

Your Project Calculations

Project Name: JAM72-D30-545MB 20-panel

S3D Model Link:

https://platform.skyciv.com/structural?preload_name=JAM72-D30-545MB%2020-panel&preload_path=Shared%20Enterprise%20Folder/MT_Solar_Projects/8_2023

Public Model Link:

https://platform.skyciv.com/structural-viewer?project_id=gT1ueAmEj6wCfpqUMP6leSLdYnFi3PWeyNKMNAOfp0jRKLqOnMITmjilZNvvCziB



Array Specification

Product:	Beam
Unique ID:	2P-22.5-6TOP-HD-45-L-4Hx5W-5J3E
Duty Classification:	HD
Module Width:	44.72 in
Module Length:	89.76in
Number of Rows:	4
Number of Columns:	5
Total Number of Modules:	20
Desired Tilt Angle:	35
Front Edge Clearance:	5
Total Array Height at Tilt:	13.60 ft
Total Frame Length:	37.50 ft
Frame Weight:	1953 lbs
Array Dimensions N/S:	15.07 ft
Array Dimensions E/W:	37.82 ft
Rail Length:	180.88 in
Rail Spacing:	3.74 ft
Rail Check:	Not Checked

Support Specifications

Pole Size:	6in Pipe Sch 40
Pole Length above Grade:	9.32 ft
Number of Poles:	2
Pole Spacing:	22.5 ft

Foundation Specifications

Foundation Type:	Square
Foundation Dimensions:	48 x 48 in
Foundation Depth (below grade):	Pile 1: 5.75 ft Pile 2: 5.75 ft
Foundation Volume:	6.815 y ³
Foundation Result:	PASSED
Mount Twist:	0.672477 kip

Site Info

Risk Category:	I
Exposure:	B
Soil Classification:	sand
Site Location:	25519 Wind Song Valley Rd, Custer, SD 57730, USA
Wind Speed:	105 mph
Snow Load:	30 psf
Design Uplift Pressure:	Multiple pressures
Design Downforce Pressure:	Multiple pressures
Design Snow Pressure:	0.011546 ksf



Design Disclaimer

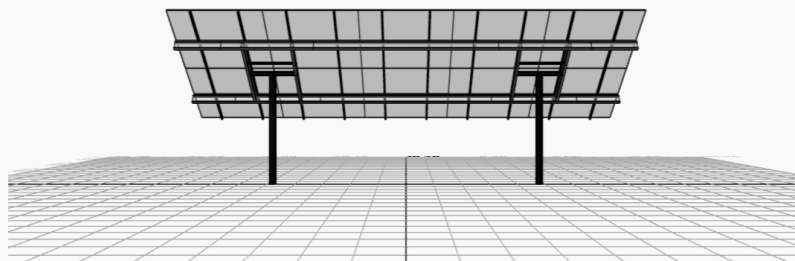
This software should be used for preliminary designs and should not be used as a final design unless reviewed, verified and designed by a qualified structural engineer.

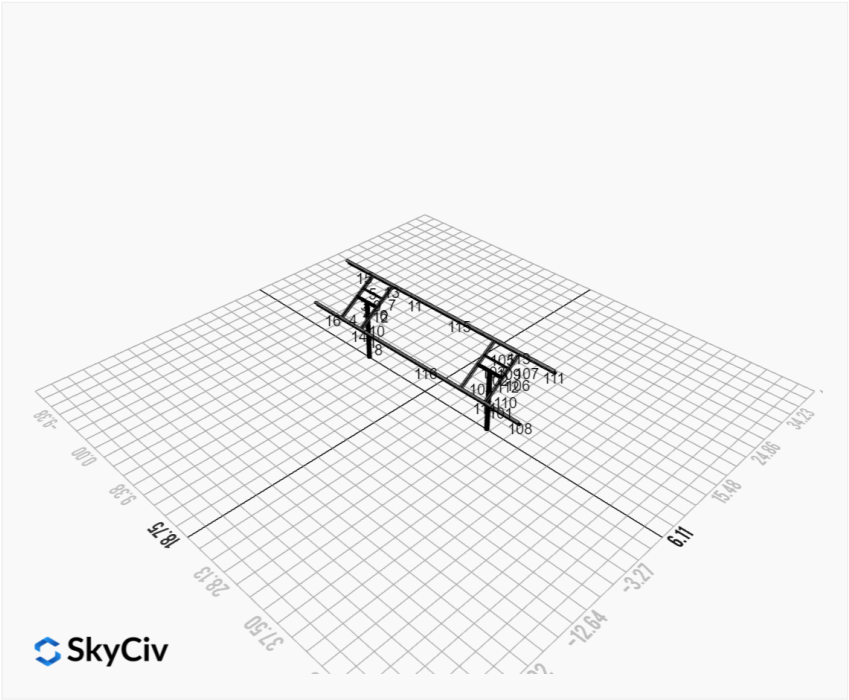
AutoDesigner Input

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  "module_length": 89.76,
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  "tilt_angle": 35,
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  "foundation_type": "Square",
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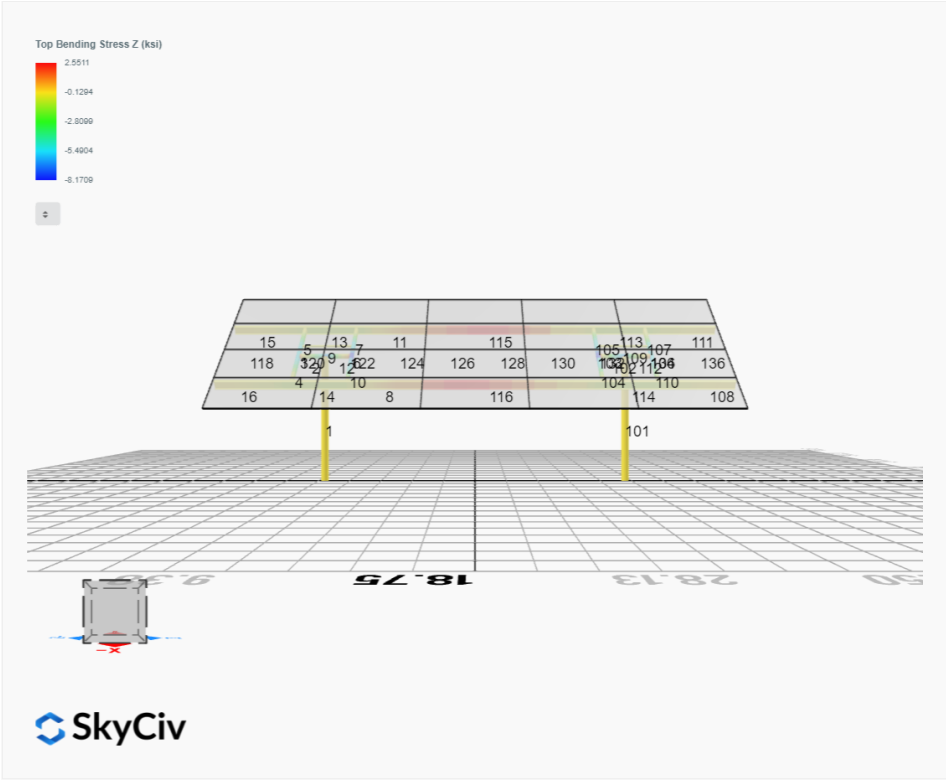
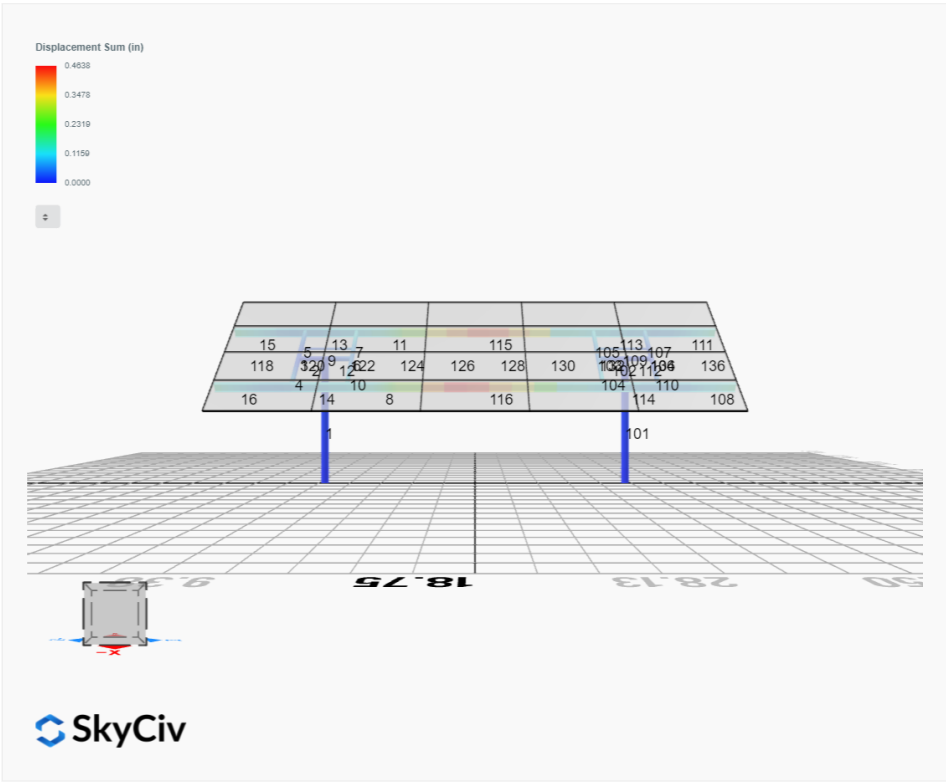
Design Notes:

- AISC Deflection checks are set to L/1 due to structure design intent
- Foundation Design and Sizing is approximate only

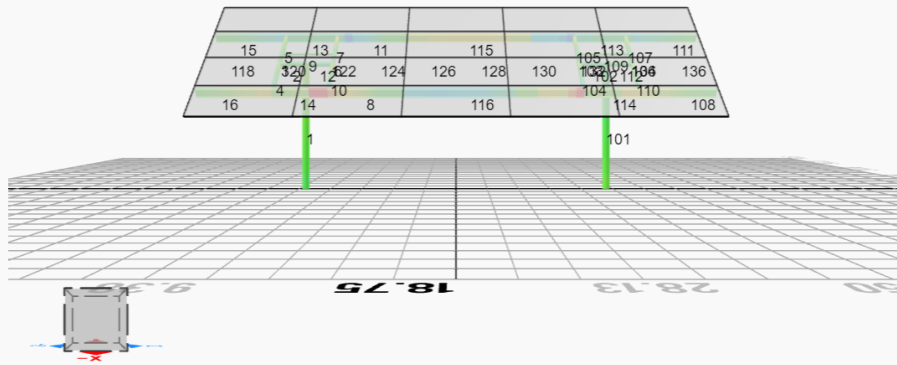




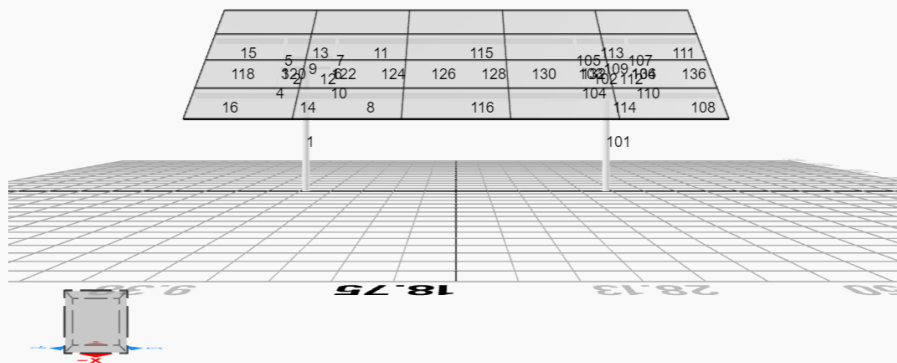
FEM Results (Envelope Worst Case for each member)



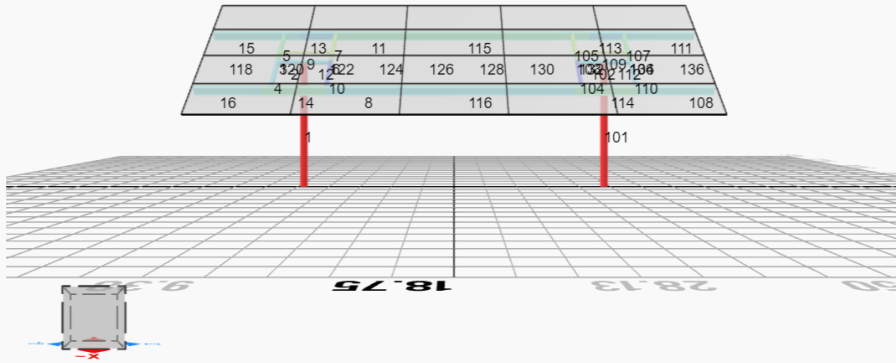
Top Bending Stress Y (ksi)



Shear Stress Y (ksi)



Axial Stress (ksi)



Reaction Forces for Foundation 1 (Node ID#1), (kip, kip-ft)

ASD Load Combination Results

Name	Fx	Fy	Fz	Mx	My	Mz
ULS: 1. D	0.0000	2.0566	0.0834	0.2383	-0.0700	0.0258
ULS: 2. D + L	0.0000	2.0566	0.0834	0.2383	-0.0700	0.0258
ULS: 3. D + (S or Lr or R)	0.0000	4.7297	0.2175	0.6220	-0.1828	0.0349
ULS: 3. D + (S or Lr or R)	0.0000	2.0566	0.0834	0.2383	-0.0700	0.0258
ULS: 4. D + 0.75L + 0.75(S or Lr or R)	0.0000	4.0614	0.1840	0.5260	-0.1546	0.0326
ULS: 4. D + 0.75L + 0.75(S or Lr or R)	0.0000	2.0566	0.0834	0.2383	-0.0700	0.0258
ULS: 5b. D + 0.7E	0.0000	2.0566	0.0834	0.2383	-0.0700	0.0258
ULS: 6b. D + 0.75L + 0.75(0.7)E + 0.75S	0.0000	4.0614	0.1840	0.5260	-0.1546	0.0326
ULS: 8. 0.6D + 0.7E	0.0000	1.2340	0.0500	0.1430	-0.0420	0.0155
ULS: 5a. D + 0.6W_Wind downforce Case A only	-2.0235	4.9465	0.2687	0.7544	-0.3895	19.5842
ULS: 5a. D + 0.6W_Wind downforce Case B only	-2.0235	4.9465	0.2687	0.7544	-0.3895	19.5842
ULS: 5a. D + 0.6W_Wind uplift Case A only	1.7073	-0.3817	-0.0722	-0.1935	0.1989	-15.5688
ULS: 5a. D + 0.6W_Wind uplift Case B only	1.4228	0.0247	-0.0473	-0.1245	0.1558	-18.6546
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind downforce Case A only	-1.5176	6.2288	0.3230	0.9131	-0.3942	14.7014
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind downforce Case B only	-1.5176	6.2288	0.3230	0.9131	-0.3942	14.7014
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind uplift Case A only	1.2805	2.2327	0.0673	0.2022	0.0471	-11.6633
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind uplift Case B only	1.0671	2.5375	0.0860	0.2540	0.0148	-13.9777
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind downforce Case A only	-1.5176	4.2240	0.2224	0.6253	-0.3097	14.6946
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind downforce Case B only	-1.5176	4.2240	0.2224	0.6253	-0.3097	14.6946
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind uplift Case A only	1.2805	0.2278	-0.0333	-0.0855	0.1317	-11.6701
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind uplift Case B only	1.0671	0.5326	-0.0146	-0.0338	0.0994	-13.9845
ULS: 7. 0.6D + 0.6W_Wind downforce Case A only	-2.0235	4.1238	0.2353	0.6591	-0.3615	19.5738
ULS: 7. 0.6D + 0.6W_Wind downforce Case B only	-2.0235	4.1238	0.2353	0.6591	-0.3615	19.5738
ULS: 7. 0.6D + 0.6W_Wind uplift Case A only	1.7073	-1.2044	-0.1056	-0.2888	0.2270	-15.5791
ULS: 7. 0.6D + 0.6W_Wind uplift Case B only	1.4228	-0.7980	-0.0807	-0.2198	0.1839	-18.6649

Worst Case Reactions LRFD

These calculations are taken directly from the FEA via SkyCiv and are used in the Concrete Checks of the Foundation Module.
Note: Worst case values are assumed as downforce wind load cases.

Result	Value (kip, kip-ft)
Axial	9.1531
Shear X	-3.3725
Shear Z	0.4763
Moment X	1.3415
Moment Y (Twist)	0.6722
Moment Z	33.3521

Worst Case Reactions ASD

These results are taken from the worst case values in the above table and are used in the Soil Checks in the Foundation Module.
Note: Worst case values are assumed as downforce wind load cases.

Result	Value (kip, kip-ft)
Axial	6.2288
Shear X	-2.0235
Shear Z	0.3230
Moment X	0.9131
Moment Y (Twist)	0.3942
Moment Z	19.5842

Reaction Forces for Foundation 2 (Node ID#101), (kip, kip-ft)

ASD Load Combination Results

Name	Fx	Fy	Fz	Mx	My	Mz
ULS: 1. D	-0.0000	2.0566	-0.0834	-0.2383	0.0701	0.0258
ULS: 2. D + L	-0.0000	2.0566	-0.0834	-0.2383	0.0701	0.0258
ULS: 3. D + (S or Lr or R)	-0.0000	4.7297	-0.2175	-0.6221	0.1829	0.0350
ULS: 3. D + (S or Lr or R)	-0.0000	2.0566	-0.0834	-0.2383	0.0701	0.0258
ULS: 4. D + 0.75L + 0.75(S or Lr or R)	-0.0000	4.0614	-0.1840	-0.5261	0.1547	0.0327
ULS: 4. D + 0.75L + 0.75(S or Lr or R)	-0.0000	2.0566	-0.0834	-0.2383	0.0701	0.0258
ULS: 5b. D + 0.7E	-0.0000	2.0566	-0.0834	-0.2383	0.0701	0.0258

Name	Fx	Fy	Fz	Mx	My	Mz
ULS: 6b. D + 0.75L + 0.75(0.7)E + 0.75S	-0.0000	4.0614	-0.1840	-0.5261	0.1547	0.0327
ULS: 8. 0.6D + 0.7E	-0.0000	1.2340	-0.0500	-0.1430	0.0420	0.0155
ULS: 5a. D + 0.6W_Wind downforce Case A only	-2.0235	4.9465	-0.2687	-0.7544	0.3896	19.5842
ULS: 5a. D + 0.6W_Wind downforce Case B only	-2.0235	4.9465	-0.2687	-0.7544	0.3896	19.5842
ULS: 5a. D + 0.6W_Wind uplift Case A only	1.7073	-0.3817	0.0722	0.1935	-0.1989	-15.5687
ULS: 5a. D + 0.6W_Wind uplift Case B only	1.4228	0.0247	0.0473	0.1245	-0.1558	-18.6546
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind downforce Case A only	-1.5176	6.2288	-0.3230	-0.9132	0.3943	14.7014
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind downforce Case B only	-1.5176	6.2288	-0.3230	-0.9132	0.3943	14.7014
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind uplift Case A only	1.2805	2.2327	-0.0673	-0.2023	-0.0470	-11.6632
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind uplift Case B only	1.0671	2.5375	-0.0860	-0.2541	-0.0147	-13.9776
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind downforce Case A only	-1.5176	4.2240	-0.2224	-0.6254	0.3097	14.6946
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind downforce Case B only	-1.5176	4.2240	-0.2224	-0.6254	0.3097	14.6946
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind uplift Case A only	1.2805	0.2278	0.0333	0.0855	-0.1317	-11.6701
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind uplift Case B only	1.0671	0.5326	0.0146	0.0338	-0.0993	-13.9845
ULS: 7. 0.6D + 0.6W_Wind downforce Case A only	-2.0235	4.1238	-0.2353	-0.6591	0.3615	19.5739
ULS: 7. 0.6D + 0.6W_Wind downforce Case B only	-2.0235	4.1238	-0.2353	-0.6591	0.3615	19.5739
ULS: 7. 0.6D + 0.6W_Wind uplift Case A only	1.7073	-1.2044	0.1056	0.2888	-0.2269	-15.5791
ULS: 7. 0.6D + 0.6W_Wind uplift Case B only	1.4228	-0.7980	0.0807	0.2198	-0.1838	-18.6649

Worst Case Reactions LRFD

These calculations are taken directly from the FEA via SkyCiv and are used in the Concrete Checks of the Foundation Module.
Note: Worst case values are assumed as downforce wind load cases.

Result	Value (kip, kip-ft)
Axial	9.1531
Shear X	-3.3725
Shear Z	-0.4763
Moment X	-1.3420
Moment Y (Twist)	0.6725
Moment Z	33.3533

Worst Case Reactions ASD

These results are taken from the worst case values in the above table and are used in the Soil Checks in the Foundation Module.
Note: Worst case values are assumed as downforce wind load cases.

Result	Value (kip, kip-ft)
Axial	6.2288
Shear X	-2.0235
Shear Z	-0.3230
Moment X	-0.9132
Moment Y (Twist)	0.3943
Moment Z	19.5842

Project Details

Design Code: AISC 360-16 LRFD
 Provision: LRFD
 Country: United States

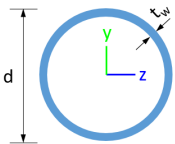
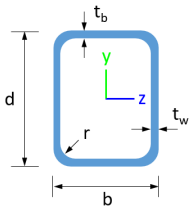
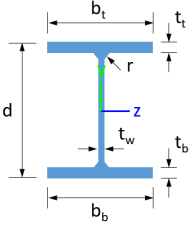
User Name: sales@mtsolar.us
 Project Name: JAM72-D30-545MB 20-panel
 Unit System: imperial



Design Input Information

Design Factors			
Φ_t	Φ_c	Φ_b	Φ_v
0.9	0.9	0.9	0.9

Design Materials			
ID	E (ksi)	F_y (ksi)	F_u (ksi)
1	29000	50	65

Section Dimensions								
								
ID	Name	d (in)	t_w (in)					
2	2in Pipe Sch 80	2.38	0.22					
5	4in Pipe Sch 80	4.50	0.34					
7	6in Pipe Sch 40	6.63	0.28					
								
ID	Name	d (in)	b (in)	t_w (in)	t_b (in)	r (in)		
16	HSS5x3x16	5.00	3.00	0.17	0.17	0.17		
								
ID	Name	d (in)	t_w (in)	b_t (in)	b_b (in)	t_t (in)	t_b (in)	r (in)
19	W8x10	7.89	0.17	3.94	3.94	0.20	0.20	0.30

Section Properties								
ID	Name	A (in ²)	J (in ⁴)	I_{yp} (in ⁴)	I_{zp} (in ⁴)	I_w (in ⁶)	S_{yp} (in ³)	S_{zp} (in ³)
2	2in Pipe Sch 80	1.48	1.74	0.87	0.87	0.00	1.02	1.02
5	4in Pipe Sch 80	4.41	19.22	9.61	9.61	0.00	5.85	5.85

7	6in Pipe Sch 40	5.58	56.28	28.14	28.14	0.00	11.28	11.28
16	HSS5x3x3/16	2.58	8.64	3.85	8.53	92.39	2.96	4.21
19	W8x10	2.96	0.04	2.09	30.80	30.90	1.66	8.87

Member Properties								
Member ID	Section ID	K _z L (ft)	K _y L (ft)	L _b (ft)	C _b	L S T	L S C	L D
1	7	19.58	19.58	9.32	-	300	200	1
2	5	1.30	1.30	2.00	-	300	200	1
3	16	0.92	0.92	1.42	1.18,1.18,1.18,1.18,1.18,1.18,1.18,1.17,1.17,1.18,1.18,1.17,1.17,1.18,1.18,1.18,1.18,1.18,1.15,1.16,1.18,1.18,1.17,1.17	300	200	1
4	16	2.44	2.44	3.75	1.69,1.68,1.69,1.67,1.68,1.69,1.67,1.67,1.65,1.69,1.67,1.67,1.66,1.82,1.67,1.67,1.68,1.67,1.67,1.67,1.62,1.70,1.67,1.67,1.66,1.53	300	200	1
5	16	1.52	1.52	2.33	1.68,1.67,1.68,1.67,1.68,1.68,1.67,1.67,1.66,1.66,1.67,1.67,1.66,1.66,1.67,1.67,1.67,1.68,1.67,1.67,1.64,1.65,1.67,1.67,1.66,1.66	300	200	1
6	16	0.92	0.92	1.42	1.19,1.19,1.19,1.18,1.19,1.19,1.18,1.18,1.17,1.18,1.18,1.18,1.18,1.18,1.18,1.19,1.19,1.18,1.18,1.16,1.17,1.18,1.18,1.18,1.18	300	200	1
7	16	1.52	1.52	2.33	1.68,1.67,1.68,1.67,1.67,1.68,1.67,1.67,1.66,1.66,1.67,1.67,1.66,1.66,1.67,1.67,1.67,1.68,1.67,1.67,1.65,1.66,1.67,1.67,1.66,1.66	300	200	1
8	19	1.33	1.33	2.05	1.56,1.56,1.56,1.56,1.56,1.56,1.54,1.54,1.51,2.09,1.54,1.54,1.53,1.09,1.55,1.55,1.59,1.61,1.54,1.54,1.50,1.90,1.54,1.54,1.53,1.19	300	200	1
9	2	2.60	2.60	4.00	-	300	200	1
10	16	2.44	2.44	3.75	1.68,1.68,1.68,1.67,1.68,1.68,1.67,1.67,1.66,1.69,1.67,1.67,1.66,1.12,1.67,1.67,1.68,1.67,1.67,1.67,1.63,1.70,1.67,1.67,1.66,1.62	300	200	1
11	19	1.33	1.33	2.05	1.57,1.57,1.57,1.57,1.57,1.57,1.56,1.56,1.52,1.61,1.55,1.55,1.54,1.60,1.56,1.56,1.60,1.53,1.56,1.56,1.50,1.62,1.55,1.55,1.54,1.60	300	200	1
12	5	1.30	1.30	2.00	-	300	200	1
13	19	4.88	4.00	7.50	1.11,1.11,1.11,1.11,1.11,1.11,1.11,1.11,1.13,1.16,1.12,1.12,1.12,1.15,1.11,1.11,1.10,1.06,1.11,1.11,1.14,1.17,1.12,1.12,1.12,1.15	300	200	1
14	19	4.88	4.00	7.50	1.10,1.10,1.10,1.10,1.10,1.10,1.11,1.11,1.13,1.37,1.11,1.11,1.12,2.06,1.11,1.11,1.09,1.12,1.11,1.11,1.13,1.20,1.11,1.11,1.12,1.18	300	200	1
15	19	7.88	7.88	3.75	2.33,2.33	300	200	1
16	19	7.88	7.88	3.75	2.33,2.33	300	200	1
101	7	19.58	19.58	9.32	-	300	200	1
102	5	1.30	1.30	2.00	-	300	200	1
103	16	0.92	0.92	1.42	1.19,1.19,1.19,1.18,1.19,1.19,1.18,1.18,1.17,1.18,1.18,1.18,1.18,1.18,1.18,1.19,1.19,1.18,1.18,1.16,1.17,1.18,1.18,1.18,1.18	300	200	1
104	16	2.44	2.44	3.75	1.68,1.68,1.68,1.67,1.68,1.68,1.67,1.67,1.66,1.69,1.67,1.67,1.66,1.13,1.67,1.67,1.68,1.67,1.67,1.67,1.63,1.70,1.67,1.67,1.66,1.62	300	200	1
105	16	1.52	1.52	2.33	1.68,1.67,1.68,1.67,1.67,1.68,1.67,1.67,1.66,1.66,1.67,1.67,1.66,1.66,1.67,1.67,1.67,1.68,1.67,1.67,1.65,1.66,1.67,1.67,1.66,1.66	300	200	1
106	16	0.92	0.92	1.42	1.18,1.18,1.18,1.18,1.18,1.18,1.18,1.18,1.17,1.17,1.18,1.18,1.17,1.17,1.18,1.18,1.18,1.18,1.18,1.15,1.16,1.18,1.18,1.17,1.17	300	200	1
107	16	1.52	1.52	2.33	1.68,1.67,1.68,1.67,1.68,1.68,1.67,1.67,1.66,1.66,1.67,1.67,1.66,1.66,1.67,1.67,1.67,1.68,1.67,1.67,1.67,1.64,1.65,1.67,1.67,1.66,1.66	300	200	1

				5	7.07,7.08,7.09,7.10,7.11,7.12,7.13,7.14,7.15,7.16,7.17,7.18,7.19,7.20,7.21,7.22,7.23,7.24,7.25,7.26,7.27,7.28,7.29,7.30,7.31,7.32,7.33,7.34,7.35,7.36,7.37,7.38,7.39,7.40,7.41,7.42,7.43,7.44,7.45,7.46,7.47,7.48,7.49,7.50,7.51,7.52,7.53,7.54,7.55,7.56,7.57,7.58,7.59,7.60,7.61,7.62,7.63,7.64,7.65,7.66,7.67,7.68,7.69,7.70,7.71,7.72,7.73,7.74,7.75,7.76,7.77,7.78,7.79,7.80,7.81,7.82,7.83,7.84,7.85,7.86,7.87,7.88,7.89,7.90,7.91,7.92,7.93,7.94,7.95,7.96,7.97,7.98,7.99,8.00,8.01,8.02,8.03,8.04,8.05,8.06,8.07,8.08,8.09,8.10,8.11,8.12,8.13,8.14,8.15,8.16,8.17,8.18,8.19,8.20,8.21,8.22,8.23,8.24,8.25,8.26,8.27,8.28,8.29,8.30,8.31,8.32,8.33,8.34,8.35,8.36,8.37,8.38,8.39,8.40,8.41,8.42,8.43,8.44,8.45,8.46,8.47,8.48,8.49,8.50,8.51,8.52,8.53,8.54,8.55,8.56,8.57,8.58,8.59,8.60,8.61,8.62,8.63,8.64,8.65,8.66,8.67,8.68,8.69,8.70,8.71,8.72,8.73,8.74,8.75,8.76,8.77,8.78,8.79,8.80,8.81,8.82,8.83,8.84,8.85,8.86,8.87,8.88,8.89,8.90,8.91,8.92,8.93,8.94,8.95,8.96,8.97,8.98,8.99,9.00,9.01,9.02,9.03,9.04,9.05,9.06,9.07,9.08,9.09,9.10,9.11,9.12,9.13,9.14,9.15,9.16,9.17,9.18,9.19,9.20,9.21,9.22,9.23,9.24,9.25,9.26,9.27,9.28,9.29,9.30,9.31,9.32,9.33,9.34,9.35,9.36,9.37,9.38,9.39,9.40,9.41,9.42,9.43,9.44,9.45,9.46,9.47,9.48,9.49,9.50,9.51,9.52,9.53,9.54,9.55,9.56,9.57,9.58,9.59,9.60,9.61,9.62,9.63,9.64,9.65,9.66,9.67,9.68,9.69,9.70,9.71,9.72,9.73,9.74,9.75,9.76,9.77,9.78,9.79,9.80,9.81,9.82,9.83,9.84,9.85,9.86,9.87,9.88,9.89,9.90,9.91,9.92,9.93,9.94,9.95,9.96,9.97,9.98,9.99,10.00,10.01,10.02,10.03,10.04,10.05,10.06,10.07,10.08,10.09,10.10,10.11,10.12,10.13,10.14,10.15,10.16,10.17,10.18,10.19,10.20,10.21,10.22,10.23,10.24,10.25,10.26,10.27,10.28,10.29,10.30,10.31,10.32,10.33,10.34,10.35,10.36,10.37,10.38,10.39,10.40,10.41,10.42,10.43,10.44,10.45,10.46,10.47,10.48,10.49,10.50,10.51,10.52,10.53,10.54,10.55,10.56,10.57,10.58,10.59,10.60,10.61,10.62,10.63,10.64,10.65,10.66,10.67,10.68,10.69,10.70,10.71,10.72,10.73,10.74,10.75,10.76,10.77,10.78,10.79,10.80,10.81,10.82,10.83,10.84,10.85,10.86,10.87,10.88,10.89,10.90,10.91,10.92,10.93,10.94,10.95,10.96,10.97,10.98,10.99,11.00,11.01,11.02,11.03,11.04,11.05,11.06,11.07,11.08,11.09,11.10,11.11,11.12,11.13,11.14,11.15,11.16,11.17,11.18,11.19,11.20,11.21,11.22,11.23,11.24,11.25,11.26,11.27,11.28,11.29,11.30,11.31,11.32,11.33,11.34,11.35,11.36,11.37,11.38,11.39,11.40,11.41,11.42,11.43,11.44,11.45,11.46,11.47,11.48,11.49,11.50,11.51,11.52,11.53,11.54,11.55,11.56,11.57,11.58,11.59,11.60,11.61,11.62,11.63,11.64,11.65,11.66,11.67,11.68,11.69,11.70,11.71,11.72,11.73,11.74,11.75,11.76,11.77,11.78,11.79,11.80,11.81,11.82,11.83,11.84,11.85,11.86,11.87,11.88,11.89,11.90,11.91,11.92,11.93,11.94,11.95,11.96,11.97,11.98,11.99,12.00,12.01,12.02,12.03,12.04,12.05,12.06,12.07,12.08,12.09,12.10,12.11,12.12,12.13,12.14,12.15,12.16,12.17,12.18,12.19,12.20,12.21,12.22,12.23,12.24,12.25,12.26,12.27,12.28,12.29,12.30,12.31,12.32,12.33,12.34,12.35,12.36,12.37,12.38,12.39,12.40,12.41,12.42,12.43,12.44,12.45,12.46,12.47,12.48,12.49,12.50,12.51,12.52,12.53,12.54,12.55,12.56,12.57,12.58,12.59,12.60,12.61,12.62,12.63,12.64,12.65,12.66,12.67,12.68,12.69,12.70,12.71,12.72,12.73,12.74,12.75,12.76,12.77,12.78,12.79,12.80,12.81,12.82,12.83,12.84,12.85,12.86,12.87,12.88,12.89,12.90,12.91,12.92,12.93,12.94,12.95,12.96,12.97,12.98,12.99,13.00,13.01,13.02,13.03,13.04,13.05,13.06,13.07,13.08,13.09,13.10,13.11,13.12,13.13,13.14,13.15,13.16,13.17,13.18,13.19,13.20,13.21,13.22,13.23,13.24,13.25,13.26,13.27,13.28,13.29,13.30,13.31,13.32,13.33,13.34,13.35,13.36,13.37,13.38,13.39,13.40,13.41,13.42,13.43,13.44,13.45,13.46,13.47,13.48,13.49,13.50,13.51,13.52,13.53,13.54,13.55,13.56,13.57,13.58,13.59,13.60,13.61,13.62,13.63,13.64,13.65,13.66,13.67,13.68,13.69,13.70,13.71,13.72,13.73,13.74,13.75,13.76,13.77,13.78,13.79,13.80,13.81,13.82,13.83,13.84,13.85,13.86,13.87,13.88,13.89,13.90,13.91,13.92,13.93,13.94,13.95,13.96,13.97,13.98,13.99,14.00,14.01,14.02,14.03,14.04,14.05,14.06,14.07,14.08,14.09,14.10,14.11,14.12,14.13,14.14,14.15,14.16,14.17,14.18,14.19,14.20,14.21,14.22,14.23,14.24,14.25,14.26,14.27,14.28,14.29,14.30,14.31,14.32,
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Member Design Capacity

Member ID	$\Phi_t P_n$ (kip)	$\Phi_c P_n$ (kip)	$\Phi_b M_{zn}$ (k-ft)	$\Phi_b M_{yn}$ (k-ft)	$\Phi_v V_{yn}$ (kip)	$\Phi_v V_{zn}$ (kip)
1	251.16	112.81	42.30	42.30	75.35	75.35
2	198.33	196.72	21.95	21.95	59.50	59.50
3	116.10	115.41	15.79	11.10	42.08	23.28
4	116.10	111.33	15.79	11.10	42.08	23.28
5	116.10	114.23	15.79	11.10	42.08	23.28
6	116.10	115.41	15.79	11.10	42.08	23.28
7	116.10	114.23	15.79	11.10	42.08	23.28
8	133.20	126.01	32.87	6.12	40.24	43.62
9	66.48	58.89	3.82	3.82	19.94	19.94
10	116.10	111.33	15.79	11.10	42.08	23.28
11	133.20	126.01	32.87	6.12	40.24	43.62
12	198.33	196.72	21.95	21.95	59.50	59.50
13	133.20	104.94	24.29	6.12	40.24	43.62
14	133.20	104.94	24.98	6.12	40.24	43.62
15	133.20	52.83	32.87	6.12	40.24	43.62
16	133.20	52.83	32.87	6.12	40.24	43.62
101	251.16	112.81	42.30	42.30	75.35	75.35
102	198.33	196.72	21.95	21.95	59.50	59.50
103	116.10	115.41	15.79	11.10	42.08	23.28
104	116.10	111.33	15.79	11.10	42.08	23.28
105	116.10	114.23	15.79	11.10	42.08	23.28
106	116.10	115.41	15.79	11.10	42.08	23.28
107	116.10	114.23	15.79	11.10	42.08	23.28
108	133.20	52.83	32.87	6.12	40.24	43.62
109	66.48	58.89	3.82	3.82	19.94	19.94
110	116.10	111.33	15.79	11.10	42.08	23.28
111	133.20	52.83	32.87	6.12	40.24	43.62
112	198.33	196.72	21.95	21.95	59.50	59.50
113	133.20	104.94	24.29	6.12	40.24	43.62
114	133.20	104.94	24.98	6.12	40.24	43.62

115	133.20	46.28	11.92	6.12	40.24	43.62
116	133.20	46.28	11.59	6.12	40.24	43.62

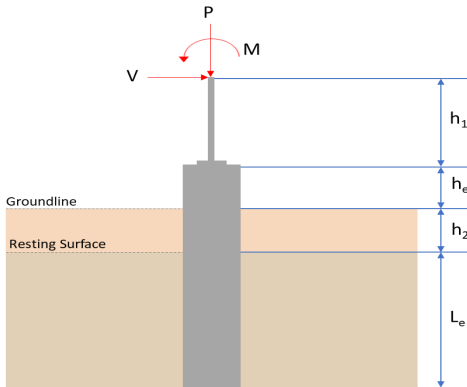
Design Ratio

Member ID	P	M _z	M _y	V _y	V _z	(P,M _z ,M _y)	Worst LC	KL/r	δ	Status
1	0.081	0.788	0.073	0.045	0.006	0.858	#13	0.523	Not Required	Pass
2	0.004	0.262	0.142	0.062	0.028	0.396	#13	0.035	Not Required	Pass
3	0.007	0.461	0.034	0.045	0.009	0.464	#13	0.045	Not Required	Pass
4	0.006	0.448	0.120	0.045	0.027	0.517	#13	0.080	Not Required	Pass
5	0.006	0.286	0.101	0.046	0.026	0.297	#13	0.074	Not Required	Pass
6	0.010	0.591	0.083	0.060	0.016	0.645	#13	0.045	Not Required	Pass
7	0.010	0.366	0.195	0.059	0.050	0.397	#13	0.074	Not Required	Pass
8	0.002	0.097	0.200	0.042	0.017	0.204	#21	0.095	Not Required	Pass
9	0.013	0.053	0.074	0.002	0.004	0.120	#21	0.204	Not Required	Pass
10	0.011	0.577	0.176	0.058	0.036	0.638	#21	0.080	Not Required	Pass
11	0.005	0.098	0.208	0.043	0.017	0.213	#21	0.095	Not Required	Pass
12	0.003	0.401	0.173	0.088	0.030	0.566	#13	0.053	Not Required	Pass
13	0.005	0.161	0.439	0.053	0.020	0.562	#21	0.286	Not Required	Pass
14	0.006	0.161	0.429	0.052	0.020	0.548	#21	0.190	Not Required	Pass
15	0.000	0.050	0.110	0.022	0.008	0.157	#21	Not Required	Not Required	Pass
16	0.000	0.049	0.110	0.021	0.008	0.156	#21	Not Required	Not Required	Pass
101	0.081	0.789	0.073	0.045	0.006	0.858	#13	0.523	Not Required	Pass
102	0.003	0.401	0.173	0.088	0.030	0.566	#13	0.053	Not Required	Pass
103	0.010	0.591	0.083	0.060	0.016	0.645	#13	0.045	Not Required	Pass
104	0.011	0.577	0.176	0.058	0.036	0.638	#21	0.080	Not Required	Pass
105	0.010	0.366	0.195	0.059	0.050	0.397	#13	0.074	Not Required	Pass
106	0.007	0.461	0.034	0.045	0.009	0.464	#13	0.045	Not Required	Pass
107	0.006	0.286	0.101	0.046	0.026	0.297	#13	0.074	Not Required	Pass
108	0.000	0.049	0.110	0.021	0.008	0.156	#21	Not Required	Not Required	Pass
109	0.013	0.053	0.074	0.002	0.004	0.120	#21	0.204	Not Required	Pass
110	0.006	0.448	0.120	0.045	0.027	0.517	#13	0.080	Not Required	Pass
111	0.000	0.050	0.110	0.022	0.008	0.157	#21	Not Required	Not Required	Pass
112	0.004	0.262	0.142	0.062	0.028	0.396	#13	0.035	Not Required	Pass
113	0.005	0.161	0.438	0.053	0.020	0.562	#21	0.190	Not Required	Pass
114	0.006	0.161	0.430	0.052	0.020	0.548	#21	0.286	Not Required	Pass
115	0.012	0.552	0.238	0.043	0.017	0.757	#21	0.601	Not Required	Pass
116	0.004	0.544	0.238	0.042	0.017	0.748	#21	0.601	Not Required	Pass

Definitions

Φ_t	Safety factor for tensile
Φ_c	Safety factor for compression
Φ_b	Safety factor for flexure
Φ_v	Safety factor for shear
E	Modulus of elasticity
F _y	Specified minimum yield stress
F _u	Specified minimum tensile strength
A	Cross-sectional area
J	Torsional constant
I _{yp}	Moment of inertia about the Y axes
I _{zp}	Moment of inertia about the Z axes
I _w	Warping constant
S _{yp}	Plastic section modulus about the Y axis
S _{zp}	Plastic section modulus about the Z axis
KL	Effective length
C _n	Buckling modification factor (from all load combinations)

L_b	Length between braced points
LST	Limited slenderness for tension
LSC	Limited slenderness for compression
LD	Limited deflection
P_n	Nominal axial strength (tension/compression)
M_n	Nominal flexural strength (about Z/Y axis)
V_n	Nominal shear strength (along Z/Y axis)
P	Design ratio in case of axial force
M_z	Design ratio in case of bending about Z axis
M_y	Design ratio in case of bending about Y axis
V_y	Design ratio in case of shear along Y axis
V_z	Design ratio in case of shear along Z axis
(P, M_z , M_y)	Design ratio in case of axial force and bending action
KL/r	Design ratio in case of section slenderness
δ	Design ratio in case of member deflection
OK	Capacity is provided
NG	Capacity is not provided

REFERENCES	CALCULATIONS	RESULTS																										
	SkyCiv Foundation Design Pile Foundation Design Information : Design code : IBC 2021 (International Building Code) Unit System : Imperial																											
	Pile Input  Geometry Pile shape: rectangular b = 48 in - Pile width D = 48 in - Pile depth L = 5.75 ft - Total pile length h1 = 0 ft - Lateral load height from the top of the pile, h2 = 0 ft - Depth to resisting surface he = 0 ft - Length of pile above the ground Tabulation of Soil Parameters <table><thead><tr><th>Layer</th><th>Label</th><th>Allowable Bearing Pressure (qa) (psf)</th><th>Allowable Lateral Pressure (R) (psf/ft)</th></tr></thead><tbody><tr><td>1</td><td>Sand, silty sand, clayey sand, silty gravel & clayey gravel</td><td>2000.000</td><td>150.000</td></tr></tbody></table> Tabulation of Loads <table><thead><tr><th>Load Component</th><th>ASD</th><th>LRFD</th></tr></thead><tbody><tr><td>P (kip)</td><td>6.229</td><td>9.153</td></tr><tr><td>Vx (kip)</td><td>-2.024</td><td>-3.373</td></tr><tr><td>Vz (kip)</td><td>0.323</td><td>0.476</td></tr><tr><td>Mx (kipft)</td><td>0.913</td><td>1.341</td></tr><tr><td>Mz (kipft)</td><td>19.584</td><td>33.352</td></tr></tbody></table> Material Properties f'ck = 2.5 ksi - Concrete strength,	Layer	Label	Allowable Bearing Pressure (qa) (psf)	Allowable Lateral Pressure (R) (psf/ft)	1	Sand, silty sand, clayey sand, silty gravel & clayey gravel	2000.000	150.000	Load Component	ASD	LRFD	P (kip)	6.229	9.153	Vx (kip)	-2.024	-3.373	Vz (kip)	0.323	0.476	Mx (kipft)	0.913	1.341	Mz (kipft)	19.584	33.352	
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	Required depth to resist lateral loads (ASD) H - Point of application of the lateral load H = h1 + h2 + he H = (0 ft) + (0 ft) + (0 ft) H = 0 ft Considering x-direction: Ho - Lateral force per length of pile, Ho = Vx / (1.57 D) Ho = (-2.024 kip) / (1.57 x (48 in)) Ho = -0.32229 kip/ft Mo - Moment per length of pile, Mo = (Mz + (Vx H)) / (1.57 D)																											

	$M_o = \frac{(19.584 \text{ kipft}) + ((-2.024 \text{ kip}) \times (0 \text{ ft}))}{1.57 \times (48 \text{ in})}$ $M_o = 3.1185 \text{ kipft/ft}$ Required depth of embedment in earth: $L_x^3 - \left(14.14 \times \frac{H_o \times L_x}{R}\right) - \left(18.85 \times \frac{M_o}{R}\right) = 0$ Solving the cubic equation: $L_{e,x} = 5.2817 \text{ ft}$ - Required depth in x-direction, Considering z-direction: H_o - Lateral force per length of pile, $H_o = \frac{V_z}{1.57 b}$ $H_o = \frac{(0.323 \text{ kip})}{1.57 \times (48 \text{ in})}$ $H_o = 0.051433 \text{ kip/ft}$ M_o - Moment per length of pile, $M_o = \frac{M_x + (V_z H)}{1.57 b}$ $M_o = \frac{(0.913 \text{ kipft}) + ((0.323 \text{ kip}) \times (0 \text{ ft}))}{1.57 \times (48 \text{ in})}$ $M_o = 0.14538 \text{ kipft/ft}$ Required depth of embedment in earth: $L_z^3 - \left(14.14 \times \frac{H_o \times L_z}{R}\right) - \left(18.85 \times \frac{M_o}{R}\right) = 0$ Solving the cubic equation: $L_{e,z} = 2.7148 \text{ ft}$ - Required depth in z-direction, Minimum embedded depth required: $L_{e,req}$ - Depth of pile required, $L_{e,req} = \text{MAX}[L_{e,x}, L_{e,z}]$ $L_{e,req} = \text{MAX}[(5.2817 \text{ ft}), (2.7148 \text{ ft})]$ $L_{e,req} = 5.282 \text{ ft}$ L_e - Actual embedded length of pile, $L_e = L - h_e - h_2$ $L_e = (5.75 \text{ ft}) - (0 \text{ ft}) - (0 \text{ ft})$ $L_e = 5.75 \text{ ft}$ Ratio - Embedded depth $\text{Ratio} = \frac{L_{e,req}}{L_e}$ $\text{Ratio} = \frac{(5.282 \text{ ft})}{(5.75 \text{ ft})}$ $\text{Ratio} = 0.91861$	Status: PASS Ratio: 0.920
	End-bearing Capacity (ASD) A - Pile cross-section area $A = b D$ $A = (48 \text{ in}) \times (48 \text{ in})$ $A = 16 \text{ ft}^2$ q - End-bearing pressure $q = \frac{P_o}{A}$ $q = \frac{(6.229 \text{ kip})}{(16 \text{ ft}^2)}$	

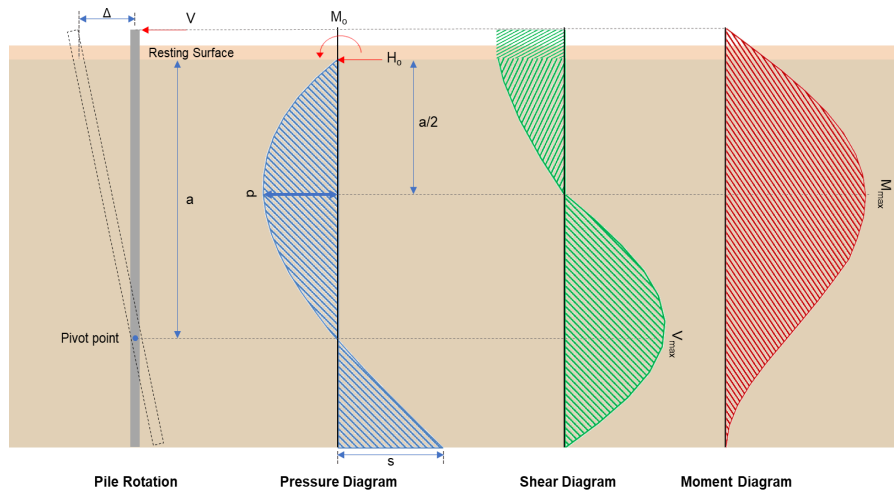
	$q = 0.00931 \text{ kip/ft}$	
	Check bearing capacity ratio: Ratio - Capacity $Ratio = \frac{q}{q_a}$ $Ratio = \frac{(0.38931 \text{ kip/ft}^2)}{(2000 \text{ psf})}$ $Ratio = 0.19466$	Status: PASS Ratio: 0.190
Czerniak	Lateral Soil Pressure (ASD): L/D - Length to least lateral dimension ratio, $L/D = \frac{L}{D}$ $L/D = \frac{(5.75 \text{ ft})}{(48 \text{ in})}$ $L/D = 1.4375$ Since $L/D \leq 10$, Pile is short. Considering x-direction: $H_o = -0.32229 \text{ kip/ft}$ - Lateral force per length of pile, $M_o = 3.1185 \text{ kipft/ft}$ - Overturning moment per length of pile, a - Distance from resting surface to pivot point, $a = \frac{(4 M_o L_e) + (3 H_o L_e^2)}{(6 M_o) + (4 H_o L_e)}$ $a = \frac{(4 \times (3.1185 \text{ kipft/ft}) \times (5.75 \text{ ft})) + (3 \times (-0.32229 \text{ kip/ft}) \times (5.75 \text{ ft})^2)}{(6 \times (3.1185 \text{ kipft/ft})) + (4 \times (-0.32229 \text{ kip/ft}) \times (5.75 \text{ ft}))}$ $a = 3.9693 \text{ ft}$ p - Earth pressure against the pile at distance $a/2$ from resting surface, $p = \frac{0.75 [(4 M_o) + (3 H_o L_e)]^2}{L_e^3 [(3 M_o) + (2 H_o L_e)]}$ $p = \frac{0.75 \times [(4 \times (3.1185 \text{ kipft/ft})) + (3 \times (-0.32229 \text{ kip/ft}) \times (5.75 \text{ ft}))]^2}{(5.75 \text{ ft})^3 \times [(3 \times (3.1185 \text{ kipft/ft})) + (2 \times (-0.32229 \text{ kip/ft}) \times (5.75 \text{ ft}))]}$ $p = 0.19198 \text{ kip/ft}^2$ s - Earth pressure against the pile at distance L_e, $s = \frac{6 [(2 M_o) + (H_o L_e)]}{L_e^2}$ $s = \frac{6 \times [(2 \times (3.1185 \text{ kipft/ft})) + ((-0.32229 \text{ kip/ft}) \times (5.75 \text{ ft}))]}{(5.75 \text{ ft})^2}$ $s = 0.79554 \text{ kip/ft}^2$ Check lateral soil pressure capacity: p_a - Allowable lateral soil pressure at depth $a/2$, $p_a = R \frac{a}{2}$ $p_a = (150 \text{ psf/ft}) \times \frac{(3.9693 \text{ ft})}{2}$ $p_a = 0.2977 \text{ kip/ft}^2$ Ratio - Lateral soil capacity $Ratio = \frac{p}{p_a}$ $Ratio = \frac{(0.19198 \text{ kip/ft}^2)}{(0.2977 \text{ kip/ft}^2)}$ $Ratio = 0.64488$ p_s - Allowable lateral soil pressure at depth L_e,	Status: PASS Ratio: 0.640

	$p_s = R L_e$ $p_s = (150 \text{ psf/ft}) \times (5.75 \text{ ft})$ $p_s = 0.8625 \text{ kip/ft}^2$ Ratio - Lateral soil capacity $Ratio = \frac{s}{p_s}$ $Ratio = \frac{(0.79554 \text{ kip/ft}^2)}{(0.8625 \text{ kip/ft}^2)}$ $Ratio = 0.92237$	Status: PASS Ratio: 0.920
	Considering z-direction: $H_o = 0.051433 \text{ kip/ft}$ - Lateral force per length of pile, $M_o = 0.14538 \text{ kipft/ft}$ - Overturning moment per length of pile, a - Distance from resting surface to pivot point, $a = \frac{(4 M_o L_e) + (3 H_o L_e^2)}{(6 M_o) + (4 H_o L_e)}$ $a = \frac{(4 \times (0.14538 \text{ kipft/ft}) \times (5.75 \text{ ft})) + (3 \times (0.051433 \text{ kip/ft}) \times (5.75 \text{ ft})^2)}{(6 \times (0.14538 \text{ kipft/ft})) + (4 \times (0.051433 \text{ kip/ft}) \times (5.75 \text{ ft}))}$ $a = 4.1091 \text{ ft}$ p - Earth pressure against the pile at distance $a/2$ from resting surface, $p = \frac{0.75 [(4 M_o) + (3 H_o L_e)]^2}{L_e^3 [(3 M_o) + (2 H_o L_e)]}$ $p = \frac{0.75 \times [(4 \times (0.14538 \text{ kipft/ft})) + (3 \times (0.051433 \text{ kip/ft}) \times (5.75 \text{ ft}))]^2}{(5.75 \text{ ft})^3 \times [(3 \times (0.14538 \text{ kipft/ft})) + (2 \times (0.051433 \text{ kip/ft}) \times (5.75 \text{ ft}))]}$ $p = 0.04762 \text{ kip/ft}^2$ s - Earth pressure against the pile at distance L_e, $s = \frac{6 [(2 M_o) + (H_o L_e)]}{L_e^2}$ $s = \frac{6 \times [(2 \times (0.14538 \text{ kipft/ft})) + ((0.051433 \text{ kip/ft}) \times (5.75 \text{ ft}))]}{(5.75 \text{ ft})^2}$ $s = 0.10644 \text{ kip/ft}^2$ Check lateral soil pressure capacity: p_a - Allowable lateral soil pressure at depth $a/2$, $p_a = R \frac{a}{2}$ $p_a = (150 \text{ psf/ft}) \times \frac{(4.1091 \text{ ft})}{2}$ $p_a = 0.30818 \text{ kip/ft}^2$ Ratio - Lateral soil capacity $Ratio = \frac{p}{p_a}$ $Ratio = \frac{(0.04762 \text{ kip/ft}^2)}{(0.30818 \text{ kip/ft}^2)}$ $Ratio = 0.15452$ p_s - Allowable lateral soil pressure at depth L_e, $p_s = R L_e$ $p_s = (150 \text{ psf/ft}) \times (5.75 \text{ ft})$ $p_s = 0.8625 \text{ kip/ft}^2$ Ratio - Lateral soil capacity $Ratio = \frac{s}{p_s}$	Status: PASS Ratio: 0.150

$$Ratio = \frac{(0.10644 \text{ kip/ft}^2)}{(0.8625 \text{ kip/ft}^2)}$$

$$Ratio = 0.1234$$

Status: **PASS**
Ratio: **0.120**



Shear force and Bending moment (x-direction, LRFD)

H_o - Lateral force per length of pile,

$$H_o = \frac{V_x}{1.57 D}$$

$$H_o = \frac{(-3.373 \text{ kip})}{1.57 \times (48 \text{ in})}$$

$$H_o = -0.5371 \text{ kip/ft}$$

M_o - Moment per length of pile,

$$M_o = \frac{M_x + (V_x H)}{1.57 D}$$

$$M_o = \frac{(33.352 \text{ kipft}) + ((-3.373 \text{ kip}) \times (0 \text{ ft}))}{1.57 \times (48 \text{ in})}$$

$$M_o = 5.3108 \text{ kipft/ft}$$

E - Distance from lateral load to resisting surface,

$$E = \frac{M_o}{H_o}$$

$$E = \frac{(5.3108 \text{ kipft/ft})}{(-0.5371 \text{ kip/ft})}$$

$$E = 9.8879 \text{ ft}$$

a - Distance from resting surface to pivot point,

$$a = \frac{(4 M_o L_e) + (3 H_o L_e^2)}{(6 M_o) + (4 H_o L_e)}$$

$$a = \frac{(4 \times (5.3108 \text{ kipft/ft}) \times (5.75 \text{ ft})) + (3 \times (-0.5371 \text{ kip/ft}) \times (5.75 \text{ ft})^2)}{(6 \times (5.3108 \text{ kipft/ft})) + (4 \times (-0.5371 \text{ kip/ft}) \times (5.75 \text{ ft}))}$$

$$a = 3.9672 \text{ ft}$$

V_{max} - Max shear force located at depth a ,

$$V_{max} = (H_o D) \left[1 - \left[3 \left(\frac{4 E}{L_e} + 3 \right) \left(\frac{a}{L_e} \right)^2 \right] + \left[4 \left(\frac{3 E}{L_e} + 2 \right) \left(\frac{a}{L_e} \right)^3 \right] \right]$$

$$V_{max} = ((-0.5371 \text{ kip/ft}) \times (48 \text{ in})) \times \left[1 - \left[3 \times \left(\frac{4 \times (9.8879 \text{ ft})}{(5.75 \text{ ft})} + 3 \right) \times \left(\frac{(3.9672 \text{ ft})}{(5.75 \text{ ft})} \right)^2 \right] + \left[4 \times \left(\frac{3 \times (9.8879 \text{ ft})}{(5.75 \text{ ft})} + 2 \right) \times \left(\frac{(3.9672 \text{ ft})}{(5.75 \text{ ft})} \right)^3 \right] \right]$$

$$V_{max} = 7.9544 \text{ kip}$$

M_{max} - Max bending moment located at depth $a/2$,

$$M_{max} = (H_o D L_e) \left[\left(\frac{E}{L_e} + \frac{a}{2 L_e} \right) - \left[\left(\frac{4 E}{L_e} + 3 \right) \left(\frac{a}{2 L_e} \right)^3 \right] + \left[\left(\frac{3 E}{L_e} + 2 \right) \left(\frac{a}{2 L_e} \right)^4 \right] \right]$$

$$M_{max} = ((-0.5371 \text{ kip/ft}) \times (48 \text{ in}) \times (5.75 \text{ ft})) \times \left[\left(\frac{(9.8879 \text{ ft})}{(5.75 \text{ ft})} + \frac{(3.9672 \text{ ft})}{2 \times (5.75 \text{ ft})} \right) - \left[\left(\frac{4 \times (9.8879 \text{ ft})}{(5.75 \text{ ft})} + 3 \right) \times \left(\frac{(3.9672 \text{ ft})}{2 \times (5.75 \text{ ft})} \right)^3 \right] + \left[\left(\frac{3 \times (9.8879 \text{ ft})}{(5.75 \text{ ft})} + 2 \right) \times \left(\frac{(3.9672 \text{ ft})}{2 \times (5.75 \text{ ft})} \right)^4 \right] \right]$$

$$M_{max} = 21.747 \text{ kipft}$$

Shear force and Bending moment (z-direction, LRFD)

H_o - Lateral force per length of pile,

$$H_o = \frac{V_z}{1.57 b}$$

$$H_o = \frac{(0.476 \text{ kip})}{1.57 \times (48 \text{ in})}$$

$$H_o = 0.075796 \text{ kip/ft}$$

M_o - Moment per length of pile,

$$M_o = \frac{M_x + (V_z H)}{1.57 b}$$

$$M_o = \frac{(1.341 \text{ kipft}) + ((0.476 \text{ kip}) \times (0 \text{ ft}))}{1.57 \times (48 \text{ in})}$$

$$M_o = 0.21354 \text{ kipft/ft}$$

E - Distance from lateral load to resisting surface,

$$E = \frac{M_o}{H_o}$$

$$E = \frac{(0.21354 \text{ kipft/ft})}{(0.075796 \text{ kip/ft})}$$

$$E = 2.8172 \text{ ft}$$

a - Distance from resting surface to pivot point,

$$a = \frac{(4 M_o L_e) + (3 H_o L_e^2)}{(6 M_o) + (4 H_o L_e)}$$

$$a = \frac{(4 \times (0.21354 \text{ kipft/ft}) \times (5.75 \text{ ft})) + (3 \times (0.075796 \text{ kip/ft}) \times (5.75 \text{ ft})^2)}{(6 \times (0.21354 \text{ kipft/ft})) + (4 \times (0.075796 \text{ kip/ft}) \times (5.75 \text{ ft}))}$$

$$a = 4.1095 \text{ ft}$$

V_{max} - Max shear force located at depth a ,

$$V_{max} = (H_o b) \left[1 - \left[3 \left(\frac{4 E}{L_e} + 3 \right) \left(\frac{a}{L_e} \right)^2 \right] + \left[4 \left(\frac{3 E}{L_e} + 2 \right) \left(\frac{a}{L_e} \right)^3 \right] \right]$$

$$V_{max} = ((0.075796 \text{ kip/ft}) \times (48 \text{ in})) \times \left[1 - \left[3 \times \left(\frac{4 \times (2.8172 \text{ ft})}{(5.75 \text{ ft})} + 3 \right) \times \left(\frac{(4.1095 \text{ ft})}{(5.75 \text{ ft})} \right)^2 \right] + \left[4 \times \left(\frac{3 \times (2.8172 \text{ ft})}{(5.75 \text{ ft})} + 2 \right) \times \left(\frac{(4.1095 \text{ ft})}{(5.75 \text{ ft})} \right)^3 \right] \right]$$

$$V_{max} = 0.46492 \text{ kip}$$

M_{max} - Max bending moment located at depth $a/2$,

$$M_{max} = (H_o b L_e) \left[\left(\frac{E}{L_e} + \frac{a}{2 L_e} \right) - \left[\left(\frac{4 E}{L_e} + 3 \right) \left(\frac{a}{2 L_e} \right)^3 \right] + \left[\left(\frac{3 E}{L_e} + 2 \right) \left(\frac{a}{2 L_e} \right)^4 \right] \right]$$

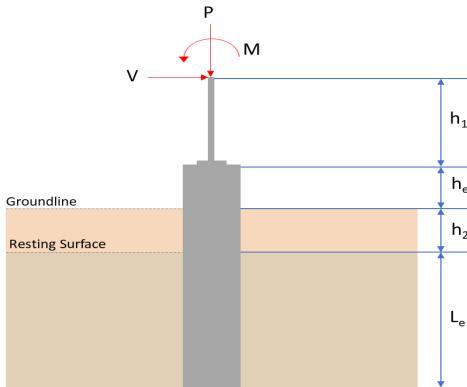
$$M_{max} = ((0.075796 \text{ kip/ft}) \times (48 \text{ in}) \times (5.75 \text{ ft})) \times \left[\left(\frac{(2.8172 \text{ ft})}{(5.75 \text{ ft})} + \frac{(4.1095 \text{ ft})}{2 \times (5.75 \text{ ft})} \right) - \left[\left(\frac{4 \times (2.8172 \text{ ft})}{(5.75 \text{ ft})} + 3 \right) \times \left(\frac{(4.1095 \text{ ft})}{2 \times (5.75 \text{ ft})} \right)^3 \right] + \left[\left(\frac{3 \times (2.8172 \text{ ft})}{(5.75 \text{ ft})} + 2 \right) \times \left(\frac{(4.1095 \text{ ft})}{2 \times (5.75 \text{ ft})} \right)^4 \right] \right]$$

		$M_{max} = 1.1812 \text{ kipft}$	
		Minimum Reinforcement Check (LRFD) Parameters: $f'_{ck} = 2.5 \text{ ksi}$ - Concrete strength, $f_{yk} = 60 \text{ ksi}$ - Longitudinal reinforcement strength, $\phi = 0.65$ - Reduction factor for axial strength, $\alpha = 0.8$ - Alpha factor for axial strength, $A_g = 2304 \text{ in}^2$ - Gross area of concrete, Longitudinal reinforcement: Required reinforcement due to axial load, $A_{st,required}$ $A_{st,required}$ $A_{st,required} = \text{Min} \left[\frac{\frac{P}{\phi \alpha} - (0.85 f'_{ck} A_g)}{f_{yk} - (0.85 f'_{ck})}, (0.08 A_g) \right]$ $A_{st,required} = \text{Min} \left[\frac{\frac{(0.153 \text{ kip})}{(0.65) \times (0.8)} - (0.85 \times (2.5 \text{ ksi}) \times (2304 \text{ in}^2))}{(60 \text{ ksi}) - (0.85 \times (2.5 \text{ ksi}))}, (0.08 \times (2304 \text{ in}^2)) \right]$ $A_{st,required} = -84.292 \text{ in}^2$ A_{min} - Governing minimum reinforcement area, $A_{min} = \text{Max} [A_{st,required}, (0.0018 A_g)]$ $A_{min} = \text{Max} [(-84.292 \text{ in}^2), (0.0018 \times (2304 \text{ in}^2))]$ $A_{min} = 4.1472 \text{ in}^2$ n_{rebar} - Required number of reinforcement, $n_{rebar} = \frac{A_{min}}{A_{rebar}}$ $n_{rebar} = \frac{(4.1472 \text{ in}^2)}{(0.3068 \text{ in}^2)}$ $n_{rebar} = 14$ A_{st} - Actual total reinforcement area, $A_{st} = n_{rebar} \frac{\pi d_{bar}^2}{4}$ $A_{st} = (14) \times \frac{\pi \times (0.625 \text{ in})^2}{4}$ $A_{st} = 4.2951 \text{ in}^2$ Ratio - Capacity $\text{Ratio} = \frac{A_{min}}{A_{st}}$ $\text{Ratio} = \frac{(4.1472 \text{ in}^2)}{(4.2951 \text{ in}^2)}$ $\text{Ratio} = 0.96556$ 25.2.3 s_{rebar} - Minimum spacing of reinforcement, $s_{rebar} = \text{Max} [1.5, (1.5 d_{bar})]$ $s_{rebar} = \text{Max} [1.5, (1.5 \times (0.625 \text{ in}))]$ $s_{rebar} = 1.5 \text{ in}$ Ties: 25.7.2.2 Since longitudinal reinforcement is $\leq \text{No. } 10\phi$: Use #3(0.375 in) 25.7.2.1 s_{ties} - Maximum spacing of ties, $s_{ties} = \text{Min} [(16 d_{bar}), (48 d_{ties}), \text{Min}(D, b)]$ $s_{ties} = \text{Min} [(16 \times (0.625 \text{ in})), (48 \times (0.375 \text{ in})), \text{Min}((48 \text{ in}), (48 \text{ in}))]$ $s_{ties} = 10 \text{ in}$ Summary: Main reinforcement: 14 - #5 (0.625 in)	Status: PASS Ratio: 0.970

		Ties: #3(0.375 in) - 10 in			
22.4.2.2		Axial Compression Strength (ACI 318-19, LRFD) ϕP_N - Allowable axial compressive strength $\phi P_N = \phi 0.80 \left[\left(0.85 f'_{ck} \left[A_g - A_{st} \right] \right) + \left(f_{yk} A_{st} \right) \right]$$\phi P_N = (0.65) \times 0.80 \times \left[\left(0.85 \times (2.5 \text{ ksi}) \times \left[(2304 \text{ in}^2) - (4.2951 \text{ in}^2) \right] \right) + \left((60 \text{ ksi}) \times (4.2951 \text{ in}^2) \right) \right]$$\phi P_N = 2675.2 \text{ kip}$ Ratio - Capacity $Ratio = \frac{P}{\phi P_N}$$Ratio = \frac{(9.153 \text{ kip})}{(2675.2 \text{ kip})}$$Ratio = 0.0034214$			
				Status: PASS Ratio: 0.000	
22.5.2.2		Shear Strength (ACI 318-19, LRFD) Parameters: $b_w = 48 \text{ in}$ - Effective width, d - Effective depth $d = 0.80 D$$d = 0.80 \times (48 \text{ in})$$d = 38.4 \text{ in}$			
22.5.5.1.3		λ_s - size effect modification factor $\lambda_s = MIN \left[\sqrt{\frac{2}{1 + \frac{d}{10}}}, 1 \right]$$\lambda_s = MIN \left[\sqrt{\frac{2}{1 + \frac{(38.4 \text{ in})}{10}}}, 1 \right]$$\lambda_s = 0.64282$			
22.5.5.1.1		The following variables were converted to be consistent with empirical formula $f'_{ck} = 2.5 \text{ ksi} \rightarrow 2500 \text{ psi}$, $V_{c,max}$ - Max shear strength of concrete $V_{c,max} = 5 \lambda_s \sqrt{f'_{ck}} b_w d$$V_{c,max} = 5 \times (0.64282) \times \sqrt{(2500 \text{ psi})} \times (48 \text{ in}) \times (38.4 \text{ in})$$V_{c,max} = 296.21 \text{ kip}$			
22.5.5.1.1(a)		The following variables were converted to be consistent with empirical formula $f'_{ck} = 2.5 \text{ ksi} \rightarrow 2500 \text{ psi}$, $P = 9.153 \text{ kip} \rightarrow 9153 \text{ lbf}$, $V_{c,a}$ - Shear strength of concrete (a) $V_{c,a} = \left[2 \lambda_s \sqrt{f'_{ck}} + \frac{P}{6 A_g} \right] b_w d$$V_{c,a} = \left[2 \times (0.64282) \times \sqrt{(2500 \text{ psi})} + \frac{(9153 \text{ lbf})}{6 \times (2304 \text{ in}^2)} \right] \times (48 \text{ in}) \times (38.4 \text{ in})$$V_{c,a} = 119.71 \text{ kip}$			
22.5.5.1.2		The following variables were converted to be consistent with empirical formula $f'_{ck} = 2.5 \text{ ksi} \rightarrow 2500 \text{ psi}$, $V_{c,b}$ - Shear strength of concrete (b) $V_{c,b} = \left[2 \lambda_s \sqrt{f'_{ck}} + (0.05 f'_{ck}) \right] b_w d$$V_{c,b} = \left[2 \times (0.64282) \times \sqrt{(2500 \text{ psi})} + (0.05 \times (2500 \text{ psi})) \right] \times (48 \text{ in}) \times (38.4 \text{ in})$$V_{c,b} = 348.89 \text{ kip}$ V_c - Governing shear strength of concrete $V_c = Min [V_{c,max}, V_{c,a}, V_{c,b}]$$V_c = Min [(296.21 \text{ kip}), (119.71 \text{ kip}), (348.89 \text{ kip})]$$V_c = 119.71 \text{ kip}$			

22.5.1.2 22.5.8.5.3 22.5.1.1	The following variables were converted to be consistent with empirical formula $f'_{ck} = 2.5 \text{ ksi} \rightarrow 2500 \text{ psi}$, $V_{s,a}$ - Shear strength of steel (a) $V_{s,a} = 8 \sqrt{f'_{ck}} b_w d$ $V_{s,a} = 8 \times \sqrt{(2500 \text{ psi})} \times (48 \text{ in}) \times (38.4 \text{ in})$ $V_{s,a} = 737.28 \text{ kip}$ A_v - Ties rebar area, $A_v = \frac{\pi d_{tes}^2}{4}$ $A_v = \frac{\pi \times (0.375 \text{ in})^2}{4}$ $A_v = 0.11045 \text{ in}^2$ $V_{s,b}$ - Shear strength of steel (b) $V_{s,b} = \frac{2 A_v f_{ysk} d}{s_{ties}}$ $V_{s,b} = \frac{2 \times (0.11045 \text{ in}^2) \times (60 \text{ ksi}) \times (38.4 \text{ in})}{(10 \text{ in})}$ $V_{s,b} = 50.894 \text{ kip}$ V_s - Governing shear strength of steel $V_s = MIN[V_{s,a}, V_{s,b}]$ $V_s = MIN[(737.28 \text{ kip}), (50.894 \text{ kip})]$ $V_s = 50.894 \text{ kip}$ ϕV_n - Allowable shear strength $\phi V_n = \phi (V_c + V_s)$ $\phi V_n = (0.65) \times ((119.71 \text{ kip}) + (50.894 \text{ kip}))$ $\phi V_n = 110.89 \text{ kip}$ Considering x-direction: $V_{max} = 7.9544 \text{ kip}$ - Maximum shear force in the x-direction, $Ratio$ - Capacity $Ratio = \frac{V_{max}}{\phi V_n}$ $Ratio = \frac{(7.9544 \text{ kip})}{(110.89 \text{ kip})}$ $Ratio = 0.071733$ Considering z-direction: $V_{max} = 0.46492 \text{ kip}$ - Maximum shear force in the z-direction, $Ratio$ - Capacity $Ratio = \frac{V_{max}}{\phi V_n}$ $Ratio = \frac{(0.46492 \text{ kip})}{(110.89 \text{ kip})}$ $Ratio = 0.0041926$	Status: PASS Ratio: 0.070 Status: PASS Ratio: 0.000
	Flexural Strength (ACI 318-19, LRFD) S_m - Section modulus $S_m = \frac{b D^3}{6}$ $S_m = \frac{(48 \text{ in}) \times (48 \text{ in})^2}{6}$ $S_m = 18432 \text{ in}^3$	

14.5.2.1b	$\lambda = 1$ - Concrete modification factor (Normal concrete), Allowable flexural strength: M_n shall be the lesser of: $\phi M_{n,1}$ $\phi M_{n,1} = \phi \times 5 \times \lambda \times \sqrt{f'_c} \times S_m$ $\phi M_{n,1} = 0.65 \times 5 \times 1 \times \sqrt{2.5 \text{ ksi}} \times 18432.001 \text{ in}^3$ $\phi M_{n,1} = 249.600 \text{ kipft}$ $\phi M_{n,2}$ $\phi M_{n,2} = \phi \times 0.85 \times f'_{ck} \times S_m$ $\phi M_{n,2} = (0.65) \times 0.85 \times (2.5 \text{ ksi}) \times (18432 \text{ in}^3)$ $\phi M_{n,2} = 2121.6 \text{ kipft}$ Therefore, ϕM_n - Allowable flexural strength, $\phi M_n = \text{MIN}[\phi M_{n,1}, \phi M_{n,2}]$ $\phi M_n = \text{MIN}[(249.6 \text{ kipft}), (2121.6 \text{ kipft})]$ $\phi M_n = 249.6 \text{ kipft}$ Considering x-direction: $M_{max} = 21.747 \text{ kipft}$ - Maximum moment in the x-direction, Ratio - Capacity $\text{Ratio} = \frac{M_{max}}{\phi M_n}$ $\text{Ratio} = \frac{(21.747 \text{ kipft})}{(249.6 \text{ kipft})}$ $\text{Ratio} = 0.087129$	Status: PASS Ratio: 0.090
	Considering z-direction: $M_{max} = 1.1812 \text{ kipft}$ - Maximum moment in the z-direction, Ratio - Capacity $\text{Ratio} = \frac{M_{max}}{\phi M_n}$ $\text{Ratio} = \frac{(1.1812 \text{ kipft})}{(249.6 \text{ kipft})}$ $\text{Ratio} = 0.0047323$	Status: PASS Ratio: 0.000

REFERENCES	CALCULATIONS	RESULTS																										
	SkyCiv Foundation Design Pile Foundation Design Information : Design code : IBC 2021 (International Building Code) Unit System : Imperial																											
	Pile Input  Geometry Pile shape: rectangular b = 48 in - Pile width D = 48 in - Pile depth L = 5.75 ft - Total pile length h1 = 0 ft - Lateral load height from the top of the pile, h2 = 0 ft - Depth to resisting surface he = 0 ft - Length of pile above the ground Tabulation of Soil Parameters <table><thead><tr><th>Layer</th><th>Label</th><th>Allowable Bearing Pressure (qa) (psf)</th><th>Allowable Lateral Pressure (R) (psf/ft)</th></tr></thead><tbody><tr><td>1</td><td>Sand, silty sand, clayey sand, silty gravel & clayey gravel</td><td>2000.000</td><td>150.000</td></tr></tbody></table> Tabulation of Loads <table><thead><tr><th>Load Component</th><th>ASD</th><th>LRFD</th></tr></thead><tbody><tr><td>P (kip)</td><td>6.229</td><td>9.153</td></tr><tr><td>Vx (kip)</td><td>-2.024</td><td>-3.373</td></tr><tr><td>Vz (kip)</td><td>-0.323</td><td>-0.476</td></tr><tr><td>Mx (kipft)</td><td>-0.913</td><td>-1.342</td></tr><tr><td>Mz (kipft)</td><td>19.584</td><td>33.353</td></tr></tbody></table> Material Properties f'ck = 2.5 ksi - Concrete strength,	Layer	Label	Allowable Bearing Pressure (qa) (psf)	Allowable Lateral Pressure (R) (psf/ft)	1	Sand, silty sand, clayey sand, silty gravel & clayey gravel	2000.000	150.000	Load Component	ASD	LRFD	P (kip)	6.229	9.153	Vx (kip)	-2.024	-3.373	Vz (kip)	-0.323	-0.476	Mx (kipft)	-0.913	-1.342	Mz (kipft)	19.584	33.353	
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	Required depth to resist lateral loads (ASD) H - Point of application of the lateral load $H = h_1 + h_2 + h_e$ $H = (0 \text{ ft}) + (0 \text{ ft}) + (0 \text{ ft})$ $H = 0 \text{ ft}$ Considering x-direction: H_o - Lateral force per length of pile, $H_o = \frac{V_x}{1.57 D}$ $H_o = \frac{(-2.024 \text{ kip})}{1.57 \times (48 \text{ in})}$ $H_o = -0.32229 \text{ kip/ft}$ M_o - Moment per length of pile, $M_o = \frac{M_z + (V_x H)}{1.57 D}$																											

	$M_o = \frac{(19.584 \text{ kipft}) + ((-2.024 \text{ kip}) \times (0 \text{ ft}))}{1.57 \times (48 \text{ in})}$ $M_o = 3.1185 \text{ kipft/ft}$ Required depth of embedment in earth: $L_x^3 - \left(14.14 \times \frac{H_o \times L_x}{R}\right) - \left(18.85 \times \frac{M_o}{R}\right) = 0$ Solving the cubic equation: $L_{e,x} = 5.2817 \text{ ft}$ - Required depth in x-direction, Considering z-direction: H_o - Lateral force per length of pile, $H_o = \frac{V_z}{1.57 b}$ $H_o = \frac{(-0.323 \text{ kip})}{1.57 \times (48 \text{ in})}$ $H_o = -0.051433 \text{ kip/ft}$ M_o - Moment per length of pile, $M_o = \frac{M_x + (V_z H)}{1.57 b}$ $M_o = \frac{(0.913 \text{ kipft}) + ((-0.323 \text{ kip}) \times (0 \text{ ft}))}{1.57 \times (48 \text{ in})}$ $M_o = 0.14538 \text{ kipft/ft}$ Required depth of embedment in earth: $L_z^3 - \left(14.14 \times \frac{H_o \times L_z}{R}\right) - \left(18.85 \times \frac{M_o}{R}\right) = 0$ Solving the cubic equation: $L_{e,z} = 1.8189 \text{ ft}$ - Required depth in z-direction, Minimum embedded depth required: $L_{e,req}$ - Depth of pile required, $L_{e,req} = MAX[L_{e,x}, L_{e,z}]$ $L_{e,req} = MAX[(5.2817 \text{ ft}), (1.8189 \text{ ft})]$ $L_{e,req} = 5.282 \text{ ft}$ L_e - Actual embedded length of pile, $L_e = L - h_e - h_2$ $L_e = (5.75 \text{ ft}) - (0 \text{ ft}) - (0 \text{ ft})$ $L_e = 5.75 \text{ ft}$ Ratio - Embedded depth $Ratio = \frac{L_{e,req}}{L_e}$ $Ratio = \frac{(5.282 \text{ ft})}{(5.75 \text{ ft})}$ $Ratio = 0.91861$	Status: PASS Ratio: 0.920
	End-bearing Capacity (ASD) A - Pile cross-section area $A = b D$ $A = (48 \text{ in}) \times (48 \text{ in})$ $A = 16 \text{ ft}^2$ q - End-bearing pressure $q = \frac{P_o}{A}$ $q = \frac{(6.229 \text{ kip})}{(16 \text{ ft}^2)}$	

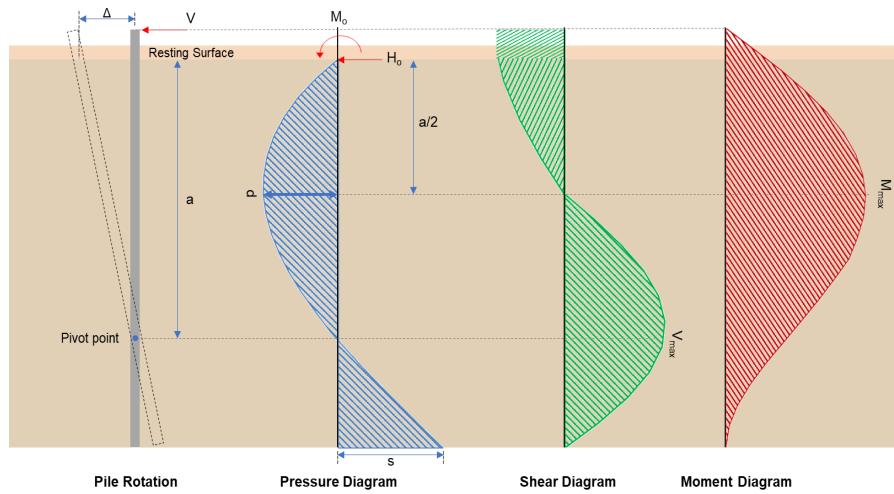
	$q = 0.00931 \text{ kip/ft}$	
	Check bearing capacity ratio: Ratio - Capacity $\text{Ratio} = \frac{q}{q_a}$ $\text{Ratio} = \frac{(0.38931 \text{ kip/ft}^2)}{(2000 \text{ psf})}$ $\text{Ratio} = 0.19466$	Status: PASS Ratio: 0.190
Czerniak	Lateral Soil Pressure (ASD): L/D - Length to least lateral dimension ratio, $L/D = \frac{L}{D}$ $L/D = \frac{(5.75 \text{ ft})}{(48 \text{ in})}$ $L/D = 1.4375$ Since $L/D \leq 10$, Pile is short. Considering x-direction: $H_o = -0.32229 \text{ kip/ft}$ - Lateral force per length of pile, $M_o = 3.1185 \text{ kipft/ft}$ - Overturning moment per length of pile, a - Distance from resting surface to pivot point, $a = \frac{(4 M_o L_e) + (3 H_o L_e^2)}{(6 M_o) + (4 H_o L_e)}$ $a = \frac{(4 \times (3.1185 \text{ kipft/ft}) \times (5.75 \text{ ft})) + (3 \times (-0.32229 \text{ kip/ft}) \times (5.75 \text{ ft})^2)}{(6 \times (3.1185 \text{ kipft/ft})) + (4 \times (-0.32229 \text{ kip/ft}) \times (5.75 \text{ ft}))}$ $a = 3.9693 \text{ ft}$ p - Earth pressure against the pile at distance $a/2$ from resting surface, $p = \frac{0.75 [(4 M_o) + (3 H_o L_e)]^2}{L_e^2 [(3 M_o) + (2 H_o L_e)]}$ $p = \frac{0.75 \times [(4 \times (3.1185 \text{ kipft/ft})) + (3 \times (-0.32229 \text{ kip/ft}) \times (5.75 \text{ ft}))]^2}{(5.75 \text{ ft})^2 \times [(3 \times (3.1185 \text{ kipft/ft})) + (2 \times (-0.32229 \text{ kip/ft}) \times (5.75 \text{ ft}))]}$ $p = 0.19198 \text{ kip/ft}^2$ s - Earth pressure against the pile at distance L_e, $s = \frac{6 [(2 M_o) + (H_o L_e)]}{L_e^2}$ $s = \frac{6 \times [(2 \times (3.1185 \text{ kipft/ft})) + ((-0.32229 \text{ kip/ft}) \times (5.75 \text{ ft}))]}{(5.75 \text{ ft})^2}$ $s = 0.79554 \text{ kip/ft}^2$ Check lateral soil pressure capacity: p_a - Allowable lateral soil pressure at depth $a/2$, $p_a = R \frac{a}{2}$ $p_a = (150 \text{ psf/ft}) \times \frac{(3.9693 \text{ ft})}{2}$ $p_a = 0.2977 \text{ kip/ft}^2$ Ratio - Lateral soil capacity $\text{Ratio} = \frac{p}{p_a}$ $\text{Ratio} = \frac{(0.19198 \text{ kip/ft}^2)}{(0.2977 \text{ kip/ft}^2)}$ $\text{Ratio} = 0.64488$ p_s - Allowable lateral soil pressure at depth L_e,	Status: PASS Ratio: 0.640

	$p_s = R L_e$ $p_s = (150 \text{ psf/ft}) \times (5.75 \text{ ft})$ $p_s = 0.8625 \text{ kip/ft}^2$ Ratio - Lateral soil capacity $\text{Ratio} = \frac{s}{p_s}$ $\text{Ratio} = \frac{(0.79554 \text{ kip/ft}^2)}{(0.8625 \text{ kip/ft}^2)}$ $\text{Ratio} = 0.92237$	Status: PASS Ratio: 0.920
	Considering z-direction: $H_o = -0.051433 \text{ kip/ft}$ - Lateral force per length of pile, $M_o = 0.14538 \text{ kipft/ft}$ - Overturning moment per length of pile, a - Distance from resting surface to pivot point, $a = \frac{(4 M_o L_e) + (3 H_o L_e^2)}{(6 M_o) + (4 H_o L_e)}$ $a = \frac{(4 \times (0.14538 \text{ kipft/ft}) \times (5.75 \text{ ft})) + (3 \times (-0.051433 \text{ kip/ft}) \times (5.75 \text{ ft})^2)}{(6 \times (0.14538 \text{ kipft/ft})) + (4 \times (-0.051433 \text{ kip/ft}) \times (5.75 \text{ ft}))}$ $a = 4.1091 \text{ ft}$ p - Earth pressure against the pile at distance $a/2$ from resting surface, $p = \frac{0.75 [(4 M_o) + (3 H_o L_e)]^2}{L_e^3 [(3 M_o) + (2 H_o L_e)]}$ $p = \frac{0.75 \times [(4 \times (0.14538 \text{ kipft/ft})) + (3 \times (-0.051433 \text{ kip/ft}) \times (5.75 \text{ ft}))]^2}{(5.75 \text{ ft})^3 \times [(3 \times (0.14538 \text{ kipft/ft})) + (2 \times (-0.051433 \text{ kip/ft}) \times (5.75 \text{ ft}))]}$ $p = -0.013647 \text{ kip/ft}^2$ s - Earth pressure against the pile at distance L_e, $s = \frac{6 [(2 M_o) + (H_o L_e)]}{L_e^2}$ $s = \frac{6 \times [(2 \times (0.14538 \text{ kipft/ft})) + ((-0.051433 \text{ kip/ft}) \times (5.75 \text{ ft}))]}{(5.75 \text{ ft})^2}$ $s = -0.00090304 \text{ kip/ft}^2$ Check lateral soil pressure capacity: p_a - Allowable lateral soil pressure at depth $a/2$, $p_a = R \frac{a}{2}$ $p_a = (150 \text{ psf/ft}) \times \frac{(4.1091 \text{ ft})}{2}$ $p_a = 0.30818 \text{ kip/ft}^2$ Ratio - Lateral soil capacity $\text{Ratio} = \frac{p}{p_a}$ $\text{Ratio} = \frac{(-0.013647 \text{ kip/ft}^2)}{(0.30818 \text{ kip/ft}^2)}$ $\text{Ratio} = -0.044281$ p_s - Allowable lateral soil pressure at depth L_e, $p_s = R L_e$ $p_s = (150 \text{ psf/ft}) \times (5.75 \text{ ft})$ $p_s = 0.8625 \text{ kip/ft}^2$ Ratio - Lateral soil capacity $\text{Ratio} = \frac{s}{p_s}$	Status: PASS Ratio: -0.040

$$Ratio = \frac{(-0.00090304 \text{ kip/ft}^2)}{(0.8625 \text{ kip/ft}^2)}$$

$$Ratio = -0.001047$$

Status: **PASS**
Ratio: **0.000**



Shear force and Bending moment (x-direction, LRFD)

H_o - Lateral force per length of pile,

$$H_o = \frac{V_x}{1.57 D}$$

$$H_o = \frac{(-3.373 \text{ kip})}{1.57 \times (48 \text{ in})}$$

$$H_o = -0.5371 \text{ kip/ft}$$

M_o - Moment per length of pile,

$$M_o = \frac{M_x + (V_x H)}{1.57 D}$$

$$M_o = \frac{(33.353 \text{ kipft}) + ((-3.373 \text{ kip}) \times (0 \text{ ft}))}{1.57 \times (48 \text{ in})}$$

$$M_o = 5.311 \text{ kipft/ft}$$

E - Distance from lateral load to resisting surface,

$$E = \frac{M_o}{H_o}$$

$$E = \frac{(5.311 \text{ kipft/ft})}{(-0.5371 \text{ kip/ft})}$$

$$E = 9.8882 \text{ ft}$$

a - Distance from resting surface to pivot point,

$$a = \frac{(4 M_o L_e) + (3 H_o L_e^2)}{(6 M_o) + (4 H_o L_e)}$$

$$a = \frac{(4 \times (5.311 \text{ kipft/ft}) \times (5.75 \text{ ft})) + (3 \times (-0.5371 \text{ kip/ft}) \times (5.75 \text{ ft})^2)}{(6 \times (5.311 \text{ kipft/ft})) + (4 \times (-0.5371 \text{ kip/ft}) \times (5.75 \text{ ft}))}$$

$$a = 3.9672 \text{ ft}$$

V_{max} - Max shear force located at depth a ,

$$V_{max} = (H_o D) \left[1 - \left[3 \left(\frac{4 E}{L_e} + 3 \right) \left(\frac{a}{L_e} \right)^2 \right] + \left[4 \left(\frac{3 E}{L_e} + 2 \right) \left(\frac{a}{L_e} \right)^3 \right] \right]$$

$$V_{max} = ((-0.5371 \text{ kip/ft}) \times (48 \text{ in})) \times \left[1 - \left[3 \times \left(\frac{4 \times (9.8882 \text{ ft})}{(5.75 \text{ ft})} + 3 \right) \times \left(\frac{(3.9672 \text{ ft})}{(5.75 \text{ ft})} \right)^2 \right] + \left[4 \times \left(\frac{3 \times (9.8882 \text{ ft})}{(5.75 \text{ ft})} + 2 \right) \times \left(\frac{(3.9672 \text{ ft})}{(5.75 \text{ ft})} \right)^3 \right] \right]$$

$$V_{max} = 7.9546 \text{ kip}$$

M_{max} - Max bending moment located at depth $a/2$,

$$M_{max} = (H_o D L_e) \left[\left(\frac{E}{L_e} + \frac{a}{2 L_e} \right) - \left[\left(\frac{4 E}{L_e} + 3 \right) \left(\frac{a}{2 L_e} \right)^3 \right] + \left[\left(\frac{3 E}{L_e} + 2 \right) \left(\frac{a}{2 L_e} \right)^4 \right] \right]$$

$$M_{max} = ((-0.5371 \text{ kip/ft}) \times (48 \text{ in}) \times (5.75 \text{ ft})) \times \left[\left(\frac{(9.8882 \text{ ft})}{(5.75 \text{ ft})} + \frac{(3.9672 \text{ ft})}{2 \times (5.75 \text{ ft})} \right) - \left[\left(\frac{4 \times (9.8882 \text{ ft})}{(5.75 \text{ ft})} + 3 \right) \times \left(\frac{(3.9672 \text{ ft})}{2 \times (5.75 \text{ ft})} \right)^3 \right] + \left[\left(\frac{3 \times (9.8882 \text{ ft})}{(5.75 \text{ ft})} + 2 \right) \times \left(\frac{(3.9672 \text{ ft})}{2 \times (5.75 \text{ ft})} \right)^4 \right] \right]$$

$$M_{max} = 21.748 \text{ kipft}$$

Shear force and Bending moment (z-direction, LRFD)

H_o - Lateral force per length of pile,

$$H_o = \frac{V_z}{1.57 b}$$

$$H_o = \frac{(-0.476 \text{ kip})}{1.57 \times (48 \text{ in})}$$

$$H_o = -0.075796 \text{ kip/ft}$$

M_o - Moment per length of pile,

$$M_o = \frac{M_x + (V_z H)}{1.57 b}$$

$$M_o = \frac{(1.342 \text{ kipft}) + ((-0.476 \text{ kip}) \times (0 \text{ ft}))}{1.57 \times (48 \text{ in})}$$

$$M_o = 0.21369 \text{ kipft/ft}$$

E - Distance from lateral load to resisting surface,

$$E = \frac{M_o}{H_o}$$

$$E = \frac{(0.21369 \text{ kipft/ft})}{(-0.075796 \text{ kip/ft})}$$

$$E = 2.8193 \text{ ft}$$

a - Distance from resting surface to pivot point,

$$a = \frac{(4 M_o L_e) + (3 H_o L_e^2)}{(6 M_o) + (4 H_o L_e)}$$

$$a = \frac{(4 \times (0.21369 \text{ kipft/ft}) \times (5.75 \text{ ft})) + (3 \times (-0.075796 \text{ kip/ft}) \times (5.75 \text{ ft})^2)}{(6 \times (0.21369 \text{ kipft/ft})) + (4 \times (-0.075796 \text{ kip/ft}) \times (5.75 \text{ ft}))}$$

$$a = 4.1094 \text{ ft}$$

V_{max} - Max shear force located at depth a ,

$$V_{max} = (H_o b) \left[1 - \left[3 \left(\frac{4 E}{L_e} + 3 \right) \left(\frac{a}{L_e} \right)^2 \right] + \left[4 \left(\frac{3 E}{L_e} + 2 \right) \left(\frac{a}{L_e} \right)^3 \right] \right]$$

$$V_{max} = ((-0.075796 \text{ kip/ft}) \times (48 \text{ in})) \times \left[1 - \left[3 \times \left(\frac{4 \times (2.8193 \text{ ft})}{(5.75 \text{ ft})} + 3 \right) \times \left(\frac{(4.1094 \text{ ft})}{(5.75 \text{ ft})} \right)^2 \right] + \left[4 \times \left(\frac{3 \times (2.8193 \text{ ft})}{(5.75 \text{ ft})} + 2 \right) \times \left(\frac{(4.1094 \text{ ft})}{(5.75 \text{ ft})} \right)^3 \right] \right]$$

$$V_{max} = 0.46511 \text{ kip}$$

M_{max} - Max bending moment located at depth $a/2$,

$$M_{max} = (H_o b L_e) \left[\left(\frac{E}{L_e} + \frac{a}{2 L_e} \right) - \left[\left(\frac{4 E}{L_e} + 3 \right) \left(\frac{a}{2 L_e} \right)^3 \right] + \left[\left(\frac{3 E}{L_e} + 2 \right) \left(\frac{a}{2 L_e} \right)^4 \right] \right]$$

$$M_{max} = ((-0.075796 \text{ kip/ft}) \times (48 \text{ in}) \times (5.75 \text{ ft})) \times \left[\left(\frac{(2.8193 \text{ ft})}{(5.75 \text{ ft})} + \frac{(4.1094 \text{ ft})}{2 \times (5.75 \text{ ft})} \right) - \left[\left(\frac{4 \times (2.8193 \text{ ft})}{(5.75 \text{ ft})} + 3 \right) \times \left(\frac{(4.1094 \text{ ft})}{2 \times (5.75 \text{ ft})} \right)^3 \right] + \left[\left(\frac{3 \times (2.8193 \text{ ft})}{(5.75 \text{ ft})} + 2 \right) \times \left(\frac{(4.1094 \text{ ft})}{2 \times (5.75 \text{ ft})} \right)^4 \right] \right]$$

		$M_{max} = 1.1817 \text{ kipft}$	
		Minimum Reinforcement Check (LRFD) Parameters: $f'_{ck} = 2.5 \text{ ksi}$ - Concrete strength, $f_{yk} = 60 \text{ ksi}$ - Longitudinal reinforcement strength, $\phi = 0.65$ - Reduction factor for axial strength, $\alpha = 0.8$ - Alpha factor for axial strength, $A_g = 2304 \text{ in}^2$ - Gross area of concrete, Longitudinal reinforcement: Required reinforcement due to axial load, $A_{st,required}$ $A_{st,required}$ $A_{st,required} = \text{Min} \left[\frac{\frac{P}{\phi \alpha} - (0.85 f'_{ck} A_g)}{f_{yk} - (0.85 f'_{ck})}, (0.08 A_g) \right]$ $A_{st,required} = \text{Min} \left[\frac{\frac{(0.153 \text{ kip})}{(0.65) \times (0.8)} - (0.85 \times (2.5 \text{ ksi}) \times (2304 \text{ in}^2))}{(60 \text{ ksi}) - (0.85 \times (2.5 \text{ ksi}))}, (0.08 \times (2304 \text{ in}^2)) \right]$ $A_{st,required} = -84.292 \text{ in}^2$ A_{min} - Governing minimum reinforcement area, $A_{min} = \text{Max} [A_{st,required}, (0.0018 A_g)]$ $A_{min} = \text{Max} [(-84.292 \text{ in}^2), (0.0018 \times (2304 \text{ in}^2))]$ $A_{min} = 4.1472 \text{ in}^2$ n_{rebar} - Required number of reinforcement, $n_{rebar} = \frac{A_{min}}{A_{rebar}}$ $n_{rebar} = \frac{(4.1472 \text{ in}^2)}{(0.3068 \text{ in}^2)}$ $n_{rebar} = 14$ A_{st} - Actual total reinforcement area, $A_{st} = n_{rebar} \frac{\pi d_{bar}^2}{4}$ $A_{st} = (14) \times \frac{\pi \times (0.625 \text{ in})^2}{4}$ $A_{st} = 4.2951 \text{ in}^2$ Ratio - Capacity $\text{Ratio} = \frac{A_{min}}{A_{st}}$ $\text{Ratio} = \frac{(4.1472 \text{ in}^2)}{(4.2951 \text{ in}^2)}$ $\text{Ratio} = 0.96556$ 25.2.3 s_{rebar} - Minimum spacing of reinforcement, $s_{rebar} = \text{Max} [1.5, (1.5 d_{bar})]$ $s_{rebar} = \text{Max} [1.5, (1.5 \times (0.625 \text{ in}))]$ $s_{rebar} = 1.5 \text{ in}$ Ties: 25.7.2.2 Since longitudinal reinforcement is $\leq \text{No. } 10\phi$: Use #3(0.375 in) 25.7.2.1 s_{ties} - Maximum spacing of ties, $s_{ties} = \text{Min} [(16 d_{bar}), (48 d_{ties}), \text{Min}(D, b)]$ $s_{ties} = \text{Min} [(16 \times (0.625 \text{ in})), (48 \times (0.375 \text{ in})), \text{Min}((48 \text{ in}), (48 \text{ in}))]$ $s_{ties} = 10 \text{ in}$ Summary: Main reinforcement: 14 - #5 (0.625 in)	Status: PASS Ratio: 0.970

	Ties: #3(0.375 in) - 10 in	
22.4.2.2	Axial Compression Strength (ACI 318-19, LRFD) ϕP_N - Allowable axial compressive strength $\phi P_N = \phi 0.80 \left[(0.85 f'_{ck} [A_g - A_{st}]) + (f_{yk} A_{st}) \right]$ $\phi P_N = (0.65) \times 0.80 \times \left[(0.85 \times (2.5 \text{ ksi}) \times [(2304 \text{ in}^2) - (4.2951 \text{ in}^2)]) + ((60 \text{ ksi}) \times (4.2951 \text{ in}^2)) \right]$ $\phi P_N = 2675.2 \text{ kip}$ Ratio - Capacity $\text{Ratio} = \frac{P}{\phi P_N}$ $\text{Ratio} = \frac{(9.153 \text{ kip})}{(2675.2 \text{ kip})}$ $\text{Ratio} = 0.0034214$	Status: PASS Ratio: 0.000
22.5.2.2	Shear Strength (ACI 318-19, LRFD) Parameters: $b_w = 48 \text{ in}$ - Effective width, d - Effective depth $d = 0.80 D$ $d = 0.80 \times (48 \text{ in})$ $d = 38.4 \text{ in}$	
22.5.5.1.3	λ_s - size effect modification factor $\lambda_s = \text{MIN} \left[\sqrt{\frac{2}{1 + \frac{d}{10}}}, 1 \right]$ $\lambda_s = \text{MIN} \left[\sqrt{\frac{2}{1 + \frac{(38.4 \text{ in})}{10}}}, 1 \right]$ $\lambda_s = 0.64282$	
22.5.5.1.1	The following variables were converted to be consistent with empirical formula $f'_{ck} = 2.5 \text{ ksi} \rightarrow 2500 \text{ psi}$, $V_{c,max}$ - Max shear strength of concrete $V_{c,max} = 5 \lambda_s \sqrt{f'_{ck}} b_w d$ $V_{c,max} = 5 \times (0.64282) \times \sqrt{(2500 \text{ psi})} \times (48 \text{ in}) \times (38.4 \text{ in})$ $V_{c,max} = 296.21 \text{ kip}$	
22.5.5.1.1(a)	The following variables were converted to be consistent with empirical formula $f'_{ck} = 2.5 \text{ ksi} \rightarrow 2500 \text{ psi}$, $P = 9.153 \text{ kip} \rightarrow 9153 \text{ lbf}$, $V_{c,a}$ - Shear strength of concrete (a) $V_{c,a} = \left[2 \lambda_s \sqrt{f'_{ck}} + \frac{P}{6 A_g} \right] b_w d$ $V_{c,a} = \left[2 \times (0.64282) \times \sqrt{(2500 \text{ psi})} + \frac{(9153 \text{ lbf})}{6 \times (2304 \text{ in}^2)} \right] \times (48 \text{ in}) \times (38.4 \text{ in})$ $V_{c,a} = 119.71 \text{ kip}$	
22.5.5.1.2	The following variables were converted to be consistent with empirical formula $f'_{ck} = 2.5 \text{ ksi} \rightarrow 2500 \text{ psi}$, $V_{c,b}$ - Shear strength of concrete (b) $V_{c,b} = \left[2 \lambda_s \sqrt{f'_{ck}} + (0.05 f'_{ck}) \right] b_w d$ $V_{c,b} = \left[2 \times (0.64282) \times \sqrt{(2500 \text{ psi})} + (0.05 \times (2500 \text{ psi})) \right] \times (48 \text{ in}) \times (38.4 \text{ in})$ $V_{c,b} = 348.89 \text{ kip}$ V_c - Governing shear strength of concrete $V_c = \text{Min} [V_{c,max}, V_{c,a}, V_{c,b}]$ $V_c = \text{Min} [(296.21 \text{ kip}), (119.71 \text{ kip}), (348.89 \text{ kip})]$ $V_c = 119.71 \text{ kip}$	

22.5.1.2 22.5.8.5.3 22.5.1.1	The following variables were converted to be consistent with empirical formula $f'_{ck} = 2.5 \text{ ksi} \rightarrow 2500 \text{ psi}$, $V_{s,a}$ - Shear strength of steel (a) $V_{s,a} = 8 \sqrt{f'_{ck}} b_w d$ $V_{s,a} = 8 \times \sqrt{(2500 \text{ psi})} \times (48 \text{ in}) \times (38.4 \text{ in})$ $V_{s,a} = 737.28 \text{ kip}$ A_v - Ties rebar area, $A_v = \frac{\pi d_{tes}^2}{4}$ $A_v = \frac{\pi \times (0.375 \text{ in})^2}{4}$ $A_v = 0.11045 \text{ in}^2$ $V_{s,b}$ - Shear strength of steel (b) $V_{s,b} = \frac{2 A_v f_{ysk} d}{s_{ties}}$ $V_{s,b} = \frac{2 \times (0.11045 \text{ in}^2) \times (60 \text{ ksi}) \times (38.4 \text{ in})}{(10 \text{ in})}$ $V_{s,b} = 50.894 \text{ kip}$ V_s - Governing shear strength of steel $V_s = MIN[V_{s,a}, V_{s,b}]$ $V_s = MIN[(737.28 \text{ kip}), (50.894 \text{ kip})]$ $V_s = 50.894 \text{ kip}$ ϕV_n - Allowable shear strength $\phi V_n = \phi (V_c + V_s)$ $\phi V_n = (0.65) \times ((119.71 \text{ kip}) + (50.894 \text{ kip}))$ $\phi V_n = 110.89 \text{ kip}$ Considering x-direction: $V_{max} = 7.9546 \text{ kip}$ - Maximum shear force in the x-direction, $Ratio$ - Capacity $Ratio = \frac{V_{max}}{\phi V_n}$ $Ratio = \frac{(7.9546 \text{ kip})}{(110.89 \text{ kip})}$ $Ratio = 0.071734$ Considering z-direction: $V_{max} = 0.46511 \text{ kip}$ - Maximum shear force in the z-direction, $Ratio$ - Capacity $Ratio = \frac{V_{max}}{\phi V_n}$ $Ratio = \frac{(0.46511 \text{ kip})}{(110.89 \text{ kip})}$ $Ratio = 0.0041944$	Status: PASS Ratio: 0.070 Status: PASS Ratio: 0.000
	Flexural Strength (ACI 318-19, LRFD) S_m - Section modulus $S_m = \frac{b D^3}{6}$ $S_m = \frac{(48 \text{ in}) \times (48 \text{ in})^2}{6}$ $S_m = 18432 \text{ in}^3$	

14.5.2.1b	$\lambda = 1$ - Concrete modification factor (Normal concrete), Allowable flexural strength: M_n shall be the lesser of: $\phi M_{n,1}$ $\phi M_{n,1} = \phi \times 5 \times \lambda \times \sqrt{f'_c} \times S_m$ $\phi M_{n,1} = 0.65 \times 5 \times 1 \times \sqrt{2.5 \text{ ksi}} \times 18432.001 \text{ in}^3$ $\phi M_{n,1} = 249.600 \text{ kipft}$ $\phi M_{n,2}$ $\phi M_{n,2} = \phi \times 0.85 \times f'_c \times S_m$ $\phi M_{n,2} = (0.65) \times 0.85 \times (2.5 \text{ ksi}) \times (18432 \text{ in}^3)$ $\phi M_{n,2} = 2121.6 \text{ kipft}$ Therefore, ϕM_n - Allowable flexural strength, $\phi M_n = \text{MIN}[\phi M_{n,1}, \phi M_{n,2}]$ $\phi M_n = \text{MIN}[(249.6 \text{ kipft}), (2121.6 \text{ kipft})]$ $\phi M_n = 249.6 \text{ kipft}$ Considering x-direction: $M_{max} = 21.748 \text{ kipft}$ - Maximum moment in the x-direction, Ratio - Capacity $\text{Ratio} = \frac{M_{max}}{\phi M_n}$ $\text{Ratio} = \frac{(21.748 \text{ kipft})}{(249.6 \text{ kipft})}$ $\text{Ratio} = 0.087131$	Status: PASS Ratio: 0.090
	Considering z-direction: $M_{max} = 1.1817 \text{ kipft}$ - Maximum moment in the z-direction, Ratio - Capacity $\text{Ratio} = \frac{M_{max}}{\phi M_n}$ $\text{Ratio} = \frac{(1.1817 \text{ kipft})}{(249.6 \text{ kipft})}$ $\text{Ratio} = 0.0047345$	Status: PASS Ratio: 0.000