAX}[L_{e,x}, L_{e,z}]$$

$$L_{e,req} = \text{MAX}[(8.7772 \text{ ft}), (2.0693 \text{ ft})]$$

$$L_{e,req} = 8.777 \text{ ft}$$

L_e - Actual embedded length of pile,

$$L_e = L - h_c - h_2$$

$$L_e = (9.25 \text{ ft}) - (0 \text{ ft}) - (0 \text{ ft})$$

$$L_e = 9.25 \text{ ft}$$

Ratio - Embedded depth

$$\text{Ratio} = \frac{L_{e,req}}{L_e}$$

$$\text{Ratio} = \frac{(8.777 \text{ ft})}{(9.25 \text{ ft})}$$

$$\text{Ratio} = 0.94886$$

Status: **PASS**
Ratio: **0.950**

End-bearing Capacity (ASD)

A - Pile cross-section area

$$A = b D$$

$$A = (48 \text{ in}) \times (48 \text{ in})$$

$$A = 16 \text{ ft}^2$$

q - End-bearing pressure

$$q = \frac{P_c}{A}$$

$$q = \frac{(7.206 \text{ kip})}{(16 \text{ ft}^2)}$$

$$q = 0.45037 \text{ kip/ft}^2$$

$$q = 0.45037 \text{ kip/ft}$$

Check bearing capacity ratio:

Ratio - Capacity

$$\text{Ratio} = \frac{q}{q_a}$$

$$\text{Ratio} = \frac{(0.45037 \text{ kip/ft}^2)}{(2000 \text{ psf})}$$

$$\text{Ratio} = 0.22519$$

Status: **PASS**
Ratio: **0.230**

Czerniak

Lateral Soil Pressure (ASD):

L/D - Length to least lateral dimension ratio,

$$L/D = \frac{L}{D}$$

$$L/D = \frac{(9.25 \text{ ft})}{(48 \text{ in})}$$

$$L/D = 2.3125$$

Since $L/D \leq 10$,

Pile is short.

Considering x-direction:

$H_o = -0.41688 \text{ kip/ft}$ - Lateral force per length of pile,

$M_o = 11.197 \text{ kipft/ft}$ - Overturning moment per length of pile,

a - Distance from resting surface to pivot point,

$$a = \frac{(4 M_o L_e) + (3 H_o L_e^2)}{(6 M_o) + (4 H_o L_e)}$$

$$a = \frac{(4 \times (11.197 \text{ kipft/ft}) \times (9.25 \text{ ft})) + (3 \times (-0.41688 \text{ kip/ft}) \times (9.25 \text{ ft})^2)}{(6 \times (11.197 \text{ kipft/ft})) + (4 \times (-0.41688 \text{ kip/ft}) \times (9.25 \text{ ft}))}$$

$$a = 6.3106 \text{ ft}$$

p - Earth pressure against the pile at distance $a/2$ from resting surface,

$$p = \frac{0.75 [(4 M_o) + (3 H_o L_e)]^2}{L_e^2 [(3 M_o) + (2 H_o L_e)]}$$

$$p = \frac{0.75 [(4 \times (11.197 \text{ kipft/ft})) + (3 \times (-0.41688 \text{ kip/ft}) \times (9.25 \text{ ft}))]^2}{(9.25 \text{ ft})^2 [(3 \times (11.197 \text{ kipft/ft})) + (2 \times (-0.41688 \text{ kip/ft}) \times (9.25 \text{ ft}))]}$$

$$p = 0.37377 \text{ kip/ft}^2$$

s - Earth pressure against the pile at distance L_e ,

$$s = \frac{6 [(2 M_o) + (H_o L_e)]}{L_e^2}$$

$$s = \frac{6 [(2 \times (11.197 \text{ kipft/ft})) + ((-0.41688 \text{ kip/ft}) \times (9.25 \text{ ft}))]}{(9.25 \text{ ft})^2}$$

$$s = 1.3 \text{ kip/ft}^2$$

Check lateral soil pressure capacity:

p_a - Allowable lateral soil pressure at depth $a/2$,

$$p_a = R \frac{a}{2}$$

$$p_a = (150 \text{ psf/ft}) \times \frac{(6.3106 \text{ ft})}{2}$$

$$p_a = 0.4733 \text{ kip/ft}^2$$

Ratio - Lateral soil capacity

$$\text{Ratio} = \frac{p}{p_a}$$

$$\text{Ratio} = \frac{(0.37377 \text{ kip/ft}^2)}{(0.4733 \text{ kip/ft}^2)}$$

$$\text{Ratio} = 0.78972$$

p_a - Allowable lateral soil pressure at depth L_e ,

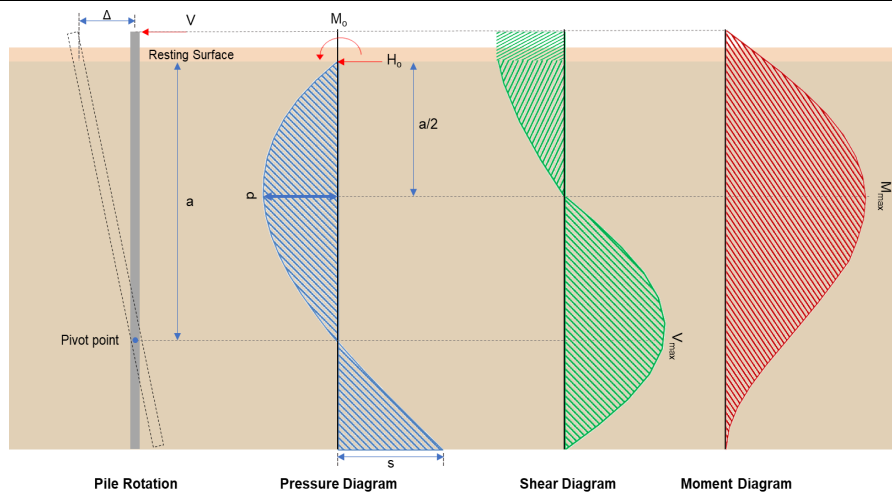
Status: **PASS**
Ratio: **0.790**

	$p_s = R L_e$ $p_s = (150 \text{ psf/ft}) \times (9.25 \text{ ft})$ $p_s = 1.3875 \text{ kip/ft}^2$ <p>Ratio - Lateral soil capacity</p> $\text{Ratio} = \frac{s}{p_s}$ $\text{Ratio} = \frac{(1.3 \text{ kip/ft}^2)}{(1.3875 \text{ kip/ft}^2)}$ $\text{Ratio} = 0.93687$	Status: PASS Ratio: 0.940
	<p>Considering z-direction:</p> <p>$H_o = -0.016561 \text{ kip/ft}$ - Lateral force per length of pile, $M_o = 0.13646 \text{ kipft/ft}$ - Overturning moment per length of pile, a - Distance from resting surface to pivot point,</p> $a = \frac{(4 M_o L_e) + (3 H_o L_e^2)}{(6 M_o) + (4 H_o L_e)}$ $a = \frac{(4 \times (0.13646 \text{ kipft/ft}) \times (9.25 \text{ ft})) + (3 \times (-0.016561 \text{ kip/ft}) \times (9.25 \text{ ft})^2)}{(6 \times (0.13646 \text{ kipft/ft})) + (4 \times (-0.016561 \text{ kip/ft}) \times (9.25 \text{ ft}))}$ $a = 6.4966 \text{ ft}$ <p>p - Earth pressure against the pile at distance $a/2$ from resting surface,</p> $p = \frac{0.75 [(4 M_o) + (3 H_o L_e)]^2}{L_e^2 [(3 M_o) + (2 H_o L_e)]}$ $p = \frac{0.75 [(4 \times (0.13646 \text{ kipft/ft})) + (3 \times (-0.016561 \text{ kip/ft}) \times (9.25 \text{ ft}))]^2}{(9.25 \text{ ft})^2 [(3 \times (0.13646 \text{ kipft/ft})) + (2 \times (-0.016561 \text{ kip/ft}) \times (9.25 \text{ ft}))]}$ $p = 0.00063374 \text{ kip/ft}^2$ <p>s - Earth pressure against the pile at distance L_e,</p> $s = \frac{6 [(2 M_o) + (H_o L_e)]}{L_e^2}$ $s = \frac{6 [(2 \times (0.13646 \text{ kipft/ft})) + ((-0.016561 \text{ kip/ft}) \times (9.25 \text{ ft}))]}{(9.25 \text{ ft})^2}$ $s = 0.008397 \text{ kip/ft}^2$ <p>Check lateral soil pressure capacity:</p> <p>p_a - Allowable lateral soil pressure at depth $a/2$,</p> $p_a = R \frac{a}{2}$ $p_a = (150 \text{ psf/ft}) \times \frac{(6.4966 \text{ ft})}{2}$ $p_a = 0.48725 \text{ kip/ft}^2$ <p>Ratio - Lateral soil capacity</p> $\text{Ratio} = \frac{p}{p_a}$ $\text{Ratio} = \frac{(0.00063374 \text{ kip/ft}^2)}{(0.48725 \text{ kip/ft}^2)}$ $\text{Ratio} = 0.0013007$ <p>p_s - Allowable lateral soil pressure at depth L_e,</p> $p_s = R L_e$ $p_s = (150 \text{ psf/ft}) \times (9.25 \text{ ft})$ $p_s = 1.3875 \text{ kip/ft}^2$ <p>Ratio - Lateral soil capacity</p> $\text{Ratio} = \frac{s}{p_s}$	Status: PASS Ratio: 0.000

$$Ratio = \frac{(0.008397 \text{ kip/ft}^2)}{(1.3875 \text{ kip/ft}^2)}$$

$$Ratio = 0.0060519$$

Status: **PASS**
Ratio: **0.010**



Shear force and Bending moment (x-direction, LRFD)

H_o - Lateral force per length of pile,

$$H_o = \frac{V_x}{1.57 D}$$

$$H_o = \frac{(-4.357 \text{ kip})}{1.57 \times (48 \text{ in})}$$

$$H_o = -0.69379 \text{ kip/ft}$$

M_o - Moment per length of pile,

$$M_o = \frac{M_x + (V_x H)}{1.57 D}$$

$$M_o = \frac{(119.82 \text{ kipft}) + ((-4.357 \text{ kip}) \times (0 \text{ ft}))}{1.57 \times (48 \text{ in})}$$

$$M_o = 19.08 \text{ kipft/ft}$$

E - Distance from lateral load to resisting surface,

$$E = \frac{M_o}{H_o}$$

$$E = \frac{(19.08 \text{ kipft/ft})}{(-0.69379 \text{ kip/ft})}$$

$$E = 27.501 \text{ ft}$$

a - Distance from resting surface to pivot point,

$$a = \frac{(4 M_o L_c) + (3 H_o L_c^2)}{(6 M_o) + (4 H_o L_c)}$$

$$a = \frac{(4 \times (19.08 \text{ kipft/ft}) \times (9.25 \text{ ft})) + (3 \times (-0.69379 \text{ kip/ft}) \times (9.25 \text{ ft})^2)}{(6 \times (19.08 \text{ kipft/ft})) + (4 \times (-0.69379 \text{ kip/ft}) \times (9.25 \text{ ft}))}$$

$$a = 6.3079 \text{ ft}$$

V_{max} - Max shear force located at depth a ,

$$V_{max} = (H_o D) \left[1 - \left[3 \left(\frac{4 E}{L_c} + 3 \right) \left(\frac{a}{L_c} \right)^2 \right] + \left[4 \left(\frac{3 E}{L_c} + 2 \right) \left(\frac{a}{L_c} \right)^3 \right] \right]$$

$$V_{max} = ((-0.69379 \text{ kip/ft}) \times (48 \text{ in})) \times \left[1 - \left[3 \times \left(\frac{4 \times (27.501 \text{ ft})}{(9.25 \text{ ft})} + 3 \right) \times \left(\frac{(6.3079 \text{ ft})}{(9.25 \text{ ft})} \right)^2 \right] + \left[4 \times \left(\frac{3 \times (27.501 \text{ ft})}{(9.25 \text{ ft})} + 2 \right) \times \left(\frac{(6.3079 \text{ ft})}{(9.25 \text{ ft})} \right)^3 \right] \right]$$

$$V_{max} = 16.444 \text{ kip}$$

M_{max} - Max bending moment located at depth $a/2$,

$$M_{max} = (H_o D L_e) \left[\left(\frac{E}{L_e} + \frac{a}{2 L_e} \right) - \left[\left(\frac{4 E}{L_e} + 3 \right) \left(\frac{a}{2 L_e} \right)^3 \right] + \left[\left(\frac{3 E}{L_e} + 2 \right) \left(\frac{a}{2 L_e} \right)^4 \right] \right]$$

$$M_{max} = ((-0.69379 \text{ kip/ft}) \times (48 \text{ in}) \times (9.25 \text{ ft})) \times \left[\left(\frac{(27.501 \text{ ft})}{(9.25 \text{ ft})} + \frac{(6.3079 \text{ ft})}{2 \times (9.25 \text{ ft})} \right) - \left[\left(\frac{4 \times (27.501 \text{ ft})}{(9.25 \text{ ft})} + 3 \right) \times \left(\frac{(6.3079 \text{ ft})}{2 \times (9.25 \text{ ft})} \right)^3 \right] + \left[\left(\frac{3 \times (27.501 \text{ ft})}{(9.25 \text{ ft})} + 2 \right) \times \left(\frac{(6.3079 \text{ ft})}{2 \times (9.25 \text{ ft})} \right)^4 \right] \right]$$

$$M_{max} = 73.706 \text{ kipft}$$

Shear force and Bending moment (z-direction, LRFD)

H_o - Lateral force per length of pile,

$$H_o = \frac{V_z}{1.57 b}$$

$$H_o = \frac{(-0.164 \text{ kip})}{1.57 \times (48 \text{ in})}$$

$$H_o = -0.026115 \text{ kip/ft}$$

M_o - Moment per length of pile,

$$M_o = \frac{M_x + (V_z H)}{1.57 b}$$

$$M_o = \frac{(1.358 \text{ kipft}) + ((-0.164 \text{ kip}) \times (0 \text{ ft}))}{1.57 \times (48 \text{ in})}$$

$$M_o = 0.21624 \text{ kipft/ft}$$

E - Distance from lateral load to resisting surface,

$$E = \frac{M_o}{H_o}$$

$$E = \frac{(0.21624 \text{ kipft/ft})}{(-0.026115 \text{ kip/ft})}$$

$$E = 8.2805 \text{ ft}$$

a - Distance from resting surface to pivot point,

$$a = \frac{(4 M_o L_e) + (3 H_o L_e^2)}{(6 M_o) + (4 H_o L_e)}$$

$$a = \frac{(4 \times (0.21624 \text{ kipft/ft}) \times (9.25 \text{ ft})) + (3 \times (-0.026115 \text{ kip/ft}) \times (9.25 \text{ ft})^2)}{(6 \times (0.21624 \text{ kipft/ft})) + (4 \times (-0.026115 \text{ kip/ft}) \times (9.25 \text{ ft}))}$$

$$a = 6.4957 \text{ ft}$$

V_{max} - Max shear force located at depth a ,

$$V_{max} = (H_o b) \left[1 - \left[3 \left(\frac{4 E}{L_e} + 3 \right) \left(\frac{a}{L_e} \right)^2 \right] + \left[4 \left(\frac{3 E}{L_e} + 2 \right) \left(\frac{a}{L_e} \right)^3 \right] \right]$$

$$V_{max} = ((-0.026115 \text{ kip/ft}) \times (48 \text{ in})) \times \left[1 - \left[3 \times \left(\frac{4 \times (8.2805 \text{ ft})}{(9.25 \text{ ft})} + 3 \right) \times \left(\frac{(6.4957 \text{ ft})}{(9.25 \text{ ft})} \right)^2 \right] + \left[4 \times \left(\frac{3 \times (8.2805 \text{ ft})}{(9.25 \text{ ft})} + 2 \right) \times \left(\frac{(6.4957 \text{ ft})}{(9.25 \text{ ft})} \right)^3 \right] \right]$$

$$V_{max} = 0.23453 \text{ kip}$$

M_{max} - Max bending moment located at depth $a/2$,

$$M_{max} = (H_o b L_e) \left[\left(\frac{E}{L_e} + \frac{a}{2 L_e} \right) - \left[\left(\frac{4 E}{L_e} + 3 \right) \left(\frac{a}{2 L_e} \right)^3 \right] + \left[\left(\frac{3 E}{L_e} + 2 \right) \left(\frac{a}{2 L_e} \right)^4 \right] \right]$$

$$M_{max} = ((-0.026115 \text{ kip/ft}) \times (48 \text{ in}) \times (9.25 \text{ ft})) \times \left[\left(\frac{(8.2805 \text{ ft})}{(9.25 \text{ ft})} + \frac{(6.4957 \text{ ft})}{2 \times (9.25 \text{ ft})} \right) - \left[\left(\frac{4 \times (8.2805 \text{ ft})}{(9.25 \text{ ft})} + 3 \right) \times \left(\frac{(6.4957 \text{ ft})}{2 \times (9.25 \text{ ft})} \right)^3 \right] + \left[\left(\frac{3 \times (8.2805 \text{ ft})}{(9.25 \text{ ft})} + 2 \right) \times \left(\frac{(6.4957 \text{ ft})}{2 \times (9.25 \text{ ft})} \right)^4 \right] \right]$$

$$M_{max} = 0.9978 \text{ kipft}$$

Minimum Reinforcement Check (LRFD)

Parameters:

$f'_{ck} = 2.5 \text{ ksi}$ - Concrete strength,
 $f_{yk} = 60 \text{ ksi}$ - Longitudinal reinforcement strength,
 $\phi = 0.65$ - Reduction factor for axial strength,
 $\alpha = 0.8$ - Alpha factor for axial strength,
 $A_g = 2304 \text{ in}^2$ - Gross area of concrete,

Table 22.4.2.1

Longitudinal reinforcement:

Required reinforcement due to axial load, $A_{st,required}$

22.4.2.2, 10.6.1.1

$A_{st,required}$

$$A_{st,required} = \text{Min} \left[\frac{\frac{P}{\phi \alpha} - (0.85 f'_{ck} A_g)}{f_{yk} - (0.85 f'_{ck})}, (0.08 A_g) \right]$$

$$A_{st,required} = \text{Min} \left[\frac{\frac{(10.776 \text{ kip})}{(0.65) \times (0.8)} - (0.85 \times (2.5 \text{ ksi}) \times (2304 \text{ in}^2))}{(60 \text{ ksi}) - (0.85 \times (2.5 \text{ ksi}))}, (0.08 \times (2304 \text{ in}^2)) \right]$$

$$A_{st,required} = -84.238 \text{ in}^2$$

A_{min} - Governing minimum reinforcement area,

$$A_{min} = \text{Max} [A_{st,required}, (0.0018 A_g)]$$

$$A_{min} = \text{Max} [(-84.238 \text{ in}^2), (0.0018 \times (2304 \text{ in}^2))]$$

$$A_{min} = 4.1472 \text{ in}^2$$

n_{rebar} - Required number of reinforcement,

$$n_{rebar} = \frac{A_{min}}{A_{rebar}}$$

$$n_{rebar} = \frac{(4.1472 \text{ in}^2)}{(0.3068 \text{ in}^2)}$$

$$n_{rebar} = 14$$

A_{st} - Actual total reinforcement area,

$$A_{st} = n_{rebar} \frac{\pi d_{bar}^2}{4}$$

$$A_{st} = (14) \times \frac{\pi \times (0.625 \text{ in})^2}{4}$$

$$A_{st} = 4.2951 \text{ in}^2$$

Ratio - Capacity

$$\text{Ratio} = \frac{A_{min}}{A_{st}}$$

$$\text{Ratio} = \frac{(4.1472 \text{ in}^2)}{(4.2951 \text{ in}^2)}$$

$$\text{Ratio} = 0.96556$$

Status: **PASS**
Ratio: **0.970**

25.2.3 s_{rebar} - Minimum spacing of reinforcement,

$$s_{rebar} = \text{Max} [1.5, (1.5 d_{bar})]$$

$$s_{rebar} = \text{Max} [1.5, (1.5 \times (0.625 \text{ in}))]$$

$$s_{rebar} = 1.5 \text{ in}$$

Ties:

25.7.2.2 Since longitudinal reinforcement is \leq No. 10: Use #3(0.375 in)

25.7.2.1 s_{ties} - Maximum spacing of ties,

$$s_{ties} = \text{Min} [(16 d_{bar}), (48 d_{ties}), \text{Min} (D, b)]$$

$$s_{ties} = \text{Min} [(16 \times (0.625 \text{ in})), (48 \times (0.375 \text{ in})), \text{Min} ((48 \text{ in}), (48 \text{ in}))]$$

$$s_{ties} = 10 \text{ in}$$

Summary:

Main reinforcement: **14 - #5 (0.625 in)**

Ties: #3(0.375 in) - 10 in

Axial Compression Strength (ACI 318-19, LRFD)

22.4.2.2 ϕP_N - Allowable axial compressive strength

$$\phi P_N = \phi 0.80 [(0.85 f'_{ck} [A_g - A_{st}]) + (f_{yk} A_{st})]$$

$$\phi P_N = (0.65) \times 0.80 \times [(0.85 \times (2.5 \text{ ksi}) \times [(2304 \text{ in}^2) - (4.2951 \text{ in}^2)]) + ((60 \text{ ksi}) \times (4.2951 \text{ in}^2))]$$

$$\phi P_N = 2675.2 \text{ kip}$$

Ratio - Capacity

$$\text{Ratio} = \frac{P}{\phi P_N}$$

$$\text{Ratio} = \frac{(10.776 \text{ kip})}{(2675.2 \text{ kip})}$$

$$\text{Ratio} = 0.0040281$$

Status: **PASS**
Ratio: **0.000**

Shear Strength (ACI 318-19, LRFD)

Parameters:

22.5.2.2 $b_w = 48 \text{ in}$ - Effective width,
 d - Effective depth

$$d = 0.80 D$$

$$d = 0.80 \times (48 \text{ in})$$

$$d = 38.4 \text{ in}$$

22.5.5.1.3 λ_s - size effect modification factor

$$\lambda_s = \text{MIN} \left[\sqrt{\frac{2}{1 + \frac{d}{10}}}, 1 \right]$$

$$\lambda_s = \text{MIN} \left[\sqrt{\frac{2}{1 + \frac{(38.4 \text{ in})}{10}}}, 1 \right]$$

$$\lambda_s = 0.64282$$

22.5.5.1.1 The following variables were converted to be consistent with empirical formula $f'_{ck} = 2.5 \text{ ksi} \rightarrow 2500 \text{ psi}$,
 $V_{c,max}$ - Max shear strength of concrete

$$V_{c,max} = 5 \lambda_s \sqrt{f'_{ck}} b_w d$$

$$V_{c,max} = 5 \times (0.64282) \times \sqrt{(2500 \text{ psi})} \times (48 \text{ in}) \times (38.4 \text{ in})$$

$$V_{c,max} = 296.21 \text{ kip}$$

22.5.5.1.1(a) The following variables were converted to be consistent with empirical formula $f'_{ck} = 2.5 \text{ ksi} \rightarrow 2500 \text{ psi}$, $P = 10.776 \text{ kip} \rightarrow 10776 \text{ lbf}$,
 $V_{c,a}$ - Shear strength of concrete (a)

$$V_{c,a} = \left[2 \lambda_s \sqrt{f'_{ck}} + \frac{P}{6 A_g} \right] b_w d$$

$$V_{c,a} = \left[2 \times (0.64282) \times \sqrt{(2500 \text{ psi})} + \frac{(10776 \text{ lbf})}{6 \times (2304 \text{ in}^2)} \right] \times (48 \text{ in}) \times (38.4 \text{ in})$$

$$V_{c,a} = 119.92 \text{ kip}$$

22.5.5.1.2 The following variables were converted to be consistent with empirical formula $f'_{ck} = 2.5 \text{ ksi} \rightarrow 2500 \text{ psi}$,
 $V_{c,b}$ - Shear strength of concrete (b)

$$V_{c,b} = \left[2 \lambda_s \sqrt{f'_{ck}} + (0.05 f'_{ck}) \right] b_w d$$

$$V_{c,b} = \left[2 \times (0.64282) \times \sqrt{(2500 \text{ psi})} + (0.05 \times (2500 \text{ psi})) \right] \times (48 \text{ in}) \times (38.4 \text{ in})$$

$$V_{c,b} = 348.89 \text{ kip}$$

V_c - Governing shear strength of concrete

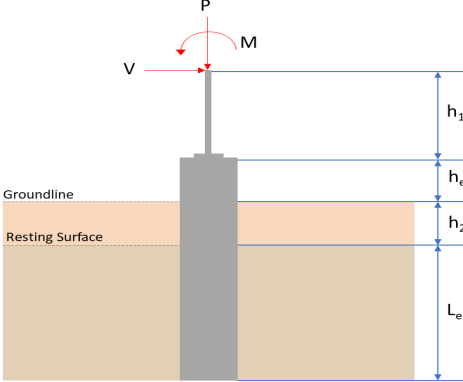
$$V_c = \text{Min}[V_{c,max}, V_{c,a}, V_{c,b}]$$

$$V_c = \text{Min}[(296.21 \text{ kip}), (119.92 \text{ kip}), (348.89 \text{ kip})]$$

$$V_c = 119.92 \text{ kip}$$

<p>22.5.1.2</p>	<p>The following variables were converted to be consistent with empirical formula $f'_{ck} = 2.5 \text{ ksi} \rightarrow 2500 \text{ psi}$.</p> <p>$V_{s,a}$ - Shear strength of steel (a)</p> $V_{s,a} = 8 \sqrt{f'_{ck}} b_w d$ $V_{s,a} = 8 \times \sqrt{(2500 \text{ psi})} \times (48 \text{ in}) \times (38.4 \text{ in})$ $V_{s,a} = 737.28 \text{ kip}$ <p>A_v - Ties rebar area,</p> $A_v = \frac{\pi d_{ties}^2}{4}$ $A_v = \frac{\pi \times (0.375 \text{ in})^2}{4}$ $A_v = 0.11045 \text{ in}^2$ <p>22.5.8.5.3 $V_{s,b}$ - Shear strength of steel (b)</p> $V_{s,b} = \frac{2 A_v f_{yt} d}{s_{ties}}$ $V_{s,b} = \frac{2 \times (0.11045 \text{ in}^2) \times (60 \text{ ksi}) \times (38.4 \text{ in})}{(10 \text{ in})}$ $V_{s,b} = 50.894 \text{ kip}$ <p>V_s - Governing shear strength of steel</p> $V_s = \text{MIN}[V_{s,a}, V_{s,b}]$ $V_s = \text{MIN}[(737.28 \text{ kip}), (50.894 \text{ kip})]$ $V_s = 50.894 \text{ kip}$ <p>22.5.1.1 ϕV_n - Allowable shear strength</p> $\phi V_n = \phi (V_c + V_s)$ $\phi V_n = (0.65) \times ((119.92 \text{ kip}) + (50.894 \text{ kip}))$ $\phi V_n = 111.03 \text{ kip}$ <p>Considering x-direction:</p> <p>$V_{max} = 16.444 \text{ kip}$ - Maximum shear force in the x-direction, Ratio - Capacity</p> $\text{Ratio} = \frac{V_{max}}{\phi V_n}$ $\text{Ratio} = \frac{(16.444 \text{ kip})}{(111.03 \text{ kip})}$ $\text{Ratio} = 0.1481$ <p>Considering z-direction:</p> <p>$V_{max} = 0.23453 \text{ kip}$ - Maximum shear force in the z-direction, Ratio - Capacity</p> $\text{Ratio} = \frac{V_{max}}{\phi V_n}$ $\text{Ratio} = \frac{(0.23453 \text{ kip})}{(111.03 \text{ kip})}$ $\text{Ratio} = 0.0021123$	<p>Status: PASS Ratio: 0.150</p> <p>Status: PASS Ratio: 0.000</p>
	<p>Flexural Strength (ACI 318-19, LRFD)</p> <p>S_m - Section modulus</p> $S_m = \frac{b D^2}{6}$ $S_m = \frac{(48 \text{ in}) \times (48 \text{ in})^2}{6}$ $S_m = 18432 \text{ in}^3$	

<p>14.5.2.1b</p>	<p>$\lambda = 1$ - Concrete modification factor (Normal concrete), Allowable flexural strength: M_n shall be the lesser of: $\phi M_{n,1}$</p> $\phi M_{n,1} = \phi \times 5 \times \lambda \times \sqrt{f'_c} \times S_m$ $\phi M_{n,1} = 0.65 \times 5 \times 1 \times \sqrt{2.5 \text{ ksi}} \times 18432.001 \text{ in}^3$ $\phi M_{n,1} = 249.600 \text{ kipft}$ <p>$\phi M_{n,2}$</p> $\phi M_{n,2} = \phi \times 0.85 \times f'_c \times S_m$ $\phi M_{n,2} = (0.65) \times 0.85 \times (2.5 \text{ ksi}) \times (18432 \text{ in}^3)$ $\phi M_{n,2} = 2121.6 \text{ kipft}$ <p>Therefore, ϕM_n - Allowable flexural strength,</p> $\phi M_n = \text{MIN}[\phi M_{n,1}, \phi M_{n,2}]$ $\phi M_n = \text{MIN}[(249.6 \text{ kipft}), (2121.6 \text{ kipft})]$ $\phi M_n = 249.6 \text{ kipft}$ <p>Considering x-direction: $M_{max} = 73.706 \text{ kipft}$ - Maximum moment in the x-direction, Ratio - Capacity</p> $\text{Ratio} = \frac{M_{max}}{\phi M_n}$ $\text{Ratio} = \frac{(73.706 \text{ kipft})}{(249.6 \text{ kipft})}$ $\text{Ratio} = 0.2953$	<p>Status: PASS Ratio: 0.300</p>
	<p>Considering z-direction: $M_{max} = 0.9978 \text{ kipft}$ - Maximum moment in the z-direction, Ratio - Capacity</p> $\text{Ratio} = \frac{M_{max}}{\phi M_n}$ $\text{Ratio} = \frac{(0.9978 \text{ kipft})}{(249.6 \text{ kipft})}$ $\text{Ratio} = 0.0039976$	<p>Status: PASS Ratio: 0.000</p>

REFERENCES	CALCULATIONS	RESULTS																										
	<p>SkyCiv Foundation Design Pile Foundation</p> <p>Design Information : Design code : IBC 2021 (International Building Code) Unit System : Imperial</p>																											
	<p>Pile Input</p>  <p>Geometry Pile shape: rectangular $b = 48$ in - Pile width $D = 48$ in - Pile depth $L = 9.25$ ft - Total pile length $h_1 = 0$ ft - Lateral load height from the top of the pile, $h_2 = 0$ ft - Depth to resting surface $h_e = 0$ ft - Length of pile above the ground</p> <p>Tabulation of Soil Parameters</p> <table border="1" data-bbox="416 1102 1193 1191"> <thead> <tr> <th>Layer</th> <th>Label</th> <th>Allowable Bearing Pressure (q_a) (psf)</th> <th>Allowable Lateral Pressure (R) (psf/ft)</th> </tr> </thead> <tbody> <tr> <td>1</td> <td>Sand, silty sand, clayey sand, silty gravel & clayey gravel</td> <td>2000.000</td> <td>150.000</td> </tr> </tbody> </table> <p>Tabulation of Loads</p> <table border="1" data-bbox="676 1285 935 1458"> <thead> <tr> <th>Load Component</th> <th>ASD</th> <th>LRFD</th> </tr> </thead> <tbody> <tr> <td>P (kip)</td> <td>7.206</td> <td>10.776</td> </tr> <tr> <td>V_x (kip)</td> <td>-2.618</td> <td>-4.357</td> </tr> <tr> <td>V_z (kip)</td> <td>0.104</td> <td>0.164</td> </tr> <tr> <td>M_x (kipft)</td> <td>0.857</td> <td>1.358</td> </tr> <tr> <td>M_z (kipft)</td> <td>70.315</td> <td>119.820</td> </tr> </tbody> </table> <p>Material Properties $f'_{ck} = 2.5$ ksi - Concrete strength,</p>	Layer	Label	Allowable Bearing Pressure (q_a) (psf)	Allowable Lateral Pressure (R) (psf/ft)	1	Sand, silty sand, clayey sand, silty gravel & clayey gravel	2000.000	150.000	Load Component	ASD	LRFD	P (kip)	7.206	10.776	V_x (kip)	-2.618	-4.357	V_z (kip)	0.104	0.164	M_x (kipft)	0.857	1.358	M_z (kipft)	70.315	119.820	
Layer	Label	Allowable Bearing Pressure (q_a) (psf)	Allowable Lateral Pressure (R) (psf/ft)																									
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M_x (kipft)	0.857	1.358																										
M_z (kipft)	70.315	119.820																										
	<p>Required depth to resist lateral loads (ASD) H - Point of application of the lateral load</p> $H = h_1 + h_2 + h_e$ $H = (0 \text{ ft}) + (0 \text{ ft}) + (0 \text{ ft})$ $H = 0 \text{ ft}$ <p>Considering x-direction: H_o - Lateral force per length of pile,</p> $H_o = \frac{V_x}{1.57 D}$ $H_o = \frac{(-2.618 \text{ kip})}{1.57 \times (48 \text{ in})}$ $H_o = -0.41688 \text{ kip/ft}$ <p>M_o - Moment per length of pile,</p> $M_o = \frac{M_x + (V_x H)}{1.57 D}$																											

$$M_o = \frac{(70.315 \text{ kipft}) + ((-2.618 \text{ kip}) \times (0 \text{ ft}))}{1.57 \times (48 \text{ in})}$$

$$M_o = 11.197 \text{ kipft/ft}$$

Required depth of embedment in earth:

$$L_x^3 - \left(14.14 \times \frac{H_o \times L_x}{R}\right) - \left(18.85 \times \frac{M_o}{R}\right) = 0$$

Solving the cubic equation:

$L_{e,x} = 8.7772 \text{ ft}$ - Required depth in x-direction,

Considering z-direction:

H_o - Lateral force per length of pile,

$$H_o = \frac{V_z}{1.57 b}$$

$$H_o = \frac{(0.104 \text{ kip})}{1.57 \times (48 \text{ in})}$$

$$H_o = 0.016561 \text{ kip/ft}$$

M_o - Moment per length of pile,

$$M_o = \frac{M_x + (V_z H)}{1.57 b}$$

$$M_o = \frac{(0.857 \text{ kipft}) + ((0.104 \text{ kip}) \times (0 \text{ ft}))}{1.57 \times (48 \text{ in})}$$

$$M_o = 0.13646 \text{ kipft/ft}$$

Required depth of embedment in earth:

$$L_z^3 - \left(14.14 \times \frac{H_o \times L_z}{R}\right) - \left(18.85 \times \frac{M_o}{R}\right) = 0$$

Solving the cubic equation:

$L_{e,z} = 2.3674 \text{ ft}$ - Required depth in z-direction,

Minimum embedded depth required:

$L_{e,req}$ - Depth of pile required,

$$L_{e,req} = \text{MAX}[L_{e,x}, L_{e,z}]$$

$$L_{e,req} = \text{MAX}[(8.7772 \text{ ft}), (2.3674 \text{ ft})]$$

$$L_{e,req} = 8.777 \text{ ft}$$

L_e - Actual embedded length of pile,

$$L_e = L - h_e - h_2$$

$$L_e = (9.25 \text{ ft}) - (0 \text{ ft}) - (0 \text{ ft})$$

$$L_e = 9.25 \text{ ft}$$

Ratio - Embedded depth

$$\text{Ratio} = \frac{L_{e,req}}{L_e}$$

$$\text{Ratio} = \frac{(8.777 \text{ ft})}{(9.25 \text{ ft})}$$

$$\text{Ratio} = 0.94886$$

Status: **PASS**
Ratio: **0.950**

End-bearing Capacity (ASD)

A - Pile cross-section area

$$A = b D$$

$$A = (48 \text{ in}) \times (48 \text{ in})$$

$$A = 16 \text{ ft}^2$$

q - End-bearing pressure

$$q = \frac{P_c}{A}$$

$$q = \frac{(7.206 \text{ kip})}{(16 \text{ ft}^2)}$$

$$q = 0.45037 \text{ kip/ft}^2$$

$$q = 0.45037 \text{ kip/ft}$$

Check bearing capacity ratio:

Ratio - Capacity

$$\text{Ratio} = \frac{q}{q_a}$$

$$\text{Ratio} = \frac{(0.45037 \text{ kip/ft}^2)}{(2000 \text{ psf})}$$

$$\text{Ratio} = 0.22519$$

Status: **PASS**
Ratio: **0.230**

Czerniak

Lateral Soil Pressure (ASD):

L/D - Length to least lateral dimension ratio,

$$L/D = \frac{L}{D}$$

$$L/D = \frac{(9.25 \text{ ft})}{(48 \text{ in})}$$

$$L/D = 2.3125$$

Since $L/D \leq 10$,

Pile is short.

Considering x-direction:

$H_o = -0.41688 \text{ kip/ft}$ - Lateral force per length of pile,

$M_o = 11.197 \text{ kipft/ft}$ - Overturning moment per length of pile,

a - Distance from resting surface to pivot point,

$$a = \frac{(4 M_o L_e) + (3 H_o L_e^2)}{(6 M_o) + (4 H_o L_e)}$$

$$a = \frac{(4 \times (11.197 \text{ kipft/ft}) \times (9.25 \text{ ft})) + (3 \times (-0.41688 \text{ kip/ft}) \times (9.25 \text{ ft})^2)}{(6 \times (11.197 \text{ kipft/ft})) + (4 \times (-0.41688 \text{ kip/ft}) \times (9.25 \text{ ft}))}$$

$$a = 6.3106 \text{ ft}$$

p - Earth pressure against the pile at distance $a/2$ from resting surface,

$$p = \frac{0.75 [(4 M_o) + (3 H_o L_e)]^2}{L_e^2 [(3 M_o) + (2 H_o L_e)]}$$

$$p = \frac{0.75 [(4 \times (11.197 \text{ kipft/ft})) + (3 \times (-0.41688 \text{ kip/ft}) \times (9.25 \text{ ft}))]^2}{(9.25 \text{ ft})^2 [(3 \times (11.197 \text{ kipft/ft})) + (2 \times (-0.41688 \text{ kip/ft}) \times (9.25 \text{ ft}))]}$$

$$p = 0.37377 \text{ kip/ft}^2$$

s - Earth pressure against the pile at distance L_e ,

$$s = \frac{6 [(2 M_o) + (H_o L_e)]}{L_e^2}$$

$$s = \frac{6 [(2 \times (11.197 \text{ kipft/ft})) + ((-0.41688 \text{ kip/ft}) \times (9.25 \text{ ft}))]}{(9.25 \text{ ft})^2}$$

$$s = 1.3 \text{ kip/ft}^2$$

Check lateral soil pressure capacity:

p_a - Allowable lateral soil pressure at depth $a/2$,

$$p_a = R \frac{a}{2}$$

$$p_a = (150 \text{ psf/ft}) \times \frac{(6.3106 \text{ ft})}{2}$$

$$p_a = 0.4733 \text{ kip/ft}^2$$

Ratio - Lateral soil capacity

$$\text{Ratio} = \frac{p}{p_a}$$

$$\text{Ratio} = \frac{(0.37377 \text{ kip/ft}^2)}{(0.4733 \text{ kip/ft}^2)}$$

$$\text{Ratio} = 0.78972$$

p_a - Allowable lateral soil pressure at depth L_e ,

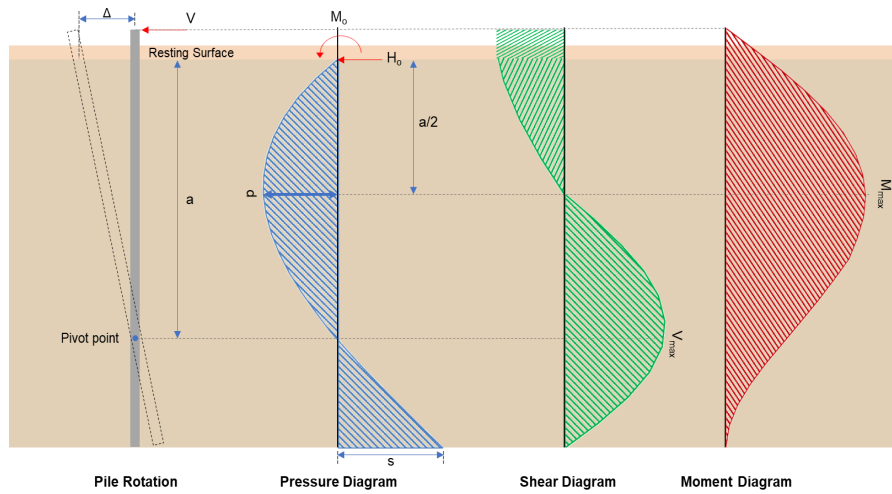
Status: **PASS**
Ratio: **0.790**

	$p_s = R L_e$ $p_s = (150 \text{ psf/ft}) \times (9.25 \text{ ft})$ $p_s = 1.3875 \text{ kip/ft}^2$ <p>Ratio - Lateral soil capacity</p> $\text{Ratio} = \frac{s}{p_s}$ $\text{Ratio} = \frac{(1.3 \text{ kip/ft}^2)}{(1.3875 \text{ kip/ft}^2)}$ $\text{Ratio} = 0.93687$	<p>Status: PASS Ratio: 0.940</p>
	<p>Considering z-direction:</p> <p>$H_o = 0.016561 \text{ kip/ft}$ - Lateral force per length of pile, $M_o = 0.13646 \text{ kipft/ft}$ - Overturning moment per length of pile, a - Distance from resting surface to pivot point,</p> $a = \frac{(4 M_o L_e) + (3 H_o L_e^2)}{(6 M_o) + (4 H_o L_e)}$ $a = \frac{(4 \times (0.13646 \text{ kipft/ft}) \times (9.25 \text{ ft})) + (3 \times (0.016561 \text{ kip/ft}) \times (9.25 \text{ ft})^2)}{(6 \times (0.13646 \text{ kipft/ft})) + (4 \times (0.016561 \text{ kip/ft}) \times (9.25 \text{ ft}))}$ $a = 6.4966 \text{ ft}$ <p>p - Earth pressure against the pile at distance $a/2$ from resting surface,</p> $p = \frac{0.75 [(4 M_o) + (3 H_o L_e)]^2}{L_e^2 [(3 M_o) + (2 H_o L_e)]}$ $p = \frac{0.75 \times [(4 \times (0.13646 \text{ kipft/ft})) + (3 \times (0.016561 \text{ kip/ft}) \times (9.25 \text{ ft}))]^2}{(9.25 \text{ ft})^2 \times [(3 \times (0.13646 \text{ kipft/ft})) + (2 \times (0.016561 \text{ kip/ft}) \times (9.25 \text{ ft}))]}$ $p = 0.012379 \text{ kip/ft}^2$ <p>s - Earth pressure against the pile at distance L_e,</p> $s = \frac{6 [(2 M_o) + (H_o L_e)]}{L_e^2}$ $s = \frac{6 \times [(2 \times (0.13646 \text{ kipft/ft})) + ((0.016561 \text{ kip/ft}) \times (9.25 \text{ ft}))]}{(9.25 \text{ ft})^2}$ $s = 0.029881 \text{ kip/ft}^2$ <p>Check lateral soil pressure capacity:</p> <p>p_a - Allowable lateral soil pressure at depth $a/2$,</p> $p_a = R \frac{a}{2}$ $p_a = (150 \text{ psf/ft}) \times \frac{(6.4966 \text{ ft})}{2}$ $p_a = 0.48725 \text{ kip/ft}^2$ <p>Ratio - Lateral soil capacity</p> $\text{Ratio} = \frac{p}{p_a}$ $\text{Ratio} = \frac{(0.012379 \text{ kip/ft}^2)}{(0.48725 \text{ kip/ft}^2)}$ $\text{Ratio} = 0.025407$ <p>p_s - Allowable lateral soil pressure at depth L_e,</p> $p_s = R L_e$ $p_s = (150 \text{ psf/ft}) \times (9.25 \text{ ft})$ $p_s = 1.3875 \text{ kip/ft}^2$ <p>Ratio - Lateral soil capacity</p> $\text{Ratio} = \frac{s}{p_s}$	<p>Status: PASS Ratio: 0.030</p>

$$Ratio = \frac{(0.029881 \text{ kip/ft}^2)}{(1.3875 \text{ kip/ft}^2)}$$

$$Ratio = 0.021536$$

Status: **PASS**
Ratio: **0.020**



Shear force and Bending moment (x-direction, LRFD)

H_o - Lateral force per length of pile,

$$H_o = \frac{V_x}{1.57 D}$$

$$H_o = \frac{(-4.357 \text{ kip})}{1.57 \times (48 \text{ in})}$$

$$H_o = -0.69379 \text{ kip/ft}$$

M_o - Moment per length of pile,

$$M_o = \frac{M_x + (V_x H)}{1.57 D}$$

$$M_o = \frac{(119.82 \text{ kipft}) + ((-4.357 \text{ kip}) \times (0 \text{ ft}))}{1.57 \times (48 \text{ in})}$$

$$M_o = 19.08 \text{ kipft/ft}$$

E - Distance from lateral load to resisting surface,

$$E = \frac{M_o}{H_o}$$

$$E = \frac{(19.08 \text{ kipft/ft})}{(-0.69379 \text{ kip/ft})}$$

$$E = 27.501 \text{ ft}$$

a - Distance from resting surface to pivot point,

$$a = \frac{(4 M_o L_c) + (3 H_o L_c^2)}{(6 M_o) + (4 H_o L_c)}$$

$$a = \frac{(4 \times (19.08 \text{ kipft/ft}) \times (9.25 \text{ ft})) + (3 \times (-0.69379 \text{ kip/ft}) \times (9.25 \text{ ft})^2)}{(6 \times (19.08 \text{ kipft/ft})) + (4 \times (-0.69379 \text{ kip/ft}) \times (9.25 \text{ ft}))}$$

$$a = 6.3079 \text{ ft}$$

V_{max} - Max shear force located at depth a ,

$$V_{max} = (H_o D) \left[1 - \left[3 \left(\frac{4 E}{L_c} + 3 \right) \left(\frac{a}{L_c} \right)^2 \right] + \left[4 \left(\frac{3 E}{L_c} + 2 \right) \left(\frac{a}{L_c} \right)^3 \right] \right]$$

$$V_{max} = ((-0.69379 \text{ kip/ft}) \times (48 \text{ in})) \times \left[1 - \left[3 \times \left(\frac{4 \times (27.501 \text{ ft})}{(9.25 \text{ ft})} + 3 \right) \times \left(\frac{(6.3079 \text{ ft})}{(9.25 \text{ ft})} \right)^2 \right] + \left[4 \times \left(\frac{3 \times (27.501 \text{ ft})}{(9.25 \text{ ft})} + 2 \right) \times \left(\frac{(6.3079 \text{ ft})}{(9.25 \text{ ft})} \right)^3 \right] \right]$$

$$V_{max} = 16.444 \text{ kip}$$

M_{max} - Max bending moment located at depth $a/2$,

$$M_{max} = (H_o D L_e) \left[\left(\frac{E}{L_e} + \frac{a}{2 L_e} \right) - \left[\left(\frac{4 E}{L_e} + 3 \right) \left(\frac{a}{2 L_e} \right)^3 \right] + \left[\left(\frac{3 E}{L_e} + 2 \right) \left(\frac{a}{2 L_e} \right)^4 \right] \right]$$

$$M_{max} = ((-0.69379 \text{ kip/ft}) \times (48 \text{ in}) \times (9.25 \text{ ft})) \times \left[\left(\frac{(27.501 \text{ ft})}{(9.25 \text{ ft})} + \frac{(6.3079 \text{ ft})}{2 \times (9.25 \text{ ft})} \right) - \left[\left(\frac{4 \times (27.501 \text{ ft})}{(9.25 \text{ ft})} + 3 \right) \times \left(\frac{(6.3079 \text{ ft})}{2 \times (9.25 \text{ ft})} \right)^3 \right] + \left[\left(\frac{3 \times (27.501 \text{ ft})}{(9.25 \text{ ft})} + 2 \right) \times \left(\frac{(6.3079 \text{ ft})}{2 \times (9.25 \text{ ft})} \right)^4 \right] \right]$$

$$M_{max} = 73.706 \text{ kipft}$$

Shear force and Bending moment (z-direction, LRFD)

H_o - Lateral force per length of pile,

$$H_o = \frac{V_z}{1.57 b}$$

$$H_o = \frac{(0.164 \text{ kip})}{1.57 \times (48 \text{ in})}$$

$$H_o = 0.026115 \text{ kip/ft}$$

M_o - Moment per length of pile,

$$M_o = \frac{M_x + (V_z H)}{1.57 b}$$

$$M_o = \frac{(1.358 \text{ kipft}) + ((0.164 \text{ kip}) \times (0 \text{ ft}))}{1.57 \times (48 \text{ in})}$$

$$M_o = 0.21624 \text{ kipft/ft}$$

E - Distance from lateral load to resisting surface,

$$E = \frac{M_o}{H_o}$$

$$E = \frac{(0.21624 \text{ kipft/ft})}{(0.026115 \text{ kip/ft})}$$

$$E = 8.2805 \text{ ft}$$

a - Distance from resting surface to pivot point,

$$a = \frac{(4 M_o L_e) + (3 H_o L_e^2)}{(6 M_o) + (4 H_o L_e)}$$

$$a = \frac{(4 \times (0.21624 \text{ kipft/ft}) \times (9.25 \text{ ft})) + (3 \times (0.026115 \text{ kip/ft}) \times (9.25 \text{ ft})^2)}{(6 \times (0.21624 \text{ kipft/ft})) + (4 \times (0.026115 \text{ kip/ft}) \times (9.25 \text{ ft}))}$$

$$a = 6.4957 \text{ ft}$$

V_{max} - Max shear force located at depth a ,

$$V_{max} = (H_o b) \left[1 - \left[3 \left(\frac{4 E}{L_e} + 3 \right) \left(\frac{a}{L_e} \right)^2 \right] + \left[4 \left(\frac{3 E}{L_e} + 2 \right) \left(\frac{a}{L_e} \right)^3 \right] \right]$$

$$V_{max} = ((0.026115 \text{ kip/ft}) \times (48 \text{ in})) \times \left[1 - \left[3 \times \left(\frac{4 \times (8.2805 \text{ ft})}{(9.25 \text{ ft})} + 3 \right) \times \left(\frac{(6.4957 \text{ ft})}{(9.25 \text{ ft})} \right)^2 \right] + \left[4 \times \left(\frac{3 \times (8.2805 \text{ ft})}{(9.25 \text{ ft})} + 2 \right) \times \left(\frac{(6.4957 \text{ ft})}{(9.25 \text{ ft})} \right)^3 \right] \right]$$

$$V_{max} = 0.23453 \text{ kip}$$

M_{max} - Max bending moment located at depth $a/2$,

$$M_{max} = (H_o b L_e) \left[\left(\frac{E}{L_e} + \frac{a}{2 L_e} \right) - \left[\left(\frac{4 E}{L_e} + 3 \right) \left(\frac{a}{2 L_e} \right)^3 \right] + \left[\left(\frac{3 E}{L_e} + 2 \right) \left(\frac{a}{2 L_e} \right)^4 \right] \right]$$

$$M_{max} = ((0.026115 \text{ kip/ft}) \times (48 \text{ in}) \times (9.25 \text{ ft})) \times \left[\left(\frac{(8.2805 \text{ ft})}{(9.25 \text{ ft})} + \frac{(6.4957 \text{ ft})}{2 \times (9.25 \text{ ft})} \right) - \left[\left(\frac{4 \times (8.2805 \text{ ft})}{(9.25 \text{ ft})} + 3 \right) \times \left(\frac{(6.4957 \text{ ft})}{2 \times (9.25 \text{ ft})} \right)^3 \right] + \left[\left(\frac{3 \times (8.2805 \text{ ft})}{(9.25 \text{ ft})} + 2 \right) \times \left(\frac{(6.4957 \text{ ft})}{2 \times (9.25 \text{ ft})} \right)^4 \right] \right]$$

$$M_{max} = 0.9978 \text{ kipft}$$

Minimum Reinforcement Check (LRFD)

Parameters:

$f'_{ck} = 2.5 \text{ ksi}$ - Concrete strength,
 $f_{yk} = 60 \text{ ksi}$ - Longitudinal reinforcement strength,
 $\phi = 0.65$ - Reduction factor for axial strength,
 $\alpha = 0.8$ - Alpha factor for axial strength,
 $A_g = 2304 \text{ in}^2$ - Gross area of concrete,

Table 22.4.2.1

Longitudinal reinforcement:

Required reinforcement due to axial load, $A_{st,required}$

22.4.2.2, 10.6.1.1

$A_{st,required}$

$$A_{st,required} = \text{Min} \left[\frac{\frac{P}{\phi \alpha} - (0.85 f'_{ck} A_g)}{f_{yk} - (0.85 f'_{ck})}, (0.08 A_g) \right]$$

$$A_{st,required} = \text{Min} \left[\frac{\frac{(10.776 \text{ kip})}{(0.65) \times (0.8)} - (0.85 \times (2.5 \text{ ksi}) \times (2304 \text{ in}^2))}{(60 \text{ ksi}) - (0.85 \times (2.5 \text{ ksi}))}, (0.08 \times (2304 \text{ in}^2)) \right]$$

$$A_{st,required} = -84.238 \text{ in}^2$$

A_{min} - Governing minimum reinforcement area,

$$A_{min} = \text{Max} [A_{st,required}, (0.0018 A_g)]$$

$$A_{min} = \text{Max} [(-84.238 \text{ in}^2), (0.0018 \times (2304 \text{ in}^2))]$$

$$A_{min} = 4.1472 \text{ in}^2$$

n_{rebar} - Required number of reinforcement,

$$n_{rebar} = \frac{A_{min}}{A_{rebar}}$$

$$n_{rebar} = \frac{(4.1472 \text{ in}^2)}{(0.3068 \text{ in}^2)}$$

$$n_{rebar} = 14$$

A_{st} - Actual total reinforcement area,

$$A_{st} = n_{rebar} \frac{\pi d_{bar}^2}{4}$$

$$A_{st} = (14) \times \frac{\pi \times (0.625 \text{ in})^2}{4}$$

$$A_{st} = 4.2951 \text{ in}^2$$

Ratio - Capacity

$$\text{Ratio} = \frac{A_{min}}{A_{st}}$$

$$\text{Ratio} = \frac{(4.1472 \text{ in}^2)}{(4.2951 \text{ in}^2)}$$

$$\text{Ratio} = 0.96556$$

Status: **PASS**
Ratio: **0.970**

25.2.3 s_{rebar} - Minimum spacing of reinforcement,

$$s_{rebar} = \text{Max} [1.5, (1.5 d_{bar})]$$

$$s_{rebar} = \text{Max} [1.5, (1.5 \times (0.625 \text{ in}))]$$

$$s_{rebar} = 1.5 \text{ in}$$

Ties:

25.7.2.2 Since longitudinal reinforcement is \leq No. 10: Use #3(0.375 in)

25.7.2.1 s_{ties} - Maximum spacing of ties,

$$s_{ties} = \text{Min} [(16 d_{bar}), (48 d_{ties}), \text{Min} (D, b)]$$

$$s_{ties} = \text{Min} [(16 \times (0.625 \text{ in})), (48 \times (0.375 \text{ in})), \text{Min} ((48 \text{ in}), (48 \text{ in}))]$$

$$s_{ties} = 10 \text{ in}$$

Summary:

Main reinforcement: **14 - #5 (0.625 in)**

Ties: #3(0.375 in) - 10 in

Axial Compression Strength (ACI 318-19, LRFD)

22.4.2.2

ϕP_N - Allowable axial compressive strength

$$\phi P_N = \phi 0.80 [(0.85 f'_{ck} [A_g - A_{st}]) + (f_{yk} A_{st})]$$

$$\phi P_N = (0.65) \times 0.80 \times [(0.85 \times (2.5 \text{ ksi}) \times [(2304 \text{ in}^2) - (4.2951 \text{ in}^2)]) + ((60 \text{ ksi}) \times (4.2951 \text{ in}^2))]$$

$$\phi P_N = 2675.2 \text{ kip}$$

Ratio - Capacity

$$\text{Ratio} = \frac{P}{\phi P_N}$$

$$\text{Ratio} = \frac{(10.776 \text{ kip})}{(2675.2 \text{ kip})}$$

$$\text{Ratio} = 0.0040281$$

Status: **PASS**
Ratio: **0.000**

Shear Strength (ACI 318-19, LRFD)

Parameters:

22.5.2.2

$b_w = 48 \text{ in}$ - Effective width,
 d - Effective depth

$$d = 0.80 D$$

$$d = 0.80 \times (48 \text{ in})$$

$$d = 38.4 \text{ in}$$

22.5.5.1.3

λ_s - size effect modification factor

$$\lambda_s = \text{MIN} \left[\sqrt{\frac{2}{1 + \frac{d}{10}}}, 1 \right]$$

$$\lambda_s = \text{MIN} \left[\sqrt{\frac{2}{1 + \frac{(38.4 \text{ in})}{10}}}, 1 \right]$$

$$\lambda_s = 0.64282$$

22.5.5.1.1

The following variables were converted to be consistent with empirical formula $f'_{ck} = 2.5 \text{ ksi} \rightarrow 2500 \text{ psi}$,
 $V_{c,max}$ - Max shear strength of concrete

$$V_{c,max} = 5 \lambda_s \sqrt{f'_{ck}} b_w d$$

$$V_{c,max} = 5 \times (0.64282) \times \sqrt{(2500 \text{ psi})} \times (48 \text{ in}) \times (38.4 \text{ in})$$

$$V_{c,max} = 296.21 \text{ kip}$$

22.5.5.1.1(a)

The following variables were converted to be consistent with empirical formula $f'_{ck} = 2.5 \text{ ksi} \rightarrow 2500 \text{ psi}$, $P = 10.776 \text{ kip} \rightarrow 10776 \text{ lbf}$,
 $V_{c,a}$ - Shear strength of concrete (a)

$$V_{c,a} = \left[2 \lambda_s \sqrt{f'_{ck}} + \frac{P}{6 A_g} \right] b_w d$$

$$V_{c,a} = \left[2 \times (0.64282) \times \sqrt{(2500 \text{ psi})} + \frac{(10776 \text{ lbf})}{6 \times (2304 \text{ in}^2)} \right] \times (48 \text{ in}) \times (38.4 \text{ in})$$

$$V_{c,a} = 119.92 \text{ kip}$$

22.5.5.1.2

The following variables were converted to be consistent with empirical formula $f'_{ck} = 2.5 \text{ ksi} \rightarrow 2500 \text{ psi}$,
 $V_{c,b}$ - Shear strength of concrete (b)

$$V_{c,b} = \left[2 \lambda_s \sqrt{f'_{ck}} + (0.05 f'_{ck}) \right] b_w d$$

$$V_{c,b} = \left[2 \times (0.64282) \times \sqrt{(2500 \text{ psi})} + (0.05 \times (2500 \text{ psi})) \right] \times (48 \text{ in}) \times (38.4 \text{ in})$$

$$V_{c,b} = 348.89 \text{ kip}$$

V_c - Governing shear strength of concrete

$$V_c = \text{Min}[V_{c,max}, V_{c,a}, V_{c,b}]$$

$$V_c = \text{Min}[(296.21 \text{ kip}), (119.92 \text{ kip}), (348.89 \text{ kip})]$$

$$V_c = 119.92 \text{ kip}$$

<p>22.5.1.2</p>	<p>The following variables were converted to be consistent with empirical formula $f'_{ck} = 2.5 \text{ ksi} \rightarrow 2500 \text{ psi}$.</p> <p>$V_{s,a}$ - Shear strength of steel (a)</p> $V_{s,a} = 8 \sqrt{f'_{ck}} b_w d$ $V_{s,a} = 8 \times \sqrt{(2500 \text{ psi})} \times (48 \text{ in}) \times (38.4 \text{ in})$ $V_{s,a} = 737.28 \text{ kip}$ <p>A_v - Ties rebar area,</p> $A_v = \frac{\pi d_{ties}^2}{4}$ $A_v = \frac{\pi \times (0.375 \text{ in})^2}{4}$ $A_v = 0.11045 \text{ in}^2$ <p>22.5.8.5.3 $V_{s,b}$ - Shear strength of steel (b)</p> $V_{s,b} = \frac{2 A_v f_{yt} d}{s_{ties}}$ $V_{s,b} = \frac{2 \times (0.11045 \text{ in}^2) \times (60 \text{ ksi}) \times (38.4 \text{ in})}{(10 \text{ in})}$ $V_{s,b} = 50.894 \text{ kip}$ <p>V_s - Governing shear strength of steel</p> $V_s = \text{MIN}[V_{s,a}, V_{s,b}]$ $V_s = \text{MIN}[(737.28 \text{ kip}), (50.894 \text{ kip})]$ $V_s = 50.894 \text{ kip}$ <p>22.5.1.1 ϕV_n - Allowable shear strength</p> $\phi V_n = \phi (V_c + V_s)$ $\phi V_n = (0.65) \times ((119.92 \text{ kip}) + (50.894 \text{ kip}))$ $\phi V_n = 111.03 \text{ kip}$ <p>Considering x-direction:</p> <p>$V_{max} = 16.444 \text{ kip}$ - Maximum shear force in the x-direction, Ratio - Capacity</p> $\text{Ratio} = \frac{V_{max}}{\phi V_n}$ $\text{Ratio} = \frac{(16.444 \text{ kip})}{(111.03 \text{ kip})}$ $\text{Ratio} = 0.1481$ <p>Considering z-direction:</p> <p>$V_{max} = 0.23453 \text{ kip}$ - Maximum shear force in the z-direction, Ratio - Capacity</p> $\text{Ratio} = \frac{V_{max}}{\phi V_n}$ $\text{Ratio} = \frac{(0.23453 \text{ kip})}{(111.03 \text{ kip})}$ $\text{Ratio} = 0.0021123$	<p>Status: PASS Ratio: 0.150</p> <p>Status: PASS Ratio: 0.000</p>
	<p>Flexural Strength (ACI 318-19, LRFD)</p> <p>S_m - Section modulus</p> $S_m = \frac{b D^2}{6}$ $S_m = \frac{(48 \text{ in}) \times (48 \text{ in})^2}{6}$ $S_m = 18432 \text{ in}^3$	

<p>14.5.2.1b</p>	<p>$\lambda = 1$ - Concrete modification factor (Normal concrete), Allowable flexural strength: M_n shall be the lesser of: $\phi M_{n,1}$</p> $\phi M_{n,1} = \phi \times 5 \times \lambda \times \sqrt{f'_c} \times S_m$ $\phi M_{n,1} = 0.65 \times 5 \times 1 \times \sqrt{2.5 \text{ksi}} \times 18432.001 \text{in}^3$ $\phi M_{n,1} = 249.600 \text{kipft}$ <p>$\phi M_{n,2}$</p> $\phi M_{n,2} = \phi \times 0.85 \times f'_c \times S_m$ $\phi M_{n,2} = (0.65) \times 0.85 \times (2.5 \text{ksi}) \times (18432 \text{in}^3)$ $\phi M_{n,2} = 2121.6 \text{kipft}$ <p>Therefore, ϕM_n - Allowable flexural strength,</p> $\phi M_n = \text{MIN}[\phi M_{n,1}, \phi M_{n,2}]$ $\phi M_n = \text{MIN}[(249.6 \text{kipft}), (2121.6 \text{kipft})]$ $\phi M_n = 249.6 \text{kipft}$ <p>Considering x-direction: $M_{max} = 73.706 \text{kipft}$ - Maximum moment in the x-direction, Ratio - Capacity</p> $\text{Ratio} = \frac{M_{max}}{\phi M_n}$ $\text{Ratio} = \frac{(73.706 \text{kipft})}{(249.6 \text{kipft})}$ $\text{Ratio} = 0.2953$	<p>Status: PASS Ratio: 0.300</p>
	<p>Considering z-direction: $M_{max} = 0.9978 \text{kipft}$ - Maximum moment in the z-direction, Ratio - Capacity</p> $\text{Ratio} = \frac{M_{max}}{\phi M_n}$ $\text{Ratio} = \frac{(0.9978 \text{kipft})}{(249.6 \text{kipft})}$ $\text{Ratio} = 0.0039976$	<p>Status: PASS Ratio: 0.000</p>