

Your Project Calculations



Project Name: MTSOLAR_LBIFLGHGK8DA

S3D Model Link:

https://platform.skyciv.com/structural?preload_name=MTSOLAR_LBIFLGHGK8DA&preload_path=Shared%20Enterprise%20Folder/MT_Solar_Projects/6_2023

Public Model Link:

https://platform.skyciv.com/structural-viewer?project_id=HUzSGtybR4m6RiQLMnGfCW7yybSxQvTUFZ2XHG3iwdsofR5masInOeFodAqWHH8b

Array Specification

Product:	Beam
Unique ID:	3P-19.75-8TOP-HD-45-L-5Hx8W-ALC5
Duty Classification:	HD
Module Width:	40.90 in
Module Length:	82.50in
Number of Rows:	5
Number of Columns:	8
Total Number of Modules:	40
Desired Tilt Angle:	42
Front Edge Clearance:	7
Total Array Height at Tilt:	18.47 ft
Total Frame Length:	54.50 ft
Frame Weight:	3397 lbs
Array Dimensions N/S:	17.25 ft
Array Dimensions E/W:	55.67 ft
Rail Length:	207.00 in
Rail Spacing:	3.44 ft
Rail Check:	Not Checked

Support Specifications

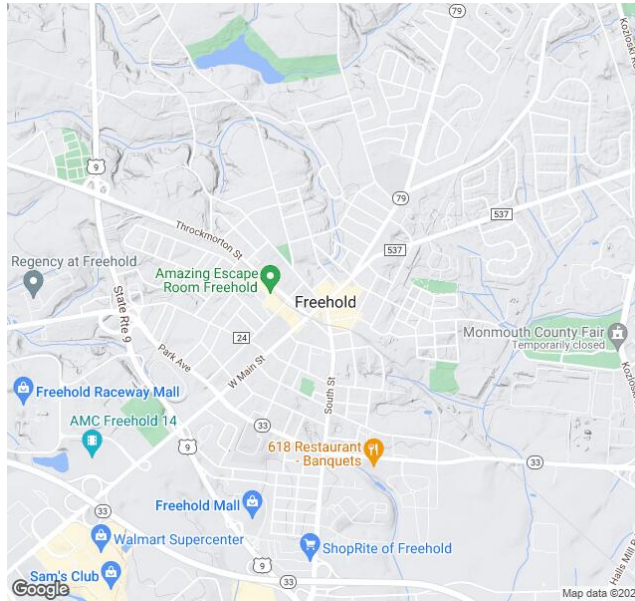
Pole Size:	8in Pipe Sch 80
Pole Length above Grade:	12.77 ft
Number of Poles:	3
Pole Spacing:	19.75 ft

Foundation Specifications

Foundation Type:	Square
Foundation Dimensions:	48 x 48 in
Foundation Depth (below grade):	Pile 1: 7.50 ft Pile 2: 7.75 ft Pile 3: 7.50 ft
Foundation Volume:	13.481 y ³
Foundation Result:	PASSED
Mount Twist:	0.890534 kip

Site Info

Risk Category:	I
Exposure:	B
Soil Classification:	sand
Site Location:	Freehold, NJ 07728, USA
Wind Speed:	108 mph
Snow Load:	25 psf
Design Uplift Pressure:	Multiple pressures
Design Downforce Pressure:	Multiple pressures
Design Snow Pressure:	0.007697 ksf



Design Disclaimer

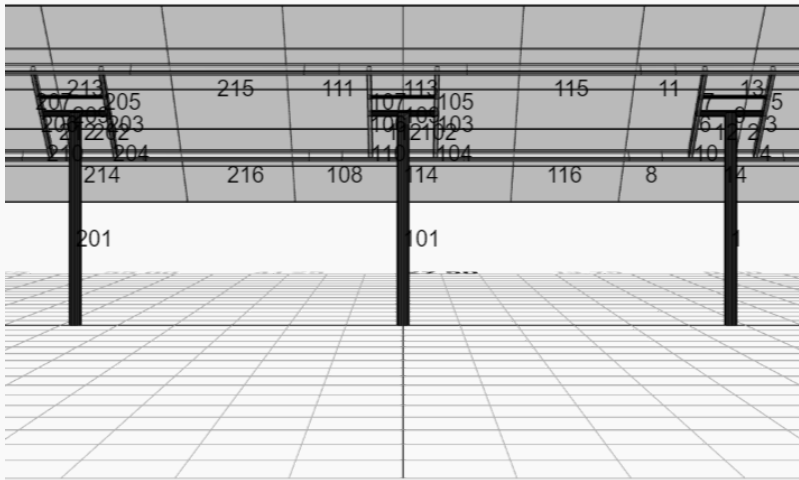
This software should be used for preliminary designs and should not be used as a final design unless reviewed, verified and designed by a qualified structural engineer.

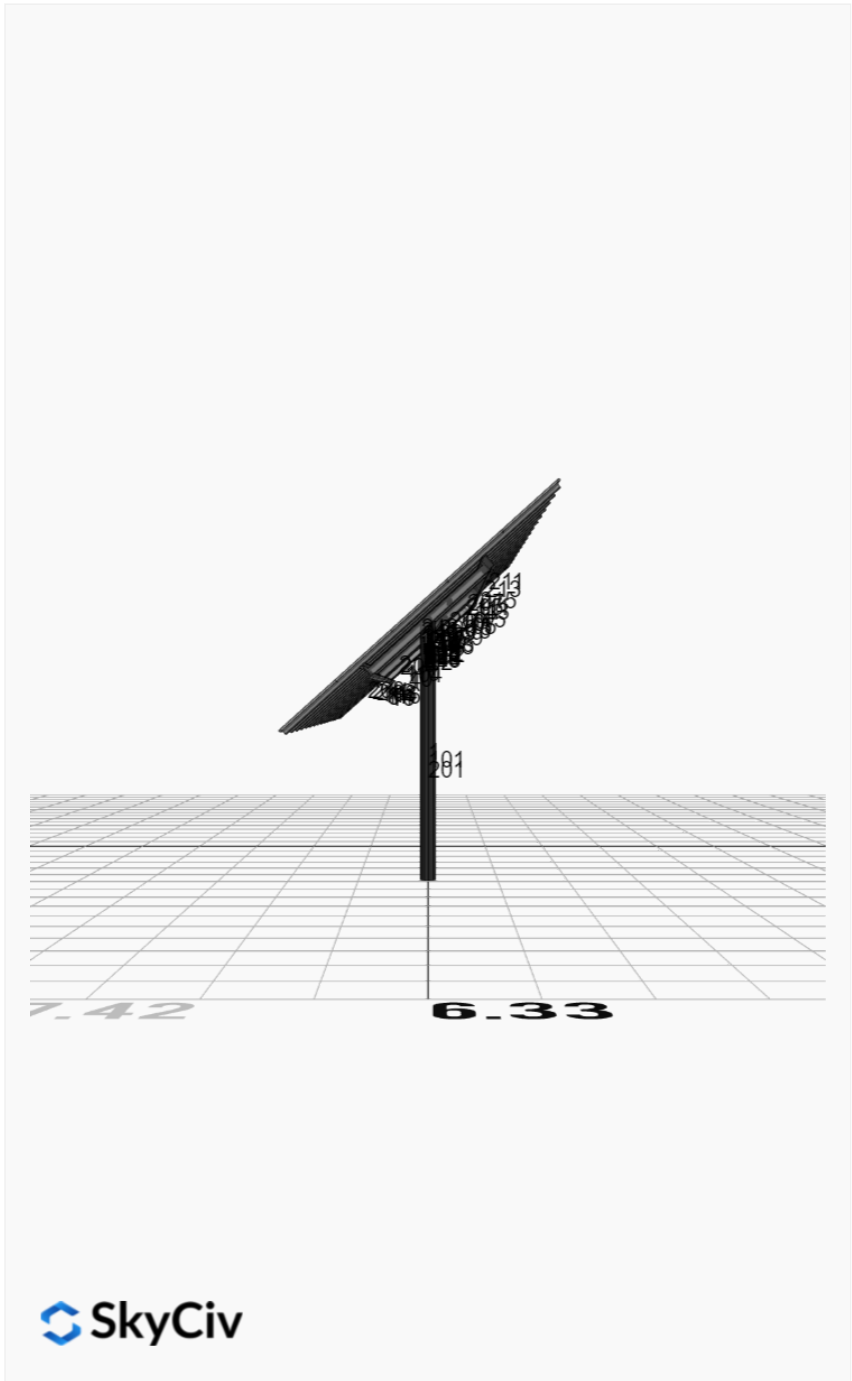
AutoDesigner Input

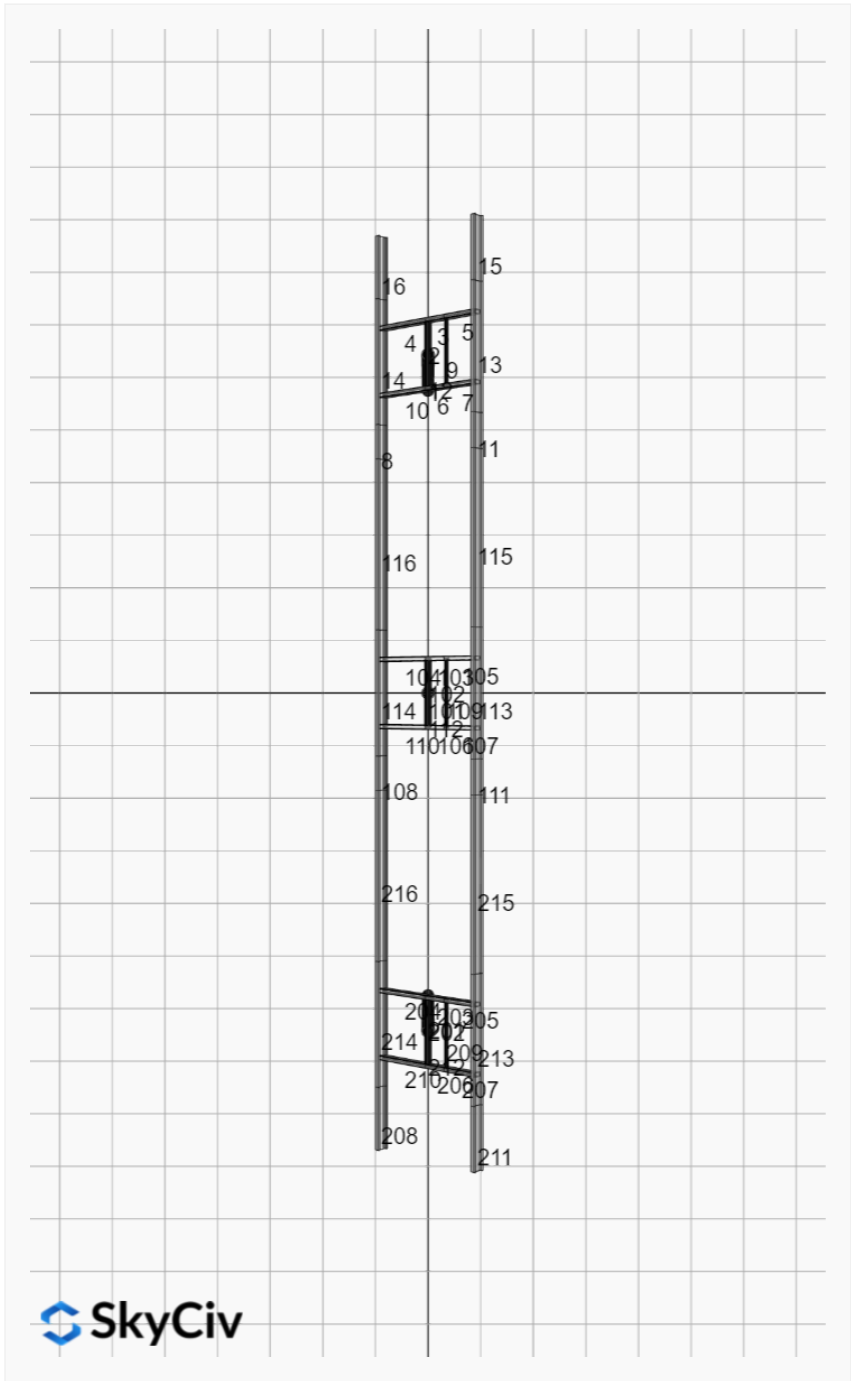
```
{"wind_speed_override":null,"snow_load_override":null,"direct_snow_load":false,"product_type":"Beam","project_id":"MTSOLAR_LBIFLGHGK8DA","site_address":"Freehold, NJ 07728, USA","module_width":40.9,"module_length":82.5,"number_rows":5,"number_columns":8,"pole_mount_section":"4_40","core_pipe_width":65,"core_pipe_section":"2_40","adjuster_section":"2_40","core_beam_height":65,"core_beam_section":"HSS3x2x1/8","main_pipe_section":"2_12GA","pole_spacing":15,"tilt_angle":42,"ground_clearance":7,"risk_category":"I","exposure_category":"B","frame_duty_override":"auto","pole_override":"auto","soil_type":"sand","foundation_type":"Square","foundation_size":48,"check_rails":false}
```

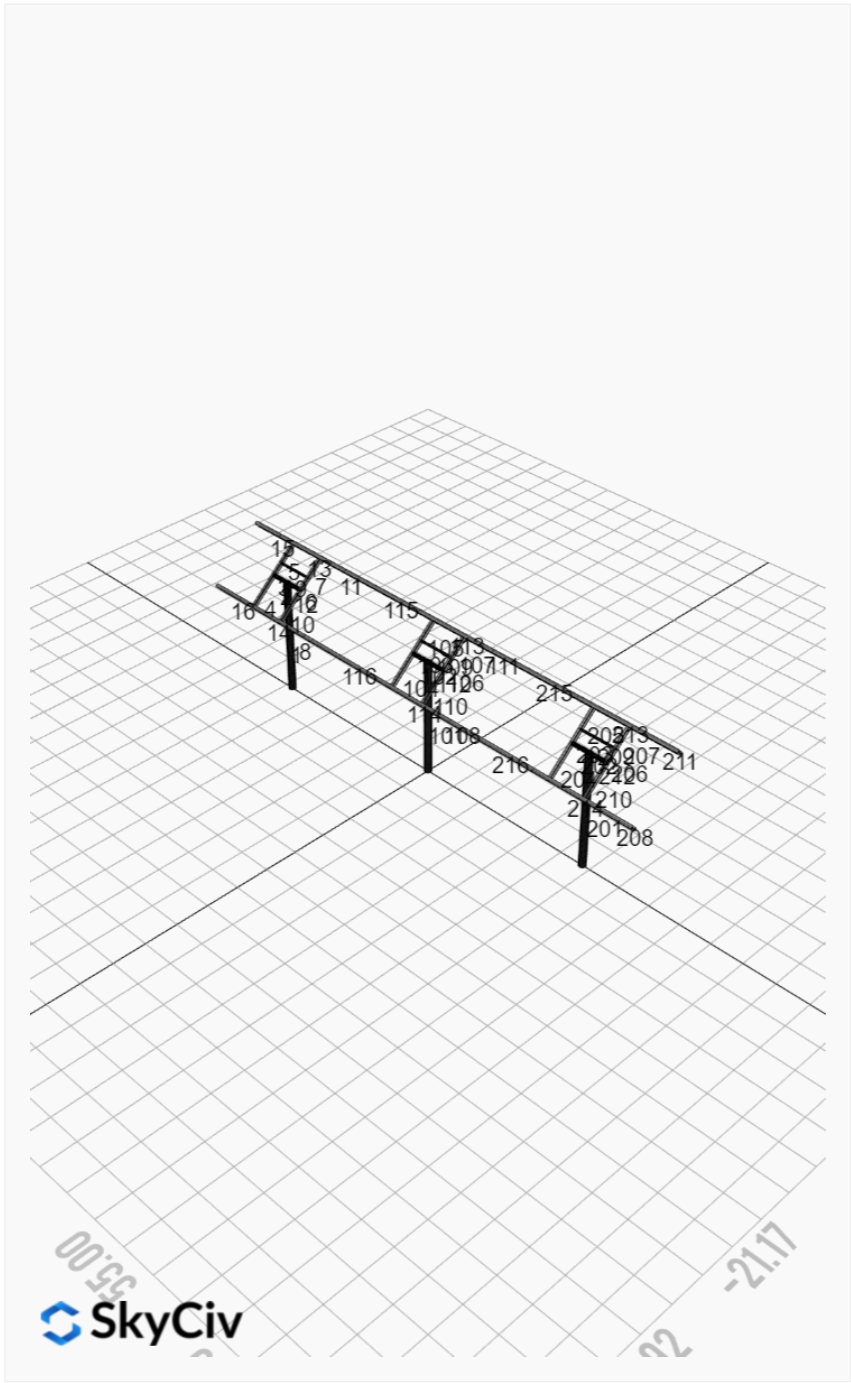
Design Notes:

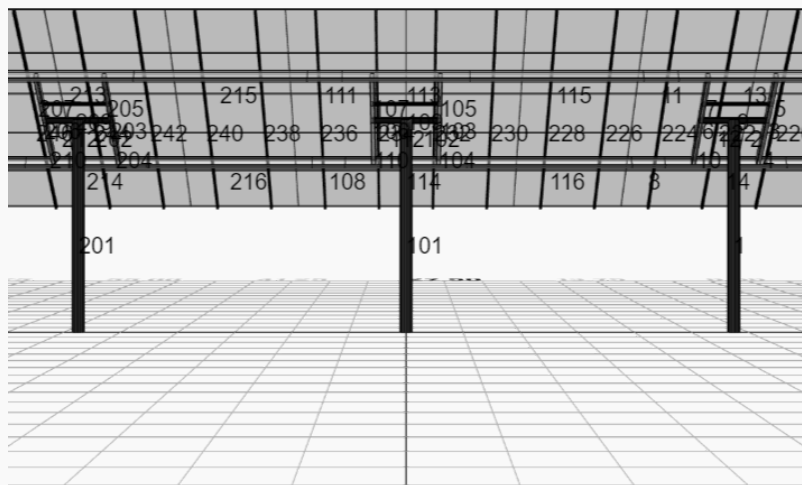
- AISC Deflection checks are set to L/1 due to structure design intent
- Foundation Design and Sizing is approximate only



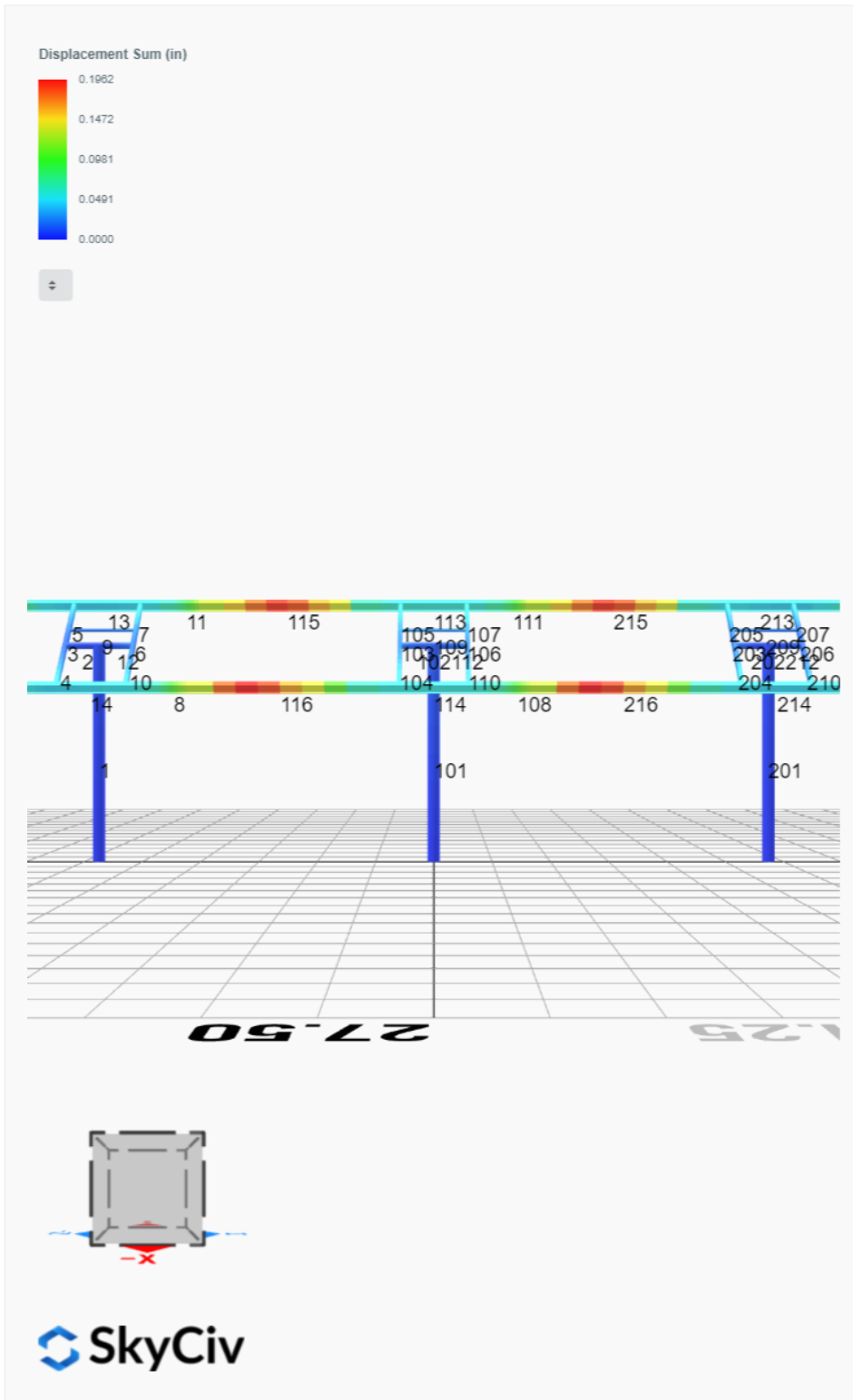




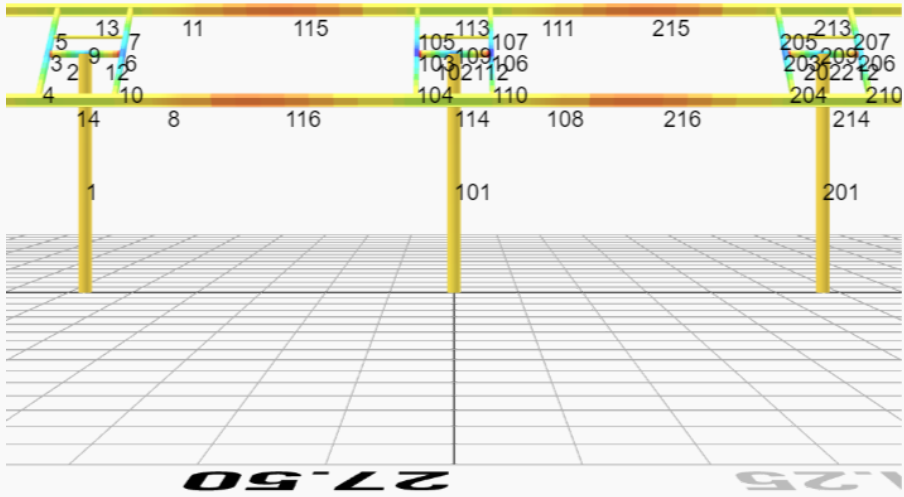
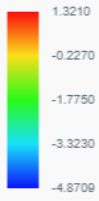




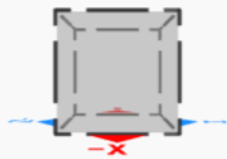
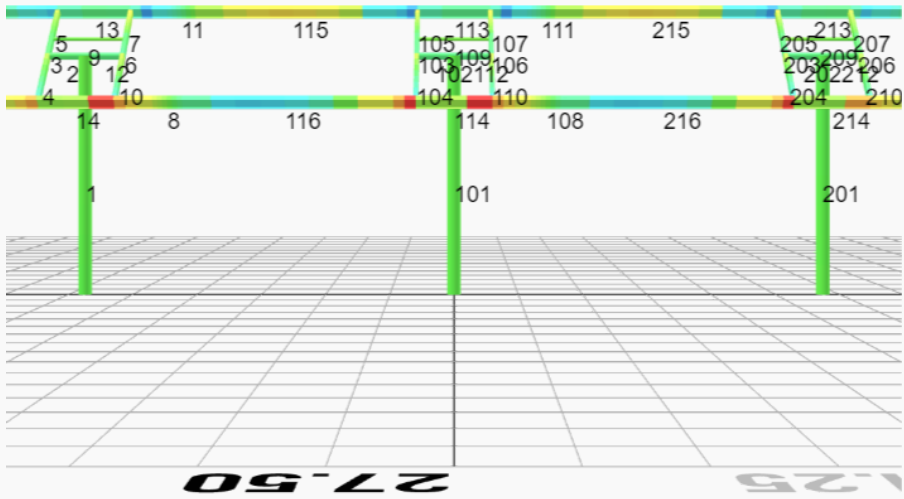
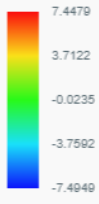
FEM Results (Envelope Worst Case for each member)



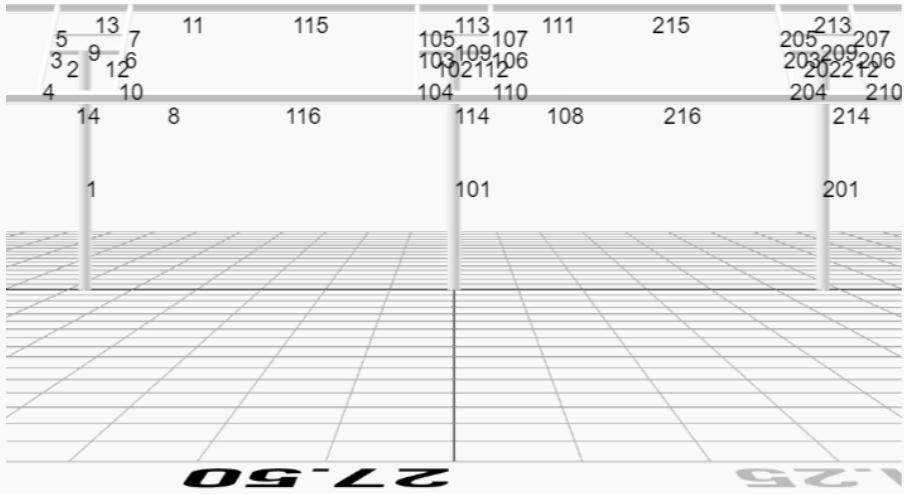
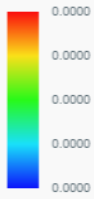
Top Bending Stress Z (ksi)



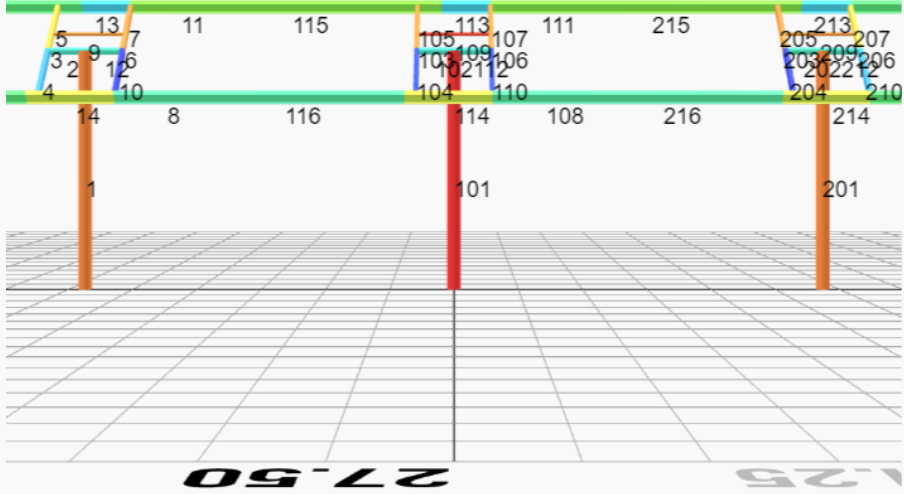
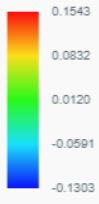
Top Bending Stress Y (ksi)



Shear Stress Y (ksi)



Axial Stress (ksi)



Reaction Forces for Foundation 1 (Node ID#1), (kip, kip-ft)

ASD Load Combination Results

Name	Fx	Fy	Fz	Mx	My	Mz
ULS: 1. D	0.0078	2.4836	0.0294	0.1131	-0.0126	-0.0680
ULS: 2. D + L	0.0078	2.4836	0.0294	0.1131	-0.0126	-0.0680
ULS: 3. D + (S or Lr or R)	0.0156	4.1876	0.0588	0.2260	-0.0255	-0.1561
ULS: 3. D + (S or Lr or R)	0.0078	2.4836	0.0294	0.1131	-0.0126	-0.0680
ULS: 4. D + 0.75L + 0.75(S or Lr or R)	0.0137	3.7616	0.0515	0.1978	-0.0223	-0.1341
ULS: 4. D + 0.75L + 0.75(S or Lr or R)	0.0078	2.4836	0.0294	0.1131	-0.0126	-0.0680
ULS: 5b. D + 0.7E	0.0078	2.4836	0.0294	0.1131	-0.0126	-0.0680
ULS: 6b. D + 0.75L + 0.75(0.7)E + 0.75S	0.0137	3.7616	0.0515	0.1978	-0.0223	-0.1341
ULS: 8. 0.6D + 0.7E	0.0047	1.4901	0.0177	0.0679	-0.0075	-0.0408
ULS: 5a. D + 0.6W_Wind downforce Case A only	-3.4525	6.2952	0.1387	0.5032	-0.5303	45.9726
ULS: 5a. D + 0.6W_Wind downforce Case B only	-3.4525	6.2952	0.1387	0.5032	-0.5303	45.9726
ULS: 5a. D + 0.6W_Wind uplift Case A only	2.6557	-0.4351	-0.0507	-0.1724	0.3671	-33.0764
ULS: 5a. D + 0.6W_Wind uplift Case B only	2.3034	-0.0407	-0.0488	-0.1654	0.3614	-36.2113
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind downforce Case A only	-2.5816	6.6203	0.1334	0.4904	-0.4106	34.3963
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind downforce Case B only	-2.5816	6.6203	0.1334	0.4904	-0.4106	34.3963
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind uplift Case A only	1.9995	1.5726	-0.0087	-0.0163	0.2625	-24.8904
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind uplift Case B only	1.7353	1.8684	-0.0072	-0.0111	0.2582	-27.2416
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind downforce Case A only	-2.5874	5.3423	0.1114	0.4057	-0.4009	34.4624
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind downforce Case B only	-2.5874	5.3423	0.1114	0.4057	-0.4009	34.4624
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind uplift Case A only	1.9937	0.2946	-0.0307	-0.1010	0.2722	-24.8243
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind uplift Case B only	1.7295	0.5903	-0.0292	-0.0958	0.2679	-27.1755
ULS: 7. 0.6D + 0.6W_Wind downforce Case A only	-3.4556	5.3018	0.1270	0.4579	-0.5253	45.9998
ULS: 7. 0.6D + 0.6W_Wind downforce Case B only	-3.4556	5.3018	0.1270	0.4579	-0.5253	45.9998
ULS: 7. 0.6D + 0.6W_Wind uplift Case A only	2.6525	-1.4285	-0.0625	-0.2176	0.3722	-33.0492
ULS: 7. 0.6D + 0.6W_Wind uplift Case B only	2.3002	-1.0342	-0.0606	-0.2107	0.3664	-36.1841

Worst Case Reactions LRFD

These calculations are taken directly from the FEA via SkyCiv and are used in the Concrete Checks of the Foundation Module.
Note: Worst case values are assumed as downforce wind load cases.

Result	Value (kip, kip-ft)
Axial	10.1862
Shear X	-5.7672
Shear Z	0.2336
Moment X	0.8478
Moment Y (Twist)	0.8904
Moment Z	77.4783

Worst Case Reactions ASD

These results are taken from the worst case values in the above table and are used in the Soil Checks in the Foundation Module.
Note: Worst case values are assumed as downforce wind load cases.

Result	Value (kip, kip-ft)
Axial	6.6203
Shear X	-3.4556
Shear Z	0.1387
Moment X	0.5032
Moment Y (Twist)	0.5303
Moment Z	45.9998

Reaction Forces for Foundation 2 (Node ID#101), (kip, kip-ft)

ASD Load Combination Results

Name	Fx	Fy	Fz	Mx	My	Mz
ULS: 1. D	-0.0156	2.7510	0.0000	0.0000	0.0000	0.2086
ULS: 2. D + L	-0.0156	2.7510	0.0000	0.0000	0.0000	0.2086
ULS: 3. D + (S or Lr or R)	-0.0312	4.7207	0.0000	0.0000	0.0000	0.3974
ULS: 3. D + (S or Lr or R)	-0.0156	2.7510	0.0000	0.0000	0.0000	0.2086
ULS: 4. D + 0.75L + 0.75(S or Lr or R)	-0.0273	4.2283	0.0000	0.0000	0.0000	0.3502
ULS: 4. D + 0.75L + 0.75(S or Lr or R)	-0.0156	2.7510	0.0000	0.0000	0.0000	0.2086
ULS: 5b. D + 0.7E	-0.0156	2.7510	0.0000	0.0000	0.0000	0.2086

Name	Fx	Fy	Fz	Mx	My	Mz
ULS: 6b. D + 0.75L + 0.75(0.7)E + 0.75S	-0.0273	4.2283	0.0000	0.0000	0.0000	0.3502
ULS: 8. 0.6D + 0.7E	-0.0094	1.6506	0.0000	0.0000	0.0000	0.1252
ULS: 5a. D + 0.6W_Wind downforce Case A only	-3.8985	7.1263	0.0000	0.0000	0.0000	51.5181
ULS: 5a. D + 0.6W_Wind downforce Case B only	-3.8985	7.1263	0.0000	0.0000	0.0000	51.5181
ULS: 5a. D + 0.6W_Wind uplift Case A only	2.9698	-0.6087	0.0000	0.0000	0.0000	-36.6019
ULS: 5a. D + 0.6W_Wind uplift Case B only	2.5322	-0.1289	0.0000	0.0000	0.0000	-39.6932
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind downforce Case A only	-2.9395	7.5097	0.0000	0.0000	0.0000	38.8324
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind downforce Case B only	-2.9395	7.5097	0.0000	0.0000	0.0000	38.8324
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind uplift Case A only	2.2117	1.7085	0.0000	0.0000	0.0000	-27.2576
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind uplift Case B only	1.8835	2.0683	0.0000	0.0000	0.0000	-29.5761
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind downforce Case A only	-2.9278	6.0325	0.0000	0.0000	0.0000	38.6907
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind downforce Case B only	-2.9278	6.0325	0.0000	0.0000	0.0000	38.6907
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind uplift Case A only	2.2234	0.2312	0.0000	0.0000	0.0000	-27.3993
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind uplift Case B only	1.8952	0.5911	0.0000	0.0000	0.0000	-29.7177
ULS: 7. 0.6D + 0.6W_Wind downforce Case A only	-3.8923	6.0259	0.0000	0.0000	0.0000	51.4347
ULS: 7. 0.6D + 0.6W_Wind downforce Case B only	-3.8923	6.0259	0.0000	0.0000	0.0000	51.4347
ULS: 7. 0.6D + 0.6W_Wind uplift Case A only	2.9760	-1.7091	0.0000	0.0000	0.0000	-36.6853
ULS: 7. 0.6D + 0.6W_Wind uplift Case B only	2.5384	-1.2293	0.0000	0.0000	0.0000	-39.7766

Worst Case Reactions LRFD

These calculations are taken directly from the FEA via SkyCiv and are used in the Concrete Checks of the Foundation Module.
Note: Worst case values are assumed as downforce wind load cases.

Result	Value (kip, kip-ft)
Axial	11.5758
Shear X	-6.4942
Shear Z	0.0000
Moment X	0.0002
Moment Y (Twist)	0.0001
Moment Z	86.8571

Worst Case Reactions ASD

These results are taken from the worst case values in the above table and are used in the Soil Checks in the Foundation Module.
Note: Worst case values are assumed as downforce wind load cases.

Result	Value (kip, kip-ft)
Axial	7.5097
Shear X	-3.8985
Shear Z	0.0000
Moment X	0.0000
Moment Y (Twist)	0.0000
Moment Z	51.5181

Reaction Forces for Foundation 3 (Node ID#201), (kip, kip-ft)

ASD Load Combination Results

Name	Fx	Fy	Fz	Mx	My	Mz
ULS: 1. D	0.0078	2.4836	-0.0294	-0.1131	0.0126	-0.0680
ULS: 2. D + L	0.0078	2.4836	-0.0294	-0.1131	0.0126	-0.0680
ULS: 3. D + (S or Lr or R)	0.0156	4.1876	-0.0588	-0.2260	0.0255	-0.1561
ULS: 3. D + (S or Lr or R)	0.0078	2.4836	-0.0294	-0.1131	0.0126	-0.0680
ULS: 4. D + 0.75L + 0.75(S or Lr or R)	0.0137	3.7616	-0.0515	-0.1978	0.0223	-0.1341
ULS: 4. D + 0.75L + 0.75(S or Lr or R)	0.0078	2.4836	-0.0294	-0.1131	0.0126	-0.0680
ULS: 5b. D + 0.7E	0.0078	2.4836	-0.0294	-0.1131	0.0126	-0.0680
ULS: 6b. D + 0.75L + 0.75(0.7)E + 0.75S	0.0137	3.7616	-0.0515	-0.1978	0.0223	-0.1341
ULS: 8. 0.6D + 0.7E	0.0047	1.4901	-0.0177	-0.0679	0.0075	-0.0408
ULS: 5a. D + 0.6W_Wind downforce Case A only	-3.4525	6.2952	-0.1387	-0.5032	0.5304	45.9726
ULS: 5a. D + 0.6W_Wind downforce Case B only	-3.4525	6.2952	-0.1387	-0.5032	0.5304	45.9726
ULS: 5a. D + 0.6W_Wind uplift Case A only	2.6557	-0.4351	0.0507	0.1724	-0.3671	-33.0764
ULS: 5a. D + 0.6W_Wind uplift Case B only	2.3034	-0.0407	0.0488	0.1654	-0.3614	-36.2113
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind downforce Case A only	-2.5816	6.6203	-0.1334	-0.4904	0.4106	34.3964
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind downforce Case B only	-2.5816	6.6203	-0.1334	-0.4904	0.4106	34.3964
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind uplift Case A only	1.9995	1.5726	0.0087	0.0163	-0.2625	-24.8903
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind uplift Case B only	1.7353	1.8684	0.0072	0.0111	-0.2582	-27.2416

Name	Fx	Fy	Fz	Mx	My	Mz
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind downforce Case A only	-2.5874	5.3423	-0.1114	-0.4057	0.4009	34.4624
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind downforce Case B only	-2.5874	5.3423	-0.1114	-0.4057	0.4009	34.4624
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind uplift Case A only	1.9937	0.2946	0.0307	0.1010	-0.2722	-24.8243
ULS: 6a. D + 0.75L + 0.75(0.6)W + 0.75(S or Lr or R)_Wind uplift Case B only	1.7295	0.5903	0.0292	0.0958	-0.2679	-27.1755
ULS: 7. 0.6D + 0.6W_Wind downforce Case A only	-3.4556	5.3018	-0.1270	-0.4580	0.5253	45.9998
ULS: 7. 0.6D + 0.6W_Wind downforce Case B only	-3.4556	5.3018	-0.1270	-0.4580	0.5253	45.9998
ULS: 7. 0.6D + 0.6W_Wind uplift Case A only	2.6525	-1.4285	0.0625	0.2176	-0.3722	-33.0492
ULS: 7. 0.6D + 0.6W_Wind uplift Case B only	2.3002	-1.0342	0.0606	0.2107	-0.3664	-36.1841

Worst Case Reactions LRFD

These calculations are taken directly from the FEA via SkyCiv and are used in the Concrete Checks of the Foundation Module.
Note: Worst case values are assumed as downforce wind load cases.

Result	Value (kip, kip-ft)
Axial	10.1862
Shear X	-5.7672
Shear Z	-0.2336
Moment X	-0.8479
Moment Y (Twist)	0.8905
Moment Z	77.4793

Worst Case Reactions ASD

These results are taken from the worst case values in the above table and are used in the Soil Checks in the Foundation Module.
Note: Worst case values are assumed as downforce wind load cases.

Result	Value (kip, kip-ft)
Axial	6.6203
Shear X	-3.4556
Shear Z	-0.1387
Moment X	-0.5032
Moment Y (Twist)	0.5304
Moment Z	45.9998

Project Details

Design Code: AISC 360-16 LRFD
 Provision: LRFD
 Country: United States
 User Name: sales@mtsolar.us
 Unit System: imperial

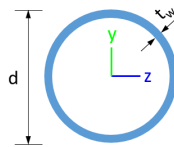


Design Input Information

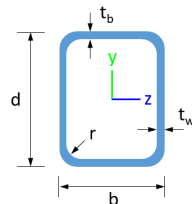
Design Factors			
Φ_t	Φ_c	Φ_b	Φ_v
0.9	0.9	0.9	0.9

Design Materials			
ID	E (ksi)	F_y (ksi)	F_u (ksi)
1	29000	50	65

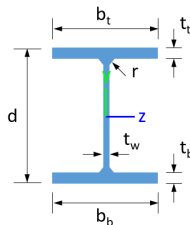
Section Dimensions



ID	Name	d (in)	t_w (in)				
2	2in Pipe Sch 80	2.38	0.22				
5	4in Pipe Sch 80	4.50	0.34				
10	8in Pipe Sch 80	8.63	0.50				



ID	Name	d (in)	b (in)	t_w (in)	t_b (in)	r (in)	
16	HSS5x3x3/16	5.00	3.00	0.17	0.17	0.17	



ID	Name	d (in)	t_w (in)	b_t (in)	b_b (in)	t_t (in)	t_b (in)	r (in)
19	W8x10	7.89	0.17	3.94	3.94	0.20	0.20	0.30

Section Properties

ID	Name	A (in ²)	J (in ⁴)	I_{yp} (in ⁴)	I_{zp} (in ⁴)	I_w (in ⁶)	S_{yp} (in ³)	S_{zp} (in ³)
2	2in Pipe Sch 80	1.48	1.74	0.87	0.87	0.00	1.02	1.02
5	4in Pipe Sch 80	4.41	19.22	9.61	9.61	0.00	5.85	5.85
10	8in Pipe Sch 80	12.76	211.43	105.72	105.72	0.00	33.05	33.05

108	19	1.33	1.33	2.0 5	2.08,2.08,2.08,2.08,2.08,2.08,2.06,2.06,1.98,1.41,2.06,2.06,2.01,1.77,2.07,2.07,1.40,2.09,2.0 6,2.06,1.91,2.27,2.06,2.06,2.03,1.89	3 0 0	2 0 0	1
109	2	2.60	2.60	4.0 0	-	3 0 0	2 0 0	1
110	16	2.44	2.44	3.7 5	1.68,1.68,1.68,1.67,1.68,1.68,1.67,1.67,1.66,1.60,1.67,1.67,1.66,1.64,1.67,1.67,1.78,1.68,1.6 7,1.67,1.65,1.75,1.67,1.67,1.66,1.65	3 0 0	2 0 0	1
111	19	1.33	1.33	2.0 5	2.07,2.07,2.07,2.07,2.07,2.07,1.69,1.69,1.51,1.55,1.67,1.67,1.56,1.59,1.79,1.79,1.33,1.17,1.7 2,1.72,1.43,1.51,1.66,1.66,1.59,1.60	3 0 0	2 0 0	1
112	5	1.30	1.30	2.0 0	-	3 0 0	2 0 0	1
113	19	4.88	4.00	7.5 0	1.04,1.04,1.04,1.04,1.04,1.04,1.05,1.05,1.05,1.06,1.05,1.05,1.05,1.05,1.04,1.04,1.02,1.82,1.0 4,1.04,1.06,1.06,1.05,1.05,1.05,1.05	3 0 0	2 0 0	1
114	19	4.88	4.00	7.5 0	1.04,1.04,1.04,1.04,1.04,1.04,1.04,1.04,1.04,1.02,1.04,1.04,1.04,1.03,1.04,1.04,1.02,1.04,1.0 4,1.04,1.04,1.91,1.04,1.04,1.04,1.03	3 0 0	2 0 0	1
115	19	6.63	6.63	10. 20	1.15,1.15,1.15,1.15,1.15,1.15,1.12,1.12,1.11,1.11,1.12,1.12,1.11,1.11,1.13,1.13,2.46,1.07,1.1 3,1.13,1.09,1.10,1.12,1.12,1.11,1.11	3 0 0	2 0 0	1
116	19	6.63	6.63	10. 20	1.16,1.16,1.16,1.16,1.16,1.16,1.15,1.15,1.14,1.10,1.15,1.15,1.14,1.13,1.15,1.15,2.27,1.16,1.1 5,1.15,1.14,1.21,1.15,1.15,1.14,1.14	3 0 0	2 0 0	1
201	10	26.8 2	26.8 2	12. 77	-	3 0 0	2 0 0	1
202	5	1.30	1.30	2.0 0	-	3 0 0	2 0 0	1
203	16	0.92	0.92	1.4 2	1.19,1.19,1.19,1.18,1.19,1.19,1.18,1.18,1.18,1.18,1.18,1.18,1.18,1.18,1.18,1.18,1.21,1.17,1.1 8,1.18,1.17,1.18,1.18,1.18,1.18,1.18	3 0 0	2 0 0	1
204	16	2.44	2.44	3.7 5	1.68,1.68,1.68,1.68,1.68,1.68,1.67,1.67,1.66,1.61,1.67,1.67,1.66,1.64,1.67,1.67,1.85,1.68,1.6 7,1.67,1.65,1.78,1.67,1.67,1.66,1.65	3 0 0	2 0 0	1
205	16	1.52	1.52	2.3 3	1.68,1.67,1.68,1.67,1.68,1.68,1.67,1.67,1.66,1.66,1.67,1.67,1.66,1.66,1.67,1.67,1.72,1.65,1.6 7,1.67,1.66,1.66,1.67,1.67,1.66,1.67	3 0 0	2 0 0	1
206	16	0.92	0.92	1.4 2	1.19,1.18,1.19,1.18,1.18,1.19,1.18,1.18,1.17,1.17,1.18,1.18,1.17,1.17,1.18,1.18,1.22,1.15,1.1 8,1.18,1.16,1.17,1.18,1.18,1.17,1.17	3 0 0	2 0 0	1
207	16	1.52	1.52	2.3 3	1.68,1.67,1.68,1.67,1.68,1.68,1.67,1.67,1.66,1.66,1.67,1.67,1.66,1.66,1.67,1.67,1.71,1.64,1.6 7,1.67,1.65,1.66,1.67,1.67,1.66,1.66	3 0 0	2 0 0	1
208	19	7.88	7.88	3.7 5	2.33,2.33,2.33,2.33,2.33,2.33,2.33,2.33,2.33,2.33,2.33,2.33,2.33,2.33,2.33,2.33,2.33,2.3 3,2.33,2.33,2.33,2.33,2.33,2.33,2.33	3 0 0	2 0 0	1
209	2	2.60	2.60	4.0 0	-	3 0 0	2 0 0	1
210	16	2.44	2.44	3.7 5	1.69,1.68,1.69,1.68,1.68,1.69,1.67,1.67,1.66,1.47,1.67,1.67,1.66,1.63,1.67,1.67,1.80,1.68,1.6 7,1.67,1.65,1.74,1.67,1.67,1.66,1.65	3 0 0	2 0 0	1
211	19	7.88	7.88	3.7 5	2.33,2.33,2.33,2.33,2.33,2.33,2.33,2.33,2.33,2.33,2.33,2.33,2.33,2.33,2.33,2.33,2.33,2.3 3,2.33,2.33,2.33,2.33,2.33,2.33,2.33	3 0 0	2 0 0	1
212	5	1.30	1.30	2.0 0	-	3 0 0	2 0 0	1
213	19	4.88	4.00	7.5 0	1.10,1.10,1.10,1.10,1.10,1.10,1.10,1.10,1.09,1.11,1.10,1.10,1.09,1.11,1.10,1.10,1.26,1.33,1.1 0,1.10,1.08,1.11,1.10,1.10,1.09,1.11	3 0 0	2 0 0	1
214	19	4.88	4.00	7.5 0	1.10,1.10,1.10,1.10,1.10,1.10,1.09,1.09,1.10,1.19,1.09,1.09,1.10,1.09,1.10,1.10,1.17,1.14,1.1 0,1.10,1.09,2.33,1.09,1.09,1.10,1.07	3 0 0	2 0 0	1
215	19	6.63	6.63	10. 20	1.13,1.13,1.13,1.13,1.13,1.13,1.14,1.14,1.14,1.14,1.14,1.14,1.14,1.14,1.13,1.13,1.41,1.20,1.1 3,1.13,1.14,1.14,1.14,1.14,1.14,1.14	3 0 0	2 0 0	1
216	19	6.63	6.63	10. 20	1.12,1.12,1.12,1.12,1.12,1.12,1.12,1.12,1.08,1.12,1.12,1.12,1.10,1.12,1.12,1.22,1.13,1.1 2,1.12,1.12,1.17,1.12,1.12,1.12,1.11	3 0 0	2 0 0	1

Member Design Capacity

Member Design Capacity

Member ID	$\Phi_t P_n$ (kip)	$\Phi_c P_n$ (kip)	$\Phi_b M_{zn}$ (k-ft)	$\Phi_b M_{yn}$ (k-ft)	$\Phi_v V_{yn}$ (kip)	$\Phi_v V_{zn}$ (kip)
1	574.32	230.19	123.94	123.94	172.30	172.30
2	198.33	196.72	21.95	21.95	59.50	59.50
3	116.10	115.41	15.79	11.10	42.08	23.28
4	116.10	111.33	15.79	11.10	42.08	23.28
5	116.10	114.23	15.79	11.10	42.08	23.28
6	116.10	115.41	15.79	11.10	42.08	23.28
7	116.10	114.23	15.79	11.10	42.08	23.28
8	133.20	126.01	32.87	6.12	40.24	43.62
9	66.48	58.89	3.82	3.82	19.94	19.94
10	116.10	111.33	15.79	11.10	42.08	23.28
11	133.20	126.01	32.87	6.12	40.24	43.62
12	198.33	196.72	21.95	21.95	59.50	59.50
13	133.20	104.94	24.75	6.12	40.24	43.62
14	133.20	104.94	24.52	6.12	40.24	43.62
15	133.20	52.83	32.87	6.12	40.24	43.62
16	133.20	52.83	32.87	6.12	40.24	43.62
101	574.32	230.19	123.94	123.94	172.30	172.30
102	198.33	196.72	21.95	21.95	59.50	59.50
103	116.10	115.41	15.79	11.10	42.08	23.28
104	116.10	111.33	15.79	11.10	42.08	23.28
105	116.10	114.23	15.79	11.10	42.08	23.28
106	116.10	115.41	15.79	11.10	42.08	23.28
107	116.10	114.23	15.79	11.10	42.08	23.28
108	133.20	126.01	32.87	6.12	40.24	43.62
109	66.48	58.89	3.82	3.82	19.94	19.94
110	116.10	111.33	15.79	11.10	42.08	23.28
111	133.20	126.01	32.87	6.12	40.24	43.62
112	198.33	196.72	21.95	21.95	59.50	59.50
113	133.20	104.94	23.37	6.12	40.24	43.62
114	133.20	104.94	23.37	6.12	40.24	43.62
115	133.20	69.16	16.56	6.12	40.24	43.62
116	133.20	69.16	17.02	6.12	40.24	43.62
201	574.32	230.19	123.94	123.94	172.30	172.30
202	198.33	196.72	21.95	21.95	59.50	59.50
203	116.10	115.41	15.79	11.10	42.08	23.28
204	116.10	111.33	15.79	11.10	42.08	23.28
205	116.10	114.23	15.79	11.10	42.08	23.28
206	116.10	115.41	15.79	11.10	42.08	23.28
207	116.10	114.23	15.79	11.10	42.08	23.28
208	133.20	52.83	32.87	6.12	40.24	43.62
209	66.48	58.89	3.82	3.82	19.94	19.94
210	116.10	111.33	15.79	11.10	42.08	23.28
211	133.20	52.83	32.87	6.12	40.24	43.62
212	198.33	196.72	21.95	21.95	59.50	59.50
213	133.20	104.94	24.75	6.12	40.24	43.62
214	133.20	104.94	24.52	6.12	40.24	43.62
215	133.20	69.16	17.49	6.12	40.24	43.62
216	133.20	69.16	16.71	6.12	40.24	43.62

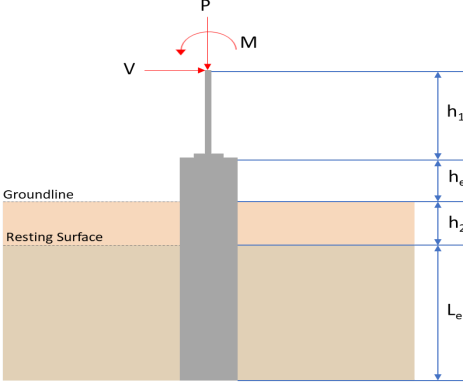
Design Ratio

Member ID	P	M _z	M _y	V _y	V _z	(P,M _z ,M _y)	Worst LC	KL/r	φ	Status
1	0.044	0.625	0.017	0.033	0.001	0.654	#13	0.559	Not Required	Pass
2	0.002	0.318	0.232	0.073	0.046	0.550	#13	0.035	Not Required	Pass
3	0.006	0.622	0.032	0.061	0.003	0.643	#13	0.045	Not Required	Pass
4	0.006	0.572	0.101	0.057	0.022	0.630	#13	0.080	Not Required	Pass
5	0.006	0.386	0.096	0.062	0.024	0.397	#13	0.074	Not Required	Pass
6	0.008	0.728	0.060	0.074	0.012	0.770	#13	0.045	Not Required	Pass
7	0.008	0.452	0.135	0.072	0.034	0.473	#13	0.074	Not Required	Pass
8	0.002	0.080	0.120	0.044	0.013	0.125	#24	0.095	Not Required	Pass
9	0.009	0.061	0.064	0.002	0.002	0.126	#13	0.204	Not Required	Pass
10	0.009	0.657	0.131	0.066	0.028	0.690	#13	0.080	Not Required	Pass
11	0.002	0.083	0.122	0.050	0.013	0.127	#24	0.095	Not Required	Pass
12	0.002	0.415	0.273	0.087	0.052	0.687	#13	0.053	Not Required	Pass
13	0.004	0.219	0.310	0.064	0.017	0.422	#21	0.286	Not Required	Pass
14	0.005	0.202	0.307	0.057	0.017	0.402	#21	0.190	Not Required	Pass
15	0.000	0.069	0.107	0.030	0.008	0.156	#21	Not Required	Not Required	Pass
16	0.000	0.064	0.107	0.028	0.008	0.154	#21	Not Required	Not Required	Pass
101	0.050	0.701	0.000	0.038	0.000	0.726	#13	0.559	Not Required	Pass
102	0.002	0.417	0.285	0.092	0.055	0.703	#13	0.035	Not Required	Pass
103	0.008	0.757	0.051	0.076	0.008	0.790	#13	0.045	Not Required	Pass
104	0.008	0.715	0.132	0.072	0.028	0.776	#13	0.080	Not Required	Pass
105	0.008	0.470	0.137	0.075	0.034	0.494	#13	0.074	Not Required	Pass
106	0.008	0.757	0.051	0.076	0.008	0.790	#13	0.045	Not Required	Pass
107	0.008	0.470	0.137	0.075	0.034	0.494	#13	0.074	Not Required	Pass
108	0.002	0.068	0.125	0.046	0.013	0.149	#21	0.095	Not Required	Pass
109	0.011	0.053	0.054	0.001	0.000	0.110	#13	0.204	Not Required	Pass
110	0.008	0.715	0.132	0.072	0.028	0.776	#13	0.080	Not Required	Pass
111	0.002	0.090	0.127	0.048	0.013	0.141	#21	0.095	Not Required	Pass
112	0.002	0.417	0.285	0.092	0.055	0.703	#13	0.035	Not Required	Pass
113	0.005	0.200	0.316	0.062	0.017	0.454	#21	0.286	Not Required	Pass
114	0.006	0.223	0.314	0.059	0.017	0.463	#21	0.286	Not Required	Pass
115	0.003	0.309	0.168	0.048	0.013	0.420	#13	0.473	Not Required	Pass
116	0.002	0.273	0.170	0.046	0.013	0.381	#13	0.473	Not Required	Pass
201	0.044	0.625	0.017	0.033	0.001	0.654	#13	0.559	Not Required	Pass
202	0.002	0.415	0.273	0.087	0.052	0.687	#13	0.053	Not Required	Pass
203	0.008	0.728	0.060	0.074	0.012	0.770	#13	0.045	Not Required	Pass
204	0.009	0.657	0.131	0.066	0.028	0.690	#13	0.080	Not Required	Pass
205	0.008	0.452	0.135	0.072	0.034	0.473	#13	0.074	Not Required	Pass
206	0.006	0.622	0.032	0.061	0.003	0.643	#13	0.045	Not Required	Pass
207	0.006	0.386	0.096	0.062	0.024	0.397	#13	0.074	Not Required	Pass
208	0.000	0.064	0.107	0.028	0.008	0.154	#21	Not Required	Not Required	Pass
209	0.009	0.061	0.064	0.002	0.002	0.126	#13	0.204	Not Required	Pass
210	0.006	0.572	0.101	0.057	0.022	0.630	#13	0.080	Not Required	Pass
211	0.000	0.069	0.107	0.030	0.008	0.156	#21	Not Required	Not Required	Pass
212	0.002	0.318	0.232	0.073	0.046	0.550	#13	0.035	Not Required	Pass
213	0.004	0.219	0.309	0.064	0.017	0.422	#21	0.190	Not Required	Pass
214	0.005	0.202	0.307	0.057	0.017	0.402	#21	0.286	Not Required	Pass
215	0.003	0.315	0.169	0.050	0.013	0.414	#13	0.473	Not Required	Pass
216	0.002	0.281	0.169	0.044	0.013	0.385	#13	0.473	Not Required	Pass

Definitions

Φ_t Safety factor for tensile

Φ_c	Safety factor for compression
Φ_b	Safety factor for flexure
Φ_v	Safety factor for shear
E	Modulus of elasticity
F_y	Specified minimum yield stress
F_u	Specified minimum tensile strength
A	Cross-sectional area
J	Torsional constant
I_{yp}	Moment of inertia about the Y axes
I_{zp}	Moment of inertia about the Z axes
I_w	Warping constant
S_{yp}	Plastic section modulus about the Y axis
S_{zp}	Plastic section modulus about the Z axis
KL	Effective length
C_b	Buckling modification factor (from all load combinations)
L_b	Length between braced points
LST	Limited slenderness for tension
LSC	Limited slenderness for compression
LD	Limited deflection
P_n	Nominal axial strength (tension/compression)
M_n	Nominal flexural strength (about Z/Y axis)
V_n	Nominal shear strength (along Z/Y axis)
P	Design ratio in case of axial force
M_z	Design ratio in case of bending about Z axis
M_y	Design ratio in case of bending about Y axis
V_y	Design ratio in case of shear along Y axis
V_z	Design ratio in case of shear along Z axis
(P, M_z , M_y)	Design ratio in case of axial force and bending action
KL/r	Design ratio in case of section slenderness
δ	Design ratio in case of member deflection
OK	Capacity is provided
NG	Capacity is not provided

REFERENCES	CALCULATIONS	RESULTS																										
	<p>SkyCiv Foundation Design Pile Foundation</p> <p>Design Information : Design code : IBC 2021 (International Building Code) Unit System : Imperial</p>																											
	<p>Pile Input</p>  <p>Geometry Pile shape: rectangular $b = 48$ in - Pile width $D = 48$ in - Pile depth $L = 7.5$ ft - Total pile length $h_1 = 0$ ft - Lateral load height from the top of the pile, $h_2 = 0$ ft - Depth to resting surface $h_e = 0$ ft - Length of pile above the ground</p> <p>Tabulation of Soil Parameters</p> <table border="1" data-bbox="416 1102 1193 1191"> <thead> <tr> <th>Layer</th> <th>Label</th> <th>Allowable Bearing Pressure (q_a) (psf)</th> <th>Allowable Lateral Pressure (R) (psf/ft)</th> </tr> </thead> <tbody> <tr> <td>1</td> <td>Sand, silty sand, clayey sand, silty gravel & clayey gravel</td> <td>2000.000</td> <td>150.000</td> </tr> </tbody> </table> <p>Tabulation of Loads</p> <table border="1" data-bbox="676 1285 933 1458"> <thead> <tr> <th>Load Component</th> <th>ASD</th> <th>LRFD</th> </tr> </thead> <tbody> <tr> <td>P (kip)</td> <td>6.620</td> <td>10.186</td> </tr> <tr> <td>V_x (kip)</td> <td>-3.456</td> <td>-5.767</td> </tr> <tr> <td>V_z (kip)</td> <td>0.139</td> <td>0.234</td> </tr> <tr> <td>M_x (kipft)</td> <td>0.503</td> <td>0.848</td> </tr> <tr> <td>M_z (kipft)</td> <td>46.000</td> <td>77.478</td> </tr> </tbody> </table> <p>Material Properties $f'_{ck} = 3$ ksi - Concrete strength,</p>	Layer	Label	Allowable Bearing Pressure (q_a) (psf)	Allowable Lateral Pressure (R) (psf/ft)	1	Sand, silty sand, clayey sand, silty gravel & clayey gravel	2000.000	150.000	Load Component	ASD	LRFD	P (kip)	6.620	10.186	V_x (kip)	-3.456	-5.767	V_z (kip)	0.139	0.234	M_x (kipft)	0.503	0.848	M_z (kipft)	46.000	77.478	
Layer	Label	Allowable Bearing Pressure (q_a) (psf)	Allowable Lateral Pressure (R) (psf/ft)																									
1	Sand, silty sand, clayey sand, silty gravel & clayey gravel	2000.000	150.000																									
Load Component	ASD	LRFD																										
P (kip)	6.620	10.186																										
V_x (kip)	-3.456	-5.767																										
V_z (kip)	0.139	0.234																										
M_x (kipft)	0.503	0.848																										
M_z (kipft)	46.000	77.478																										
	<p>Required depth to resist lateral loads (ASD) H - Point of application of the lateral load</p> $H = h_1 + h_2 + h_e$ $H = (0 \text{ ft}) + (0 \text{ ft}) + (0 \text{ ft})$ $H = 0 \text{ ft}$ <p>Considering x-direction: H_o - Lateral force per length of pile,</p> $H_o = \frac{V_x}{1.57 D}$ $H_o = \frac{(-3.456 \text{ kip})}{1.57 \times (48 \text{ in})}$ $H_o = -0.55032 \text{ kip/ft}$ <p>M_o - Moment per length of pile,</p> $M_o = \frac{M_z + (V_x H)}{1.57 D}$																											

$$M_o = \frac{(46 \text{ kipft}) + ((-3.456 \text{ kip}) \times (0 \text{ ft}))}{1.57 \times (48 \text{ in})}$$

$$M_o = 7.3248 \text{ kipft/ft}$$

Required depth of embedment in earth:

$$L_x^3 - \left(14.14 \times \frac{H_o \times L_x}{R}\right) - \left(18.85 \times \frac{M_o}{R}\right) = 0$$

Solving the cubic equation:

$L_{e,x} = 7.0653 \text{ ft}$ - Required depth in x-direction,

Considering z-direction:

H_o - Lateral force per length of pile,

$$H_o = \frac{V_z}{1.57 b}$$

$$H_o = \frac{(0.139 \text{ kip})}{1.57 \times (48 \text{ in})}$$

$$H_o = 0.022134 \text{ kip/ft}$$

M_o - Moment per length of pile,

$$M_o = \frac{M_x + (V_z H)}{1.57 b}$$

$$M_o = \frac{(0.503 \text{ kipft}) + ((0.139 \text{ kip}) \times (0 \text{ ft}))}{1.57 \times (48 \text{ in})}$$

$$M_o = 0.080096 \text{ kipft/ft}$$

Required depth of embedment in earth:

$$L_z^3 - \left(14.14 \times \frac{H_o \times L_z}{R}\right) - \left(18.85 \times \frac{M_o}{R}\right) = 0$$

Solving the cubic equation:

$L_{e,z} = 2.0946 \text{ ft}$ - Required depth in z-direction,

Minimum embedded depth required:

$L_{e,req}$ - Depth of pile required,

$$L_{e,req} = \text{MAX}[L_{e,x}, L_{e,z}]$$

$$L_{e,req} = \text{MAX}[(7.0653 \text{ ft}), (2.0946 \text{ ft})]$$

$$L_{e,req} = 7.065 \text{ ft}$$

L_e - Actual embedded length of pile,

$$L_e = L - h_c - h_2$$

$$L_e = (7.5 \text{ ft}) - (0 \text{ ft}) - (0 \text{ ft})$$

$$L_e = 7.5 \text{ ft}$$

Ratio - Embedded depth

$$\text{Ratio} = \frac{L_{e,req}}{L_e}$$

$$\text{Ratio} = \frac{(7.065 \text{ ft})}{(7.5 \text{ ft})}$$

$$\text{Ratio} = 0.942$$

Status: **PASS**
Ratio: **0.940**

End-bearing Capacity (ASD)

A - Pile cross-section area

$$A = b D$$

$$A = (48 \text{ in}) \times (48 \text{ in})$$

$$A = 16 \text{ ft}^2$$

q - End-bearing pressure

$$q = \frac{P_c}{A}$$

$$q = \frac{(6.62 \text{ kip})}{(16 \text{ ft}^2)}$$

$$q = 0.41375 \text{ kip/ft}^2$$

$$q = 0.41375 \text{ kip/ft}$$

Check bearing capacity ratio:

Ratio - Capacity

$$\text{Ratio} = \frac{q}{q_a}$$

$$\text{Ratio} = \frac{(0.41375 \text{ kip/ft}^2)}{(2000 \text{ psf})}$$

$$\text{Ratio} = 0.20688$$

Status: **PASS**
Ratio: **0.210**

Czerniak

Lateral Soil Pressure (ASD):

L/D - Length to least lateral dimension ratio,

$$L/D = \frac{L}{D}$$

$$L/D = \frac{(7.5 \text{ ft})}{(48 \text{ in})}$$

$$L/D = 1.875$$

Since $L/D \leq 10$,

Pile is short.

Considering x-direction:

$H_o = -0.55032 \text{ kip/ft}$ - Lateral force per length of pile,

$M_o = 7.3248 \text{ kipft/ft}$ - Overturning moment per length of pile,

a - Distance from resting surface to pivot point,

$$a = \frac{(4 M_o L_e) + (3 H_o L_e^2)}{(6 M_o) + (4 H_o L_e)}$$

$$a = \frac{(4 \times (7.3248 \text{ kipft/ft}) \times (7.5 \text{ ft})) + (3 \times (-0.55032 \text{ kip/ft}) \times (7.5 \text{ ft})^2)}{(6 \times (7.3248 \text{ kipft/ft})) + (4 \times (-0.55032 \text{ kip/ft}) \times (7.5 \text{ ft}))}$$

$$a = 5.1707 \text{ ft}$$

p - Earth pressure against the pile at distance $a/2$ from resting surface,

$$p = \frac{0.75 [(4 M_o) + (3 H_o L_e)]^2}{L_e^2 [(3 M_o) + (2 H_o L_e)]}$$

$$p = \frac{0.75 [(4 \times (7.3248 \text{ kipft/ft})) + (3 \times (-0.55032 \text{ kip/ft}) \times (7.5 \text{ ft}))]^2}{(7.5 \text{ ft})^2 [(3 \times (7.3248 \text{ kipft/ft})) + (2 \times (-0.55032 \text{ kip/ft}) \times (7.5 \text{ ft}))]}$$

$$p = 0.27813 \text{ kip/ft}^2$$

s - Earth pressure against the pile at distance L_e ,

$$s = \frac{6 [(2 M_o) + (H_o L_e)]}{L_e^2}$$

$$s = \frac{6 \times [(2 \times (7.3248 \text{ kipft/ft})) + ((-0.55032 \text{ kip/ft}) \times (7.5 \text{ ft}))]}{(7.5 \text{ ft})^2}$$

$$s = 1.1224 \text{ kip/ft}^2$$

Check lateral soil pressure capacity:

p_a - Allowable lateral soil pressure at depth $a/2$,

$$p_a = R \frac{a}{2}$$

$$p_a = (150 \text{ psf/ft}) \times \frac{(5.1707 \text{ ft})}{2}$$

$$p_a = 0.3878 \text{ kip/ft}^2$$

Ratio - Lateral soil capacity

$$\text{Ratio} = \frac{p}{p_a}$$

$$\text{Ratio} = \frac{(0.27813 \text{ kip/ft}^2)}{(0.3878 \text{ kip/ft}^2)}$$

$$\text{Ratio} = 0.7172$$

p_a - Allowable lateral soil pressure at depth L_e ,

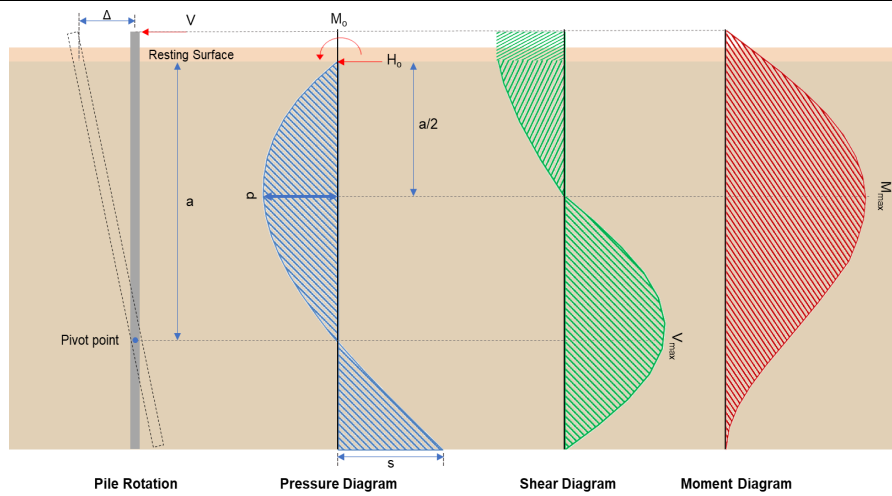
Status: **PASS**
Ratio: **0.720**

	$p_s = R L_e$ $p_s = (150 \text{ psf/ft}) \times (7.5 \text{ ft})$ $p_s = 1.125 \text{ kip/ft}^2$ <p>Ratio - Lateral soil capacity</p> $\text{Ratio} = \frac{s}{p_s}$ $\text{Ratio} = \frac{(1.1224 \text{ kip/ft}^2)}{(1.125 \text{ kip/ft}^2)}$ $\text{Ratio} = 0.99767$	<p>Status: PASS Ratio: 1.000</p>
	<p>Considering z-direction:</p> <p>$H_o = 0.022134 \text{ kip/ft}$ - Lateral force per length of pile, $M_o = 0.080096 \text{ kipft/ft}$ - Overturning moment per length of pile, a - Distance from resting surface to pivot point,</p> $a = \frac{(4 M_o L_e) + (3 H_o L_e^2)}{(6 M_o) + (4 H_o L_e)}$ $a = \frac{(4 \times (0.080096 \text{ kipft/ft}) \times (7.5 \text{ ft})) + (3 \times (0.022134 \text{ kip/ft}) \times (7.5 \text{ ft})^2)}{(6 \times (0.080096 \text{ kipft/ft})) + (4 \times (0.022134 \text{ kip/ft}) \times (7.5 \text{ ft}))}$ $a = 5.3626 \text{ ft}$ <p>p - Earth pressure against the pile at distance $a/2$ from resting surface,</p> $p = \frac{0.75 [(4 M_o) + (3 H_o L_e)]^2}{L_e^2 [(3 M_o) + (2 H_o L_e)]}$ $p = \frac{0.75 [(4 \times (0.080096 \text{ kipft/ft})) + (3 \times (0.022134 \text{ kip/ft}) \times (7.5 \text{ ft}))]^2}{(7.5 \text{ ft})^2 [(3 \times (0.080096 \text{ kipft/ft})) + (2 \times (0.022134 \text{ kip/ft}) \times (7.5 \text{ ft}))]}$ $p = 0.015604 \text{ kip/ft}^2$ <p>s - Earth pressure against the pile at distance L_e,</p> $s = \frac{6 [(2 M_o) + (H_o L_e)]}{L_e^2}$ $s = \frac{6 [(2 \times (0.080096 \text{ kipft/ft})) + ((0.022134 \text{ kip/ft}) \times (7.5 \text{ ft}))]}{(7.5 \text{ ft})^2}$ $s = 0.034794 \text{ kip/ft}^2$ <p>Check lateral soil pressure capacity:</p> <p>p_a - Allowable lateral soil pressure at depth $a/2$,</p> $p_a = R \frac{a}{2}$ $p_a = (150 \text{ psf/ft}) \times \frac{(5.3626 \text{ ft})}{2}$ $p_a = 0.40219 \text{ kip/ft}^2$ <p>Ratio - Lateral soil capacity</p> $\text{Ratio} = \frac{p}{p_a}$ $\text{Ratio} = \frac{(0.015604 \text{ kip/ft}^2)}{(0.40219 \text{ kip/ft}^2)}$ $\text{Ratio} = 0.038798$ <p>p_s - Allowable lateral soil pressure at depth L_e,</p> $p_s = R L_e$ $p_s = (150 \text{ psf/ft}) \times (7.5 \text{ ft})$ $p_s = 1.125 \text{ kip/ft}^2$ <p>Ratio - Lateral soil capacity</p> $\text{Ratio} = \frac{s}{p_s}$	<p>Status: PASS Ratio: 0.040</p>

$$Ratio = \frac{(0.034794 \text{ kip/ft}^2)}{(1.125 \text{ kip/ft}^2)}$$

$$Ratio = 0.030928$$

Status: **PASS**
Ratio: **0.030**



Shear force and Bending moment (x-direction, LRFD)

H_o - Lateral force per length of pile,

$$H_o = \frac{V_x}{1.57 D}$$

$$H_o = \frac{(-5.767 \text{ kip})}{1.57 \times (48 \text{ in})}$$

$$H_o = -0.91831 \text{ kip/ft}$$

M_o - Moment per length of pile,

$$M_o = \frac{M_x + (V_x H)}{1.57 D}$$

$$M_o = \frac{(77.478 \text{ kipft}) + ((-5.767 \text{ kip}) \times (0 \text{ ft}))}{1.57 \times (48 \text{ in})}$$

$$M_o = 12.337 \text{ kipft/ft}$$

E - Distance from lateral load to resisting surface,

$$E = \frac{M_o}{H_o}$$

$$E = \frac{(12.337 \text{ kipft/ft})}{(-0.91831 \text{ kip/ft})}$$

$$E = 13.435 \text{ ft}$$

a - Distance from resting surface to pivot point,

$$a = \frac{(4 M_o L_c) + (3 H_o L_c^2)}{(6 M_o) + (4 H_o L_c)}$$

$$a = \frac{(4 \times (12.337 \text{ kipft/ft}) \times (7.5 \text{ ft})) + (3 \times (-0.91831 \text{ kip/ft}) \times (7.5 \text{ ft})^2)}{(6 \times (12.337 \text{ kipft/ft})) + (4 \times (-0.91831 \text{ kip/ft}) \times (7.5 \text{ ft}))}$$

$$a = 5.1695 \text{ ft}$$

V_{max} - Max shear force located at depth a ,

$$V_{max} = (H_o D) \left[1 - \left[3 \left(\frac{4 E}{L_c} + 3 \right) \left(\frac{a}{L_c} \right)^2 \right] + \left[4 \left(\frac{3 E}{L_c} + 2 \right) \left(\frac{a}{L_c} \right)^3 \right] \right]$$

$$V_{max} = ((-0.91831 \text{ kip/ft}) \times (48 \text{ in})) \times \left[1 - \left[3 \times \left(\frac{4 \times (13.435 \text{ ft})}{(7.5 \text{ ft})} + 3 \right) \times \left(\frac{(5.1695 \text{ ft})}{(7.5 \text{ ft})} \right)^2 \right] + \left[4 \times \left(\frac{3 \times (13.435 \text{ ft})}{(7.5 \text{ ft})} + 2 \right) \times \left(\frac{(5.1695 \text{ ft})}{(7.5 \text{ ft})} \right)^3 \right] \right]$$

$$V_{max} = 14.066 \text{ kip}$$

M_{max} - Max bending moment located at depth $a/2$,

$$M_{max} = (H_o D L_e) \left[\left(\frac{E}{L_e} + \frac{a}{2 L_e} \right) - \left[\left(\frac{4E}{L_e} + 3 \right) \left(\frac{a}{2 L_e} \right)^3 + \left[\left(\frac{3E}{L_e} + 2 \right) \left(\frac{a}{2 L_e} \right)^4 \right] \right]$$

$$M_{max} = ((-0.91831 \text{ kip/ft}) \times (48 \text{ in}) \times (7.5 \text{ ft})) \times \left[\left(\frac{(13.435 \text{ ft})}{(7.5 \text{ ft})} + \frac{(5.1695 \text{ ft})}{2 \times (7.5 \text{ ft})} \right) - \left[\left(\frac{4 \times (13.435 \text{ ft})}{(7.5 \text{ ft})} + 3 \right) \times \left(\frac{(5.1695 \text{ ft})}{2 \times (7.5 \text{ ft})} \right)^3 + \left[\left(\frac{3 \times (13.435 \text{ ft})}{(7.5 \text{ ft})} + 2 \right) \times \left(\frac{(5.1695 \text{ ft})}{2 \times (7.5 \text{ ft})} \right)^4 \right] \right]$$

$$M_{max} = 50.246 \text{ kipft}$$

Shear force and Bending moment (z-direction, LRFD)

H_o - Lateral force per length of pile,

$$H_o = \frac{V_z}{1.57 b}$$

$$H_o = \frac{(0.234 \text{ kip})}{1.57 \times (48 \text{ in})}$$

$$H_o = 0.037261 \text{ kip/ft}$$

M_o - Moment per length of pile,

$$M_o = \frac{M_x + (V_z H)}{1.57 b}$$

$$M_o = \frac{(0.848 \text{ kipft}) + ((0.234 \text{ kip}) \times (0 \text{ ft}))}{1.57 \times (48 \text{ in})}$$

$$M_o = 0.13503 \text{ kipft/ft}$$

E - Distance from lateral load to resisting surface,

$$E = \frac{M_o}{H_o}$$

$$E = \frac{(0.13503 \text{ kipft/ft})}{(0.037261 \text{ kip/ft})}$$

$$E = 3.6239 \text{ ft}$$

a - Distance from resting surface to pivot point,

$$a = \frac{(4 M_o L_e) + (3 H_o L_e^2)}{(6 M_o) + (4 H_o L_e)}$$

$$a = \frac{(4 \times (0.13503 \text{ kipft/ft}) \times (7.5 \text{ ft})) + (3 \times (0.037261 \text{ kip/ft}) \times (7.5 \text{ ft})^2)}{(6 \times (0.13503 \text{ kipft/ft})) + (4 \times (0.037261 \text{ kip/ft}) \times (7.5 \text{ ft}))}$$

$$a = 5.3624 \text{ ft}$$

V_{max} - Max shear force located at depth a ,

$$V_{max} = (H_o b) \left[1 - \left[3 \left(\frac{4E}{L_e} + 3 \right) \left(\frac{a}{L_e} \right)^2 + 4 \left(\frac{3E}{L_e} + 2 \right) \left(\frac{a}{L_e} \right)^3 \right] \right]$$

$$V_{max} = ((0.037261 \text{ kip/ft}) \times (48 \text{ in})) \times \left[1 - \left[3 \times \left(\frac{4 \times (3.6239 \text{ ft})}{(7.5 \text{ ft})} + 3 \right) \times \left(\frac{(5.3624 \text{ ft})}{(7.5 \text{ ft})} \right)^2 + 4 \times \left(\frac{3 \times (3.6239 \text{ ft})}{(7.5 \text{ ft})} + 2 \right) \times \left(\frac{(5.3624 \text{ ft})}{(7.5 \text{ ft})} \right)^3 \right] \right]$$

$$V_{max} = 0.22679 \text{ kip}$$

M_{max} - Max bending moment located at depth $a/2$,

$$M_{max} = (H_o b L_e) \left[\left(\frac{E}{L_e} + \frac{a}{2 L_e} \right) - \left[\left(\frac{4E}{L_e} + 3 \right) \left(\frac{a}{2 L_e} \right)^3 + \left[\left(\frac{3E}{L_e} + 2 \right) \left(\frac{a}{2 L_e} \right)^4 \right] \right]$$

$$M_{max} = ((0.037261 \text{ kip/ft}) \times (48 \text{ in}) \times (7.5 \text{ ft})) \times \left[\left(\frac{(3.6239 \text{ ft})}{(7.5 \text{ ft})} + \frac{(5.3624 \text{ ft})}{2 \times (7.5 \text{ ft})} \right) - \left[\left(\frac{4 \times (3.6239 \text{ ft})}{(7.5 \text{ ft})} + 3 \right) \times \left(\frac{(5.3624 \text{ ft})}{2 \times (7.5 \text{ ft})} \right)^3 + \left[\left(\frac{3 \times (3.6239 \text{ ft})}{(7.5 \text{ ft})} + 2 \right) \times \left(\frac{(5.3624 \text{ ft})}{2 \times (7.5 \text{ ft})} \right)^4 \right] \right]$$

$$M_{max} = 0.7508 \text{ kipft}$$

Minimum Reinforcement Check (LRFD)

Parameters:

$f'_{ck} = 3 \text{ ksi}$ - Concrete strength,
 $f_{yk} = 60 \text{ ksi}$ - Longitudinal reinforcement strength,
 $\phi = 0.65$ - Reduction factor for axial strength,
 $\alpha = 0.8$ - Alpha factor for axial strength,
 $A_g = 2304 \text{ in}^2$ - Gross area of concrete,

Table 22.4.2.1

Longitudinal reinforcement:

Required reinforcement due to axial load, $A_{st,required}$

22.4.2.2, 10.6.1.1

$A_{st,required}$

$$A_{st,required} = \text{Min} \left[\frac{\frac{P}{\phi \alpha} - (0.85 f'_{ck} A_g)}{f_{yk} - (0.85 f'_{ck})}, (0.08 A_g) \right]$$

$$A_{st,required} = \text{Min} \left[\frac{\frac{(10.186 \text{ kip})}{(0.65) \times (0.8)} - (0.85 \times (3 \text{ ksi}) \times (2304 \text{ in}^2))}{(60 \text{ ksi}) - (0.85 \times (3 \text{ ksi}))}, (0.08 \times (2304 \text{ in}^2)) \right]$$

$$A_{st,required} = -101.93 \text{ in}^2$$

A_{min} - Governing minimum reinforcement area,

$$A_{min} = \text{Max} [A_{st,required}, (0.0018 A_g)]$$

$$A_{min} = \text{Max} [(-101.93 \text{ in}^2), (0.0018 \times (2304 \text{ in}^2))]$$

$$A_{min} = 4.1472 \text{ in}^2$$

n_{rebar} - Required number of reinforcement,

$$n_{rebar} = \frac{A_{min}}{A_{rebar}}$$

$$n_{rebar} = \frac{(4.1472 \text{ in}^2)}{(0.3068 \text{ in}^2)}$$

$$n_{rebar} = 14$$

A_{st} - Actual total reinforcement area,

$$A_{st} = n_{rebar} \frac{\pi d_{bar}^2}{4}$$

$$A_{st} = (14) \times \frac{\pi \times (0.625 \text{ in})^2}{4}$$

$$A_{st} = 4.2951 \text{ in}^2$$

Ratio - Capacity

$$\text{Ratio} = \frac{A_{min}}{A_{st}}$$

$$\text{Ratio} = \frac{(4.1472 \text{ in}^2)}{(4.2951 \text{ in}^2)}$$

$$\text{Ratio} = 0.96556$$

Status: **PASS**
Ratio: **0.970**

25.2.3

s_{rebar} - Minimum spacing of reinforcement,

$$s_{rebar} = \text{Max} [1.5, (1.5 d_{bar})]$$

$$s_{rebar} = \text{Max} [1.5, (1.5 \times (0.625 \text{ in}))]$$

$$s_{rebar} = 1.5 \text{ in}$$

Ties:

25.7.2.2 Since longitudinal reinforcement is \leq No. 10: Use #3(0.375 in)

25.7.2.1 s_{ties} - Maximum spacing of ties,

$$s_{ties} = \text{Min} [(16 d_{bar}), (48 d_{ties}), \text{Min} (D, b)]$$

$$s_{ties} = \text{Min} [(16 \times (0.625 \text{ in})), (48 \times (0.375 \text{ in})), \text{Min} ((48 \text{ in}), (48 \text{ in}))]$$

$$s_{ties} = 10 \text{ in}$$

Summary:

Main reinforcement: **14 - #5 (0.625 in)**

Ties: #3(0.375 in) - 10 in

Axial Compression Strength (ACI 318-19, LRFD)

22.4.2.2

ϕP_N - Allowable axial compressive strength

$$\phi P_N = \phi 0.80 [(0.85 f'_{ck} [A_g - A_{st}]) + (f_{yk} A_{st})]$$

$$\phi P_N = (0.65) \times 0.80 \times [(0.85 \times (3 \text{ ksi}) \times [(2304 \text{ in}^2) - (4.2951 \text{ in}^2)]) + ((60 \text{ ksi}) \times (4.2951 \text{ in}^2))]$$

$$\phi P_N = 3183.4 \text{ kip}$$

Ratio - Capacity

$$\text{Ratio} = \frac{P}{\phi P_N}$$

$$\text{Ratio} = \frac{(10.186 \text{ kip})}{(3183.4 \text{ kip})}$$

$$\text{Ratio} = 0.0031997$$

Status: **PASS**
Ratio: **0.000**

Shear Strength (ACI 318-19, LRFD)

Parameters:

22.5.2.2

$b_w = 48 \text{ in}$ - Effective width,
 d - Effective depth

$$d = 0.80 D$$

$$d = 0.80 \times (48 \text{ in})$$

$$d = 38.4 \text{ in}$$

22.5.5.1.3

λ_s - size effect modification factor

$$\lambda_s = \text{MIN} \left[\sqrt{\frac{2}{1 + \frac{d}{10}}}, 1 \right]$$

$$\lambda_s = \text{MIN} \left[\sqrt{\frac{2}{1 + \frac{(38.4 \text{ in})}{10}}}, 1 \right]$$

$$\lambda_s = 0.64282$$

22.5.5.1.1

The following variables were converted to be consistent with empirical formula $f'_{ck} = 3 \text{ ksi} \rightarrow 3000 \text{ psi}$,
 $V_{c,max}$ - Max shear strength of concrete

$$V_{c,max} = 5 \lambda_s \sqrt{f'_{ck}} b_w d$$

$$V_{c,max} = 5 \times (0.64282) \times \sqrt{(3000 \text{ psi})} \times (48 \text{ in}) \times (38.4 \text{ in})$$

$$V_{c,max} = 324.49 \text{ kip}$$

22.5.5.1.1(a)

The following variables were converted to be consistent with empirical formula $f'_{ck} = 3 \text{ ksi} \rightarrow 3000 \text{ psi}$, $P = 10.186 \text{ kip} \rightarrow 10186 \text{ lbf}$,
 $V_{c,a}$ - Shear strength of concrete (a)

$$V_{c,a} = \left[2 \lambda_s \sqrt{f'_{ck}} + \frac{P}{6 A_g} \right] b_w d$$

$$V_{c,a} = \left[2 \times (0.64282) \times \sqrt{(3000 \text{ psi})} + \frac{(10186 \text{ lbf})}{6 \times (2304 \text{ in}^2)} \right] \times (48 \text{ in}) \times (38.4 \text{ in})$$

$$V_{c,a} = 131.15 \text{ kip}$$

22.5.5.1.2

The following variables were converted to be consistent with empirical formula $f'_{ck} = 3 \text{ ksi} \rightarrow 3000 \text{ psi}$,
 $V_{c,b}$ - Shear strength of concrete (b)

$$V_{c,b} = \left[2 \lambda_s \sqrt{f'_{ck}} + (0.05 f'_{ck}) \right] b_w d$$

$$V_{c,b} = \left[2 \times (0.64282) \times \sqrt{(3000 \text{ psi})} + (0.05 \times (3000 \text{ psi})) \right] \times (48 \text{ in}) \times (38.4 \text{ in})$$

$$V_{c,b} = 406.27 \text{ kip}$$

V_c - Governing shear strength of concrete

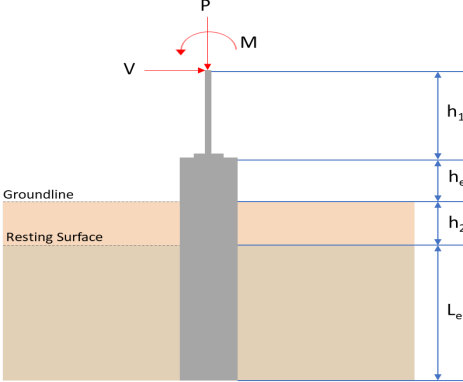
$$V_c = \text{Min}[V_{c,max}, V_{c,a}, V_{c,b}]$$

$$V_c = \text{Min}[(324.49 \text{ kip}), (131.15 \text{ kip}), (406.27 \text{ kip})]$$

$$V_c = 131.15 \text{ kip}$$

<p>22.5.1.2</p>	<p>The following variables were converted to be consistent with empirical formula $f'_{ck} = 3 \text{ ksi} \rightarrow 3000 \text{ psi}$, $V_{s,a}$ - Shear strength of steel (a)</p> $V_{s,a} = 8 \sqrt{f'_{ck}} b_w d$ $V_{s,a} = 8 \times \sqrt{(3000 \text{ psi})} \times (48 \text{ in}) \times (38.4 \text{ in})$ $V_{s,a} = 807.65 \text{ kip}$ <p>A_v - Ties rebar area,</p> $A_v = \frac{\pi d_{ties}^2}{4}$ $A_v = \frac{\pi \times (0.375 \text{ in})^2}{4}$ $A_v = 0.11045 \text{ in}^2$ <p>22.5.8.5.3 $V_{s,b}$ - Shear strength of steel (b)</p> $V_{s,b} = \frac{2 A_v f_{yties} d}{s_{ties}}$ $V_{s,b} = \frac{2 \times (0.11045 \text{ in}^2) \times (60 \text{ ksi}) \times (38.4 \text{ in})}{(10 \text{ in})}$ $V_{s,b} = 50.894 \text{ kip}$ <p>V_s - Governing shear strength of steel</p> $V_s = \text{MIN}[V_{s,a}, V_{s,b}]$ $V_s = \text{MIN}[(807.65 \text{ kip}), (50.894 \text{ kip})]$ $V_s = 50.894 \text{ kip}$ <p>22.5.1.1 ϕV_n - Allowable shear strength</p> $\phi V_n = \phi (V_c + V_s)$ $\phi V_n = (0.65) \times ((131.15 \text{ kip}) + (50.894 \text{ kip}))$ $\phi V_n = 118.33 \text{ kip}$ <p>Considering x-direction:</p> <p>$V_{max} = 14.066 \text{ kip}$ - Maximum shear force in the x-direction, Ratio - Capacity</p> $\text{Ratio} = \frac{V_{max}}{\phi V_n}$ $\text{Ratio} = \frac{(14.066 \text{ kip})}{(118.33 \text{ kip})}$ $\text{Ratio} = 0.11887$ <p>Considering z-direction:</p> <p>$V_{max} = 0.22679 \text{ kip}$ - Maximum shear force in the z-direction, Ratio - Capacity</p> $\text{Ratio} = \frac{V_{max}}{\phi V_n}$ $\text{Ratio} = \frac{(0.22679 \text{ kip})}{(118.33 \text{ kip})}$ $\text{Ratio} = 0.0019166$	<p>Status: PASS Ratio: 0.120</p> <p>Status: PASS Ratio: 0.000</p>
	<p>Flexural Strength (ACI 318-19, LRFD)</p> <p>S_m - Section modulus</p> $S_m = \frac{b D^2}{6}$ $S_m = \frac{(48 \text{ in}) \times (48 \text{ in})^2}{6}$ $S_m = 18432 \text{ in}^3$	

<p>14.5.2.1b</p>	<p>$\lambda = 1$ - Concrete modification factor (Normal concrete), Allowable flexural strength: M_n shall be the lesser of: $\phi M_{n,1}$</p> $\phi M_{n,1} = \phi \times 5 \times \lambda \times \sqrt{f'_c} \times S_m$ $\phi M_{n,1} = 0.65 \times 5 \times 1 \times \sqrt{3\text{ksi}} \times 18432.001\text{in}^3$ $\phi M_{n,1} = 273.423\text{kipft}$ <p>$\phi M_{n,2}$</p> $\phi M_{n,2} = \phi \times 0.85 \times f'_c \times S_m$ $\phi M_{n,2} = (0.65) \times 0.85 \times (3\text{ksi}) \times (18432\text{in}^3)$ $\phi M_{n,2} = 2545.9\text{kipft}$ <p>Therefore, ϕM_n - Allowable flexural strength,</p> $\phi M_n = \text{MIN}[\phi M_{n,1}, \phi M_{n,2}]$ $\phi M_n = \text{MIN}[(273.42\text{kipft}), (2545.9\text{kipft})]$ $\phi M_n = 273.42\text{kipft}$ <p>Considering x-direction: $M_{max} = 50.246\text{kipft}$ - Maximum moment in the x-direction, Ratio - Capacity</p> $\text{Ratio} = \frac{M_{max}}{\phi M_n}$ $\text{Ratio} = \frac{(50.246\text{kipft})}{(273.42\text{kipft})}$ $\text{Ratio} = 0.18377$	<p>Status: PASS Ratio: 0.180</p>
	<p>Considering z-direction: $M_{max} = 0.7508\text{kipft}$ - Maximum moment in the z-direction, Ratio - Capacity</p> $\text{Ratio} = \frac{M_{max}}{\phi M_n}$ $\text{Ratio} = \frac{(0.7508\text{kipft})}{(273.42\text{kipft})}$ $\text{Ratio} = 0.0027459$	<p>Status: PASS Ratio: 0.000</p>

REFERENCES	CALCULATIONS	RESULTS																										
	<p>SkyCiv Foundation Design Pile Foundation</p> <p>Design Information : Design code : IBC 2021 (International Building Code) Unit System : Imperial</p>																											
	<p>Pile Input</p>  <p>Geometry Pile shape: rectangular $b = 48$ in - Pile width $D = 48$ in - Pile depth $L = 7.5$ ft - Total pile length $h_1 = 0$ ft - Lateral load height from the top of the pile, $h_2 = 0$ ft - Depth to resting surface $h_e = 0$ ft - Length of pile above the ground</p> <p>Tabulation of Soil Parameters</p> <table border="1" data-bbox="416 1102 1193 1191"> <thead> <tr> <th>Layer</th> <th>Label</th> <th>Allowable Bearing Pressure (q_a) (psf)</th> <th>Allowable Lateral Pressure (R) (psf/ft)</th> </tr> </thead> <tbody> <tr> <td>1</td> <td>Sand, silty sand, clayey sand, silty gravel & clayey gravel</td> <td>2000.000</td> <td>150.000</td> </tr> </tbody> </table> <p>Tabulation of Loads</p> <table border="1" data-bbox="676 1285 933 1458"> <thead> <tr> <th>Load Component</th> <th>ASD</th> <th>LRFD</th> </tr> </thead> <tbody> <tr> <td>P (kip)</td> <td>6.620</td> <td>10.186</td> </tr> <tr> <td>V_x (kip)</td> <td>-3.456</td> <td>-5.767</td> </tr> <tr> <td>V_z (kip)</td> <td>-0.139</td> <td>-0.234</td> </tr> <tr> <td>M_x (kipft)</td> <td>-0.503</td> <td>-0.848</td> </tr> <tr> <td>M_z (kipft)</td> <td>46.000</td> <td>77.479</td> </tr> </tbody> </table> <p>Material Properties $f'_{ck} = 3$ ksi - Concrete strength,</p>	Layer	Label	Allowable Bearing Pressure (q_a) (psf)	Allowable Lateral Pressure (R) (psf/ft)	1	Sand, silty sand, clayey sand, silty gravel & clayey gravel	2000.000	150.000	Load Component	ASD	LRFD	P (kip)	6.620	10.186	V_x (kip)	-3.456	-5.767	V_z (kip)	-0.139	-0.234	M_x (kipft)	-0.503	-0.848	M_z (kipft)	46.000	77.479	
Layer	Label	Allowable Bearing Pressure (q_a) (psf)	Allowable Lateral Pressure (R) (psf/ft)																									
1	Sand, silty sand, clayey sand, silty gravel & clayey gravel	2000.000	150.000																									
Load Component	ASD	LRFD																										
P (kip)	6.620	10.186																										
V_x (kip)	-3.456	-5.767																										
V_z (kip)	-0.139	-0.234																										
M_x (kipft)	-0.503	-0.848																										
M_z (kipft)	46.000	77.479																										
	<p>Required depth to resist lateral loads (ASD) H - Point of application of the lateral load</p> $H = h_1 + h_2 + h_e$ $H = (0 \text{ ft}) + (0 \text{ ft}) + (0 \text{ ft})$ $H = 0 \text{ ft}$ <p>Considering x-direction: H_o - Lateral force per length of pile,</p> $H_o = \frac{V_x}{1.57 D}$ $H_o = \frac{(-3.456 \text{ kip})}{1.57 \times (48 \text{ in})}$ $H_o = -0.55032 \text{ kip/ft}$ <p>M_o - Moment per length of pile,</p> $M_o = \frac{M_z + (V_x H)}{1.57 D}$																											

$$M_o = \frac{(46 \text{ kipft}) + ((-3.456 \text{ kip}) \times (0 \text{ ft}))}{1.57 \times (48 \text{ in})}$$

$$M_o = 7.3248 \text{ kipft/ft}$$

Required depth of embedment in earth:

$$L_x^3 - \left(14.14 \times \frac{H_o \times L_x}{R}\right) - \left(18.85 \times \frac{M_o}{R}\right) = 0$$

Solving the cubic equation:

$L_{e,x} = 7.0653 \text{ ft}$ - Required depth in x-direction,

Considering z-direction:

H_o - Lateral force per length of pile,

$$H_o = \frac{V_z}{1.57 b}$$

$$H_o = \frac{(-0.139 \text{ kip})}{1.57 \times (48 \text{ in})}$$

$$H_o = -0.022134 \text{ kip/ft}$$

M_o - Moment per length of pile,

$$M_o = \frac{M_x + (V_z H)}{1.57 b}$$

$$M_o = \frac{(0.503 \text{ kipft}) + ((-0.139 \text{ kip}) \times (0 \text{ ft}))}{1.57 \times (48 \text{ in})}$$

$$M_o = 0.080096 \text{ kipft/ft}$$

Required depth of embedment in earth:

$$L_z^3 - \left(14.14 \times \frac{H_o \times L_z}{R}\right) - \left(18.85 \times \frac{M_o}{R}\right) = 0$$

Solving the cubic equation:

$L_{e,z} = 1.6206 \text{ ft}$ - Required depth in z-direction,

Minimum embedded depth required:

$L_{e,req}$ - Depth of pile required,

$$L_{e,req} = \text{MAX}[L_{e,x}, L_{e,z}]$$

$$L_{e,req} = \text{MAX}[(7.0653 \text{ ft}), (1.6206 \text{ ft})]$$

$$L_{e,req} = 7.065 \text{ ft}$$

L_e - Actual embedded length of pile,

$$L_e = L - h_e - h_2$$

$$L_e = (7.5 \text{ ft}) - (0 \text{ ft}) - (0 \text{ ft})$$

$$L_e = 7.5 \text{ ft}$$

Ratio - Embedded depth

$$\text{Ratio} = \frac{L_{e,req}}{L_e}$$

$$\text{Ratio} = \frac{(7.065 \text{ ft})}{(7.5 \text{ ft})}$$

$$\text{Ratio} = 0.942$$

Status: **PASS**
Ratio: **0.940**

End-bearing Capacity (ASD)

A - Pile cross-section area

$$A = b D$$

$$A = (48 \text{ in}) \times (48 \text{ in})$$

$$A = 16 \text{ ft}^2$$

q - End-bearing pressure

$$q = \frac{P_c}{A}$$

$$q = \frac{(6.62 \text{ kip})}{(16 \text{ ft}^2)}$$

$$q = 0.41375 \text{ kip/ft}^2$$

$$q = 0.41375 \text{ kip/ft}$$

Check bearing capacity ratio:

Ratio - Capacity

$$\text{Ratio} = \frac{q}{q_a}$$

$$\text{Ratio} = \frac{(0.41375 \text{ kip/ft}^2)}{(2000 \text{ psf})}$$

$$\text{Ratio} = 0.20688$$

Status: **PASS**
Ratio: **0.210**

Czerniak

Lateral Soil Pressure (ASD):

L/D - Length to least lateral dimension ratio,

$$L/D = \frac{L}{D}$$

$$L/D = \frac{(7.5 \text{ ft})}{(48 \text{ in})}$$

$$L/D = 1.875$$

Since $L/D \leq 10$,

Pile is short.

Considering x-direction:

$H_o = -0.55032 \text{ kip/ft}$ - Lateral force per length of pile,

$M_o = 7.3248 \text{ kipft/ft}$ - Overturning moment per length of pile,

a - Distance from resting surface to pivot point,

$$a = \frac{(4 M_o L_e) + (3 H_o L_e^2)}{(6 M_o) + (4 H_o L_e)}$$

$$a = \frac{(4 \times (7.3248 \text{ kipft/ft}) \times (7.5 \text{ ft})) + (3 \times (-0.55032 \text{ kip/ft}) \times (7.5 \text{ ft})^2)}{(6 \times (7.3248 \text{ kipft/ft})) + (4 \times (-0.55032 \text{ kip/ft}) \times (7.5 \text{ ft}))}$$

$$a = 5.1707 \text{ ft}$$

p - Earth pressure against the pile at distance $a/2$ from resting surface,

$$p = \frac{0.75 [(4 M_o) + (3 H_o L_e)]^2}{L_e^2 [(3 M_o) + (2 H_o L_e)]}$$

$$p = \frac{0.75 [(4 \times (7.3248 \text{ kipft/ft})) + (3 \times (-0.55032 \text{ kip/ft}) \times (7.5 \text{ ft}))]^2}{(7.5 \text{ ft})^2 [(3 \times (7.3248 \text{ kipft/ft})) + (2 \times (-0.55032 \text{ kip/ft}) \times (7.5 \text{ ft}))]}$$

$$p = 0.27813 \text{ kip/ft}^2$$

s - Earth pressure against the pile at distance L_e ,

$$s = \frac{6 [(2 M_o) + (H_o L_e)]}{L_e^2}$$

$$s = \frac{6 [(2 \times (7.3248 \text{ kipft/ft})) + ((-0.55032 \text{ kip/ft}) \times (7.5 \text{ ft}))]}{(7.5 \text{ ft})^2}$$

$$s = 1.1224 \text{ kip/ft}^2$$

Check lateral soil pressure capacity:

p_a - Allowable lateral soil pressure at depth $a/2$,

$$p_a = R \frac{a}{2}$$

$$p_a = (150 \text{ psf/ft}) \times \frac{(5.1707 \text{ ft})}{2}$$

$$p_a = 0.3878 \text{ kip/ft}^2$$

Ratio - Lateral soil capacity

$$\text{Ratio} = \frac{p}{p_a}$$

$$\text{Ratio} = \frac{(0.27813 \text{ kip/ft}^2)}{(0.3878 \text{ kip/ft}^2)}$$

$$\text{Ratio} = 0.7172$$

p_a - Allowable lateral soil pressure at depth L_e ,

Status: **PASS**
Ratio: **0.720**

$$p_s = R L_e$$

$$p_s = (150 \text{ psf/ft}) \times (7.5 \text{ ft})$$

$$p_s = 1.125 \text{ kip/ft}^2$$

Ratio - Lateral soil capacity

$$\text{Ratio} = \frac{s}{p_s}$$

$$\text{Ratio} = \frac{(1.1224 \text{ kip/ft}^2)}{(1.125 \text{ kip/ft}^2)}$$

$$\text{Ratio} = 0.99767$$

Status: **PASS**
Ratio: **1.000**

Considering z-direction:

$H_o = -0.022134 \text{ kip/ft}$ - Lateral force per length of pile,

$M_o = 0.080096 \text{ kipft/ft}$ - Overturning moment per length of pile,

a - Distance from resting surface to pivot point,

$$a = \frac{(4 M_o L_e) + (3 H_o L_e^2)}{(6 M_o) + (4 H_o L_e)}$$

$$a = \frac{(4 \times (0.080096 \text{ kipft/ft}) \times (7.5 \text{ ft})) + (3 \times (-0.022134 \text{ kip/ft}) \times (7.5 \text{ ft})^2)}{(6 \times (0.080096 \text{ kipft/ft})) + (4 \times (-0.022134 \text{ kip/ft}) \times (7.5 \text{ ft}))}$$

$$a = 5.3626 \text{ ft}$$

p - Earth pressure against the pile at distance $a/2$ from resting surface,

$$p = \frac{0.75 [(4 M_o) + (3 H_o L_e)]^2}{L_e^2 [(3 M_o) + (2 H_o L_e)]}$$

$$p = \frac{0.75 \times [(4 \times (0.080096 \text{ kipft/ft})) + (3 \times (-0.022134 \text{ kip/ft}) \times (7.5 \text{ ft}))]^2}{(7.5 \text{ ft})^2 \times [(3 \times (0.080096 \text{ kipft/ft})) + (2 \times (-0.022134 \text{ kip/ft}) \times (7.5 \text{ ft}))]}$$

$$p = -0.0045867 \text{ kip/ft}^2$$

s - Earth pressure against the pile at distance L_e ,

$$s = \frac{6 [(2 M_o) + (H_o L_e)]}{L_e^2}$$

$$s = \frac{6 \times [(2 \times (0.080096 \text{ kipft/ft})) + ((-0.022134 \text{ kip/ft}) \times (7.5 \text{ ft}))]}{(7.5 \text{ ft})^2}$$

$$s = -0.00061996 \text{ kip/ft}^2$$

Check lateral soil pressure capacity:

p_a - Allowable lateral soil pressure at depth $a/2$,

$$p_a = R \frac{a}{2}$$

$$p_a = (150 \text{ psf/ft}) \times \frac{(5.3626 \text{ ft})}{2}$$

$$p_a = 0.40219 \text{ kip/ft}^2$$

Ratio - Lateral soil capacity

$$\text{Ratio} = \frac{p}{p_a}$$

$$\text{Ratio} = \frac{(-0.0045867 \text{ kip/ft}^2)}{(0.40219 \text{ kip/ft}^2)}$$

$$\text{Ratio} = -0.011404$$

p_s - Allowable lateral soil pressure at depth L_e ,

$$p_s = R L_e$$

$$p_s = (150 \text{ psf/ft}) \times (7.5 \text{ ft})$$

$$p_s = 1.125 \text{ kip/ft}^2$$

Ratio - Lateral soil capacity

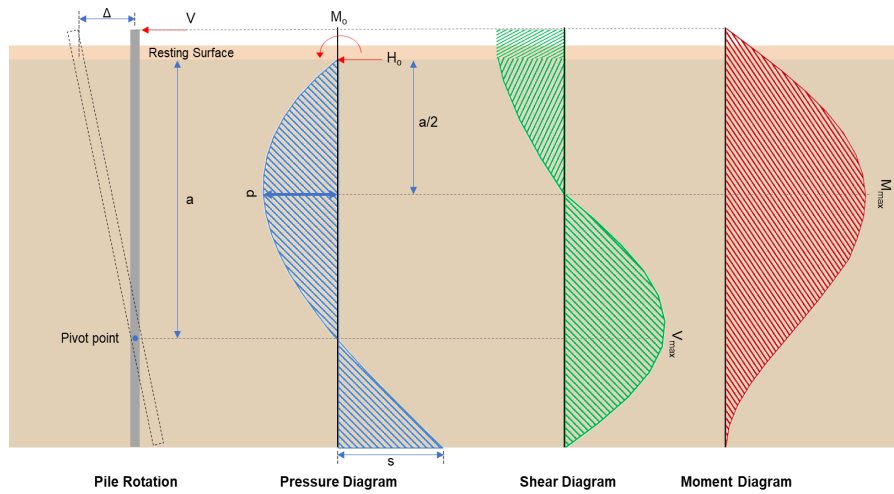
$$\text{Ratio} = \frac{s}{p_s}$$

Status: **PASS**
Ratio: **-0.010**

$$Ratio = \frac{(-0.00061996 \text{ kip/ft}^2)}{(1.125 \text{ kip/ft}^2)}$$

$$Ratio = -0.00055107$$

Status: **PASS**
Ratio: **0.000**



Shear force and Bending moment (x-direction, LRFD)

H_o - Lateral force per length of pile,

$$H_o = \frac{V_x}{1.57 D}$$

$$H_o = \frac{(-5.767 \text{ kip})}{1.57 \times (48 \text{ in})}$$

$$H_o = -0.91831 \text{ kip/ft}$$

M_o - Moment per length of pile,

$$M_o = \frac{M_x + (V_x H)}{1.57 D}$$

$$M_o = \frac{(77.479 \text{ kipft}) + ((-5.767 \text{ kip}) \times (0 \text{ ft}))}{1.57 \times (48 \text{ in})}$$

$$M_o = 12.337 \text{ kipft/ft}$$

E - Distance from lateral load to resisting surface,

$$E = \frac{M_o}{H_o}$$

$$E = \frac{(12.337 \text{ kipft/ft})}{(-0.91831 \text{ kip/ft})}$$

$$E = 13.435 \text{ ft}$$

a - Distance from resting surface to pivot point,

$$a = \frac{(4 M_o L_c) + (3 H_o L_c^2)}{(6 M_o) + (4 H_o L_c)}$$

$$a = \frac{(4 \times (12.337 \text{ kipft/ft}) \times (7.5 \text{ ft})) + (3 \times (-0.91831 \text{ kip/ft}) \times (7.5 \text{ ft})^2)}{(6 \times (12.337 \text{ kipft/ft})) + (4 \times (-0.91831 \text{ kip/ft}) \times (7.5 \text{ ft}))}$$

$$a = 5.1695 \text{ ft}$$

V_{max} - Max shear force located at depth a ,

$$V_{max} = (H_o D) \left[1 - \left[3 \left(\frac{4 E}{L_c} + 3 \right) \left(\frac{a}{L_c} \right)^2 \right] + \left[4 \left(\frac{3 E}{L_c} + 2 \right) \left(\frac{a}{L_c} \right)^3 \right] \right]$$

$$V_{max} = ((-0.91831 \text{ kip/ft}) \times (48 \text{ in})) \times \left[1 - \left[3 \times \left(\frac{4 \times (13.435 \text{ ft})}{(7.5 \text{ ft})} + 3 \right) \times \left(\frac{(5.1695 \text{ ft})}{(7.5 \text{ ft})} \right)^2 \right] + \left[4 \times \left(\frac{3 \times (13.435 \text{ ft})}{(7.5 \text{ ft})} + 2 \right) \times \left(\frac{(5.1695 \text{ ft})}{(7.5 \text{ ft})} \right)^3 \right] \right]$$

$$V_{max} = 14.066 \text{ kip}$$

M_{max} - Max bending moment located at depth $a/2$,

$$M_{max} = (H_o D L_e) \left[\left(\frac{E}{L_e} + \frac{a}{2 L_e} \right) - \left[\left(\frac{4E}{L_e} + 3 \right) \left(\frac{a}{2 L_e} \right)^3 + \left[\left(\frac{3E}{L_e} + 2 \right) \left(\frac{a}{2 L_e} \right)^4 \right] \right] \right]$$

$$M_{max} = ((-0.91831 \text{ kip/ft}) \times (48 \text{ in}) \times (7.5 \text{ ft})) \times \left[\left(\frac{(13.435 \text{ ft})}{(7.5 \text{ ft})} + \frac{(5.1695 \text{ ft})}{2 \times (7.5 \text{ ft})} \right) - \left[\left(\frac{4 \times (13.435 \text{ ft})}{(7.5 \text{ ft})} + 3 \right) \times \left(\frac{(5.1695 \text{ ft})}{2 \times (7.5 \text{ ft})} \right)^3 + \left[\left(\frac{3 \times (13.435 \text{ ft})}{(7.5 \text{ ft})} + 2 \right) \times \left(\frac{(5.1695 \text{ ft})}{2 \times (7.5 \text{ ft})} \right)^4 \right] \right] \right]$$

$$M_{max} = 50.247 \text{ kipft}$$

Shear force and Bending moment (z-direction, LRFD)

H_o - Lateral force per length of pile,

$$H_o = \frac{V_z}{1.57 b}$$

$$H_o = \frac{(-0.234 \text{ kip})}{1.57 \times (48 \text{ in})}$$

$$H_o = -0.037261 \text{ kip/ft}$$

M_o - Moment per length of pile,

$$M_o = \frac{M_x + (V_z H)}{1.57 b}$$

$$M_o = \frac{(0.848 \text{ kipft}) + ((-0.234 \text{ kip}) \times (0 \text{ ft}))}{1.57 \times (48 \text{ in})}$$

$$M_o = 0.13503 \text{ kipft/ft}$$

E - Distance from lateral load to resisting surface,

$$E = \frac{M_o}{H_o}$$

$$E = \frac{(0.13503 \text{ kipft/ft})}{(-0.037261 \text{ kip/ft})}$$

$$E = 3.6239 \text{ ft}$$

a - Distance from resting surface to pivot point,

$$a = \frac{(4 M_o L_e) + (3 H_o L_e^2)}{(6 M_o) + (4 H_o L_e)}$$

$$a = \frac{(4 \times (0.13503 \text{ kipft/ft}) \times (7.5 \text{ ft})) + (3 \times (-0.037261 \text{ kip/ft}) \times (7.5 \text{ ft})^2)}{(6 \times (0.13503 \text{ kipft/ft})) + (4 \times (-0.037261 \text{ kip/ft}) \times (7.5 \text{ ft}))}$$

$$a = 5.3624 \text{ ft}$$

V_{max} - Max shear force located at depth a ,

$$V_{max} = (H_o b) \left[1 - \left[3 \left(\frac{4E}{L_e} + 3 \right) \left(\frac{a}{L_e} \right)^2 + 4 \left(\frac{3E}{L_e} + 2 \right) \left(\frac{a}{L_e} \right)^3 \right] \right]$$

$$V_{max} = ((-0.037261 \text{ kip/ft}) \times (48 \text{ in})) \times \left[1 - \left[3 \times \left(\frac{4 \times (3.6239 \text{ ft})}{(7.5 \text{ ft})} + 3 \right) \times \left(\frac{(5.3624 \text{ ft})}{(7.5 \text{ ft})} \right)^2 + 4 \times \left(\frac{3 \times (3.6239 \text{ ft})}{(7.5 \text{ ft})} + 2 \right) \times \left(\frac{(5.3624 \text{ ft})}{(7.5 \text{ ft})} \right)^3 \right] \right]$$

$$V_{max} = 0.22679 \text{ kip}$$

M_{max} - Max bending moment located at depth $a/2$,

$$M_{max} = (H_o b L_e) \left[\left(\frac{E}{L_e} + \frac{a}{2 L_e} \right) - \left[\left(\frac{4E}{L_e} + 3 \right) \left(\frac{a}{2 L_e} \right)^3 + \left[\left(\frac{3E}{L_e} + 2 \right) \left(\frac{a}{2 L_e} \right)^4 \right] \right] \right]$$

$$M_{max} = ((-0.037261 \text{ kip/ft}) \times (48 \text{ in}) \times (7.5 \text{ ft})) \times \left[\left(\frac{(3.6239 \text{ ft})}{(7.5 \text{ ft})} + \frac{(5.3624 \text{ ft})}{2 \times (7.5 \text{ ft})} \right) - \left[\left(\frac{4 \times (3.6239 \text{ ft})}{(7.5 \text{ ft})} + 3 \right) \times \left(\frac{(5.3624 \text{ ft})}{2 \times (7.5 \text{ ft})} \right)^3 + \left[\left(\frac{3 \times (3.6239 \text{ ft})}{(7.5 \text{ ft})} + 2 \right) \times \left(\frac{(5.3624 \text{ ft})}{2 \times (7.5 \text{ ft})} \right)^4 \right] \right] \right]$$

$$M_{max} = 0.7508 \text{ kipft}$$

Minimum Reinforcement Check (LRFD)

Parameters:

$f'_{ck} = 3 \text{ ksi}$ - Concrete strength,
 $f_{yk} = 60 \text{ ksi}$ - Longitudinal reinforcement strength,
 $\phi = 0.65$ - Reduction factor for axial strength,
 $\alpha = 0.8$ - Alpha factor for axial strength,
 $A_g = 2304 \text{ in}^2$ - Gross area of concrete,

Table 22.4.2.1

Longitudinal reinforcement:

Required reinforcement due to axial load, $A_{st,required}$

22.4.2.2, 10.6.1.1

$A_{st,required}$

$$A_{st,required} = \text{Min} \left[\frac{\frac{P}{\phi \alpha} - (0.85 f'_{ck} A_g)}{f_{yk} - (0.85 f'_{ck})}, (0.08 A_g) \right]$$

$$A_{st,required} = \text{Min} \left[\frac{\frac{(10.186 \text{ kip})}{(0.65) \times (0.8)} - (0.85 \times (3 \text{ ksi}) \times (2304 \text{ in}^2))}{(60 \text{ ksi}) - (0.85 \times (3 \text{ ksi}))}, (0.08 \times (2304 \text{ in}^2)) \right]$$

$$A_{st,required} = -101.93 \text{ in}^2$$

A_{min} - Governing minimum reinforcement area,

$$A_{min} = \text{Max} [A_{st,required}, (0.0018 A_g)]$$

$$A_{min} = \text{Max} [(-101.93 \text{ in}^2), (0.0018 \times (2304 \text{ in}^2))]$$

$$A_{min} = 4.1472 \text{ in}^2$$

n_{rebar} - Required number of reinforcement,

$$n_{rebar} = \frac{A_{min}}{A_{rebar}}$$

$$n_{rebar} = \frac{(4.1472 \text{ in}^2)}{(0.3068 \text{ in}^2)}$$

$$n_{rebar} = 14$$

A_{st} - Actual total reinforcement area,

$$A_{st} = n_{rebar} \frac{\pi d_{bar}^2}{4}$$

$$A_{st} = (14) \times \frac{\pi \times (0.625 \text{ in})^2}{4}$$

$$A_{st} = 4.2951 \text{ in}^2$$

Ratio - Capacity

$$\text{Ratio} = \frac{A_{min}}{A_{st}}$$

$$\text{Ratio} = \frac{(4.1472 \text{ in}^2)}{(4.2951 \text{ in}^2)}$$

$$\text{Ratio} = 0.96556$$

Status: **PASS**
Ratio: **0.970**

25.2.3

s_{rebar} - Minimum spacing of reinforcement,

$$s_{rebar} = \text{Max} [1.5, (1.5 d_{bar})]$$

$$s_{rebar} = \text{Max} [1.5, (1.5 \times (0.625 \text{ in}))]$$

$$s_{rebar} = 1.5 \text{ in}$$

Ties:

25.7.2.2 Since longitudinal reinforcement is \leq No. 10: Use #3(0.375 in)

25.7.2.1 s_{ties} - Maximum spacing of ties,

$$s_{ties} = \text{Min} [(16 d_{bar}), (48 d_{ties}), \text{Min} (D, b)]$$

$$s_{ties} = \text{Min} [(16 \times (0.625 \text{ in})), (48 \times (0.375 \text{ in})), \text{Min} ((48 \text{ in}), (48 \text{ in}))]$$

$$s_{ties} = 10 \text{ in}$$

Summary:

Main reinforcement: **14 - #5 (0.625 in)**

Ties: #3(0.375 in) - 10 in

Axial Compression Strength (ACI 318-19, LRFD)

22.4.2.2

ϕP_N - Allowable axial compressive strength

$$\phi P_N = \phi 0.80 [(0.85 f'_{ck} [A_g - A_{st}]) + (f_{yk} A_{st})]$$

$$\phi P_N = (0.65) \times 0.80 \times [(0.85 \times (3 \text{ ksi}) \times [(2304 \text{ in}^2) - (4.2951 \text{ in}^2)]) + ((60 \text{ ksi}) \times (4.2951 \text{ in}^2))]$$

$$\phi P_N = 3183.4 \text{ kip}$$

Ratio - Capacity

$$\text{Ratio} = \frac{P}{\phi P_N}$$

$$\text{Ratio} = \frac{(10.186 \text{ kip})}{(3183.4 \text{ kip})}$$

$$\text{Ratio} = 0.0031997$$

Status: **PASS**
Ratio: **0.000**

Shear Strength (ACI 318-19, LRFD)

Parameters:

22.5.2.2

$b_w = 48 \text{ in}$ - Effective width,
 d - Effective depth

$$d = 0.80 D$$

$$d = 0.80 \times (48 \text{ in})$$

$$d = 38.4 \text{ in}$$

22.5.5.1.3

λ_s - size effect modification factor

$$\lambda_s = \text{MIN} \left[\sqrt{\frac{2}{1 + \frac{d}{10}}}, 1 \right]$$

$$\lambda_s = \text{MIN} \left[\sqrt{\frac{2}{1 + \frac{(38.4 \text{ in})}{10}}}, 1 \right]$$

$$\lambda_s = 0.64282$$

22.5.5.1.1

The following variables were converted to be consistent with empirical formula $f'_{ck} = 3 \text{ ksi} \rightarrow 3000 \text{ psi}$,
 $V_{c,max}$ - Max shear strength of concrete

$$V_{c,max} = 5 \lambda_s \sqrt{f'_{ck}} b_w d$$

$$V_{c,max} = 5 \times (0.64282) \times \sqrt{(3000 \text{ psi})} \times (48 \text{ in}) \times (38.4 \text{ in})$$

$$V_{c,max} = 324.49 \text{ kip}$$

22.5.5.1.1(a)

The following variables were converted to be consistent with empirical formula $f'_{ck} = 3 \text{ ksi} \rightarrow 3000 \text{ psi}$, $P = 10.186 \text{ kip} \rightarrow 10186 \text{ lbf}$,
 $V_{c,a}$ - Shear strength of concrete (a)

$$V_{c,a} = \left[2 \lambda_s \sqrt{f'_{ck}} + \frac{P}{6 A_g} \right] b_w d$$

$$V_{c,a} = \left[2 \times (0.64282) \times \sqrt{(3000 \text{ psi})} + \frac{(10186 \text{ lbf})}{6 \times (2304 \text{ in}^2)} \right] \times (48 \text{ in}) \times (38.4 \text{ in})$$

$$V_{c,a} = 131.15 \text{ kip}$$

22.5.5.1.2

The following variables were converted to be consistent with empirical formula $f'_{ck} = 3 \text{ ksi} \rightarrow 3000 \text{ psi}$,
 $V_{c,b}$ - Shear strength of concrete (b)

$$V_{c,b} = \left[2 \lambda_s \sqrt{f'_{ck}} + (0.05 f'_{ck}) \right] b_w d$$

$$V_{c,b} = \left[2 \times (0.64282) \times \sqrt{(3000 \text{ psi})} + (0.05 \times (3000 \text{ psi})) \right] \times (48 \text{ in}) \times (38.4 \text{ in})$$

$$V_{c,b} = 406.27 \text{ kip}$$

V_c - Governing shear strength of concrete

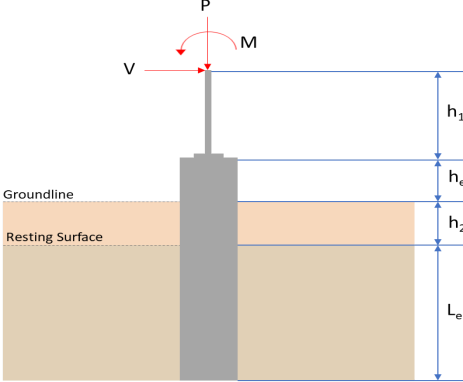
$$V_c = \text{Min}[V_{c,max}, V_{c,a}, V_{c,b}]$$

$$V_c = \text{Min}[(324.49 \text{ kip}), (131.15 \text{ kip}), (406.27 \text{ kip})]$$

$$V_c = 131.15 \text{ kip}$$

<p>22.5.1.2</p>	<p>The following variables were converted to be consistent with empirical formula $f'_{ck} = 3 \text{ ksi} \rightarrow 3000 \text{ psi}$, $V_{s,a}$ - Shear strength of steel (a)</p> $V_{s,a} = 8 \sqrt{f'_{ck}} b_w d$ $V_{s,a} = 8 \times \sqrt{(3000 \text{ psi})} \times (48 \text{ in}) \times (38.4 \text{ in})$ $V_{s,a} = 807.65 \text{ kip}$ <p>A_v - Ties rebar area,</p> $A_v = \frac{\pi d_{ties}^2}{4}$ $A_v = \frac{\pi \times (0.375 \text{ in})^2}{4}$ $A_v = 0.11045 \text{ in}^2$ <p>22.5.8.5.3 $V_{s,b}$ - Shear strength of steel (b)</p> $V_{s,b} = \frac{2 A_v f_{yt} d}{s_{ties}}$ $V_{s,b} = \frac{2 \times (0.11045 \text{ in}^2) \times (60 \text{ ksi}) \times (38.4 \text{ in})}{(10 \text{ in})}$ $V_{s,b} = 50.894 \text{ kip}$ <p>V_s - Governing shear strength of steel</p> $V_s = \text{MIN}[V_{s,a}, V_{s,b}]$ $V_s = \text{MIN}[(807.65 \text{ kip}), (50.894 \text{ kip})]$ $V_s = 50.894 \text{ kip}$ <p>22.5.1.1 ϕV_n - Allowable shear strength</p> $\phi V_n = \phi (V_c + V_s)$ $\phi V_n = (0.65) \times ((131.15 \text{ kip}) + (50.894 \text{ kip}))$ $\phi V_n = 118.33 \text{ kip}$ <p>Considering x-direction:</p> <p>$V_{max} = 14.066 \text{ kip}$ - Maximum shear force in the x-direction, Ratio - Capacity</p> $\text{Ratio} = \frac{V_{max}}{\phi V_n}$ $\text{Ratio} = \frac{(14.066 \text{ kip})}{(118.33 \text{ kip})}$ $\text{Ratio} = 0.11887$ <p>Considering z-direction:</p> <p>$V_{max} = 0.22679 \text{ kip}$ - Maximum shear force in the z-direction, Ratio - Capacity</p> $\text{Ratio} = \frac{V_{max}}{\phi V_n}$ $\text{Ratio} = \frac{(0.22679 \text{ kip})}{(118.33 \text{ kip})}$ $\text{Ratio} = 0.0019166$	<p>Status: PASS Ratio: 0.120</p> <p>Status: PASS Ratio: 0.000</p>
	<p>Flexural Strength (ACI 318-19, LRFD)</p> <p>S_m - Section modulus</p> $S_m = \frac{b D^2}{6}$ $S_m = \frac{(48 \text{ in}) \times (48 \text{ in})^2}{6}$ $S_m = 18432 \text{ in}^3$	

<p>14.5.2.1b</p>	<p>$\lambda = 1$ - Concrete modification factor (Normal concrete), Allowable flexural strength: M_n shall be the lesser of: $\phi M_{n,1}$</p> $\phi M_{n,1} = \phi \times 5 \times \lambda \times \sqrt{f'_c} \times S_m$ $\phi M_{n,1} = 0.65 \times 5 \times 1 \times \sqrt{3\text{ksi}} \times 18432.001\text{in}^3$ $\phi M_{n,1} = 273.423\text{kipft}$ <p>$\phi M_{n,2}$</p> $\phi M_{n,2} = \phi \times 0.85 \times f'_c \times S_m$ $\phi M_{n,2} = (0.65) \times 0.85 \times (3\text{ksi}) \times (18432\text{in}^3)$ $\phi M_{n,2} = 2545.9\text{kipft}$ <p>Therefore, ϕM_n - Allowable flexural strength,</p> $\phi M_n = \text{MIN}[\phi M_{n,1}, \phi M_{n,2}]$ $\phi M_n = \text{MIN}[(273.42\text{kipft}), (2545.9\text{kipft})]$ $\phi M_n = 273.42\text{kipft}$ <p>Considering x-direction: $M_{max} = 50.247\text{kipft}$ - Maximum moment in the x-direction, Ratio - Capacity</p> $\text{Ratio} = \frac{M_{max}}{\phi M_n}$ $\text{Ratio} = \frac{(50.247\text{kipft})}{(273.42\text{kipft})}$ $\text{Ratio} = 0.18377$	<p>Status: PASS Ratio: 0.180</p>
	<p>Considering z-direction: $M_{max} = 0.7508\text{kipft}$ - Maximum moment in the z-direction, Ratio - Capacity</p> $\text{Ratio} = \frac{M_{max}}{\phi M_n}$ $\text{Ratio} = \frac{(0.7508\text{kipft})}{(273.42\text{kipft})}$ $\text{Ratio} = 0.0027459$	<p>Status: PASS Ratio: 0.000</p>

REFERENCES	CALCULATIONS	RESULTS																										
	<p>SkyCiv Foundation Design Pile Foundation</p> <p>Design Information : Design code : IBC 2021 (International Building Code) Unit System : Imperial</p>																											
	<p>Pile Input</p>  <p>Geometry Pile shape: rectangular $b = 48$ in - Pile width $D = 48$ in - Pile depth $L = 7.75$ ft - Total pile length $h_1 = 0$ ft - Lateral load height from the top of the pile, $h_2 = 0$ ft - Depth to resting surface $h_e = 0$ ft - Length of pile above the ground</p> <p>Tabulation of Soil Parameters</p> <table border="1" data-bbox="416 1102 1193 1191"> <thead> <tr> <th>Layer</th> <th>Label</th> <th>Allowable Bearing Pressure (q_a) (psf)</th> <th>Allowable Lateral Pressure (R) (psf/ft)</th> </tr> </thead> <tbody> <tr> <td>1</td> <td>Sand, silty sand, clayey sand, silty gravel & clayey gravel</td> <td>2000.000</td> <td>150.000</td> </tr> </tbody> </table> <p>Tabulation of Loads</p> <table border="1" data-bbox="676 1288 933 1458"> <thead> <tr> <th>Load Component</th> <th>ASD</th> <th>LRFD</th> </tr> </thead> <tbody> <tr> <td>P (kip)</td> <td>7.510</td> <td>11.576</td> </tr> <tr> <td>V_x (kip)</td> <td>-3.899</td> <td>-6.494</td> </tr> <tr> <td>V_z (kip)</td> <td>0.000</td> <td>0.000</td> </tr> <tr> <td>M_x (kipft)</td> <td>0.000</td> <td>0.000</td> </tr> <tr> <td>M_z (kipft)</td> <td>51.518</td> <td>86.857</td> </tr> </tbody> </table> <p>Material Properties $f'_{ck} = 3$ ksi - Concrete strength,</p>	Layer	Label	Allowable Bearing Pressure (q_a) (psf)	Allowable Lateral Pressure (R) (psf/ft)	1	Sand, silty sand, clayey sand, silty gravel & clayey gravel	2000.000	150.000	Load Component	ASD	LRFD	P (kip)	7.510	11.576	V_x (kip)	-3.899	-6.494	V_z (kip)	0.000	0.000	M_x (kipft)	0.000	0.000	M_z (kipft)	51.518	86.857	
Layer	Label	Allowable Bearing Pressure (q_a) (psf)	Allowable Lateral Pressure (R) (psf/ft)																									
1	Sand, silty sand, clayey sand, silty gravel & clayey gravel	2000.000	150.000																									
Load Component	ASD	LRFD																										
P (kip)	7.510	11.576																										
V_x (kip)	-3.899	-6.494																										
V_z (kip)	0.000	0.000																										
M_x (kipft)	0.000	0.000																										
M_z (kipft)	51.518	86.857																										
	<p>Required depth to resist lateral loads (ASD) H - Point of application of the lateral load</p> $H = h_1 + h_2 + h_e$ $H = (0 \text{ ft}) + (0 \text{ ft}) + (0 \text{ ft})$ $H = 0 \text{ ft}$ <p>Considering x-direction: H_o - Lateral force per length of pile,</p> $H_o = \frac{V_x}{1.57 D}$ $H_o = \frac{(-3.899 \text{ kip})}{1.57 \times (48 \text{ in})}$ $H_o = -0.62086 \text{ kip/ft}$ <p>M_o - Moment per length of pile,</p> $M_o = \frac{M_z + (V_x H)}{1.57 D}$																											

	$M_o = \frac{(51.518 \text{ kipft}) + ((-3.899 \text{ kip}) \times (0 \text{ ft}))}{1.57 \times (48 \text{ in})}$ $M_o = 8.2035 \text{ kipft/ft}$ <p>Required depth of embedment in earth:</p> $L_x^3 - \left(14.14 \times \frac{H_o \times L_x}{R}\right) - \left(18.85 \times \frac{M_o}{R}\right) = 0$ <p>Solving the cubic equation: $L_{e,x} = 7.2762 \text{ ft}$ - Required depth in x-direction,</p> <p>Considering z-direction: $L_{e,z} = 0 \text{ ft}$ - Required depth in z-direction,</p> <p>Minimum embedded depth required: $L_{e,req}$ - Depth of pile required,</p> $L_{e,req} = \text{MAX}[L_{e,x}, L_{e,z}]$ $L_{e,req} = \text{MAX}[(7.2762 \text{ ft}), (0 \text{ ft})]$ $L_{e,req} = 7.276 \text{ ft}$ <p>L_e - Actual embedded length of pile,</p> $L_e = L - h_e - h_2$ $L_e = (7.75 \text{ ft}) - (0 \text{ ft}) - (0 \text{ ft})$ $L_e = 7.75 \text{ ft}$ <p>Ratio - Embedded depth</p> $\text{Ratio} = \frac{L_{e,req}}{L_e}$ $\text{Ratio} = \frac{(7.276 \text{ ft})}{(7.75 \text{ ft})}$ $\text{Ratio} = 0.93884$	<p>Status: PASS Ratio: 0.940</p>
	<p>End-bearing Capacity (ASD) A - Pile cross-section area</p> $A = b D$ $A = (48 \text{ in}) \times (48 \text{ in})$ $A = 16 \text{ ft}^2$ <p>q - End-bearing pressure</p> $q = \frac{P_v}{A}$ $q = \frac{(7.51 \text{ kip})}{(16 \text{ ft}^2)}$ $q = 0.46937 \text{ kip/ft}^2$ <p>Check bearing capacity ratio: Ratio - Capacity</p> $\text{Ratio} = \frac{q}{q_o}$ $\text{Ratio} = \frac{(0.46937 \text{ kip/ft}^2)}{(2000 \text{ psf})}$ $\text{Ratio} = 0.23469$	<p>Status: PASS Ratio: 0.230</p>
<p>Czerniak</p>	<p>Lateral Soil Pressure (ASD): L/D - Length to least lateral dimension ratio,</p> $L/D = \frac{L}{D}$ $L/D = \frac{(7.75 \text{ ft})}{(48 \text{ in})}$	

$$L/D = 1.9375$$

Since $L/D \leq 10$,

Pile is short.

Considering x-direction:

$H_o = -0.62086$ kip/ft - Lateral force per length of pile,

$M_o = 8.2035$ kipft/ft - Overturning moment per length of pile,

a - Distance from resting surface to pivot point,

$$a = \frac{(4 M_o L_e) + (3 H_o L_e^2)}{(6 M_o) + (4 H_o L_e)}$$

$$a = \frac{(4 \times (8.2035 \text{ kipft/ft}) \times (7.75 \text{ ft})) + (3 \times (-0.62086 \text{ kip/ft}) \times (7.75 \text{ ft})^2)}{(6 \times (8.2035 \text{ kipft/ft})) + (4 \times (-0.62086 \text{ kip/ft}) \times (7.75 \text{ ft}))}$$

$$a = 5.3482 \text{ ft}$$

p - Earth pressure against the pile at distance $a/2$ from resting surface,

$$p = \frac{0.75 [(4 M_o) + (3 H_o L_e)]^2}{L_e^2 [(3 M_o) + (2 H_o L_e)]}$$

$$p = \frac{0.75 \times [(4 \times (8.2035 \text{ kipft/ft})) + (3 \times (-0.62086 \text{ kip/ft}) \times (7.75 \text{ ft}))]^2}{(7.75 \text{ ft})^2 \times [(3 \times (8.2035 \text{ kipft/ft})) + (2 \times (-0.62086 \text{ kip/ft}) \times (7.75 \text{ ft}))]}$$

$$p = 0.28144 \text{ kip/ft}^2$$

s - Earth pressure against the pile at distance L_e ,

$$s = \frac{6 [(2 M_o) + (H_o L_e)]}{L_e^2}$$

$$s = \frac{6 \times [(2 \times (8.2035 \text{ kipft/ft})) + ((-0.62086 \text{ kip/ft}) \times (7.75 \text{ ft}))]}{(7.75 \text{ ft})^2}$$

$$s = 1.1583 \text{ kip/ft}^2$$

Check lateral soil pressure capacity:

p_a - Allowable lateral soil pressure at depth $a/2$,

$$p_a = R \frac{q}{2}$$

$$p_a = (150 \text{ psf/ft}) \times \frac{(5.3482 \text{ ft})}{2}$$

$$p_a = 0.40112 \text{ kip/ft}^2$$

Ratio - Lateral soil capacity

$$\text{Ratio} = \frac{p}{p_a}$$

$$\text{Ratio} = \frac{(0.28144 \text{ kip/ft}^2)}{(0.40112 \text{ kip/ft}^2)}$$

$$\text{Ratio} = 0.70164$$

p_s - Allowable lateral soil pressure at depth L_e ,

$$p_s = R L_e$$

$$p_s = (150 \text{ psf/ft}) \times (7.75 \text{ ft})$$

$$p_s = 1.1625 \text{ kip/ft}^2$$

Ratio - Lateral soil capacity

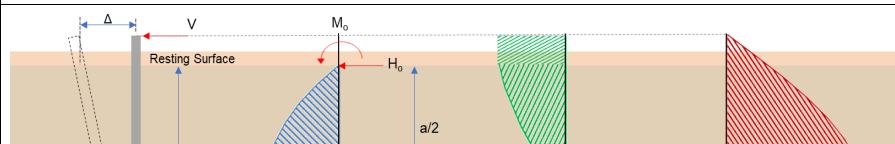
$$\text{Ratio} = \frac{s}{p_s}$$

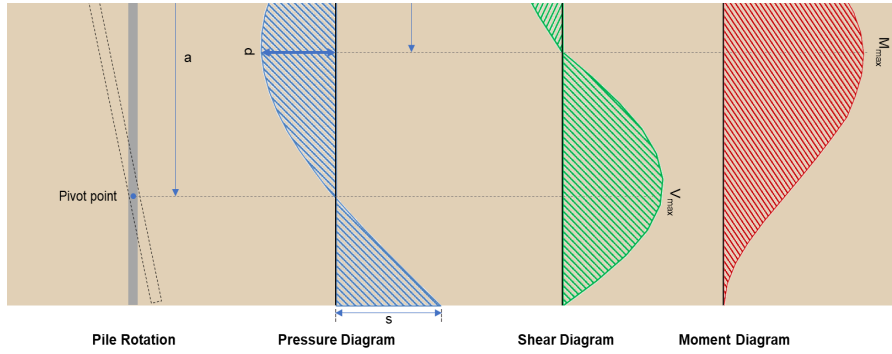
$$\text{Ratio} = \frac{(1.1583 \text{ kip/ft}^2)}{(1.1625 \text{ kip/ft}^2)}$$

$$\text{Ratio} = 0.99641$$

Status: **PASS**
Ratio: **0.700**

Status: **PASS**
Ratio: **1.000**





Shear force and Bending moment (x-direction, LRFD)

H_o - Lateral force per length of pile,

$$H_o = \frac{V_x}{1.57 D}$$

$$H_o = \frac{(-6.494 \text{ kip})}{1.57 \times (48 \text{ in})}$$

$$H_o = -1.0341 \text{ kip/ft}$$

M_o - Moment per length of pile,

$$M_o = \frac{M_x + (V_x H)}{1.57 D}$$

$$M_o = \frac{(86.857 \text{ kipft}) + ((-6.494 \text{ kip}) \times (0 \text{ ft}))}{1.57 \times (48 \text{ in})}$$

$$M_o = 13.831 \text{ kipft/ft}$$

E - Distance from lateral load to resisting surface,

$$E = \frac{M_o}{H_o}$$

$$E = \frac{(13.831 \text{ kipft/ft})}{(-1.0341 \text{ kip/ft})}$$

$$E = 13.375 \text{ ft}$$

a - Distance from resting surface to pivot point,

$$a = \frac{(4 M_o L_c) + (3 H_o L_c^2)}{(6 M_o) + (4 H_o L_c)}$$

$$a = \frac{(4 \times (13.831 \text{ kipft/ft}) \times (7.75 \text{ ft})) + (3 \times (-1.0341 \text{ kip/ft}) \times (7.75 \text{ ft})^2)}{(6 \times (13.831 \text{ kipft/ft})) + (4 \times (-1.0341 \text{ kip/ft}) \times (7.75 \text{ ft}))}$$

$$a = 5.3466 \text{ ft}$$

V_{max} - Max shear force located at depth a ,

$$V_{max} = (H_o D) \left[1 - \left[3 \left(\frac{4 E}{L_c} + 3 \right) \left(\frac{a}{L_c} \right)^2 \right] + \left[4 \left(\frac{3 E}{L_c} + 2 \right) \left(\frac{a}{L_c} \right)^3 \right] \right]$$

$$V_{max} = ((-1.0341 \text{ kip/ft}) \times (48 \text{ in})) \times \left[1 - \left[3 \times \left(\frac{4 \times (13.375 \text{ ft})}{(7.75 \text{ ft})} + 3 \right) \times \left(\frac{5.3466 \text{ ft}}{(7.75 \text{ ft})} \right)^2 \right] + \left[4 \times \left(\frac{3 \times (13.375 \text{ ft})}{(7.75 \text{ ft})} + 2 \right) \times \left(\frac{5.3466 \text{ ft}}{(7.75 \text{ ft})} \right)^3 \right] \right]$$

$$V_{max} = 15.36 \text{ kip}$$

M_{max} - Max bending moment located at depth $a/2$,

$$M_{max} = (H_o D L_c) \left[\left(\frac{E}{L_c} + \frac{a}{2 L_c} \right) - \left[\left(\frac{4 E}{L_c} + 3 \right) \left(\frac{a}{2 L_c} \right)^3 \right] + \left[\left(\frac{3 E}{L_c} + 2 \right) \left(\frac{a}{2 L_c} \right)^4 \right] \right]$$

$$M_{max} = ((-1.0341 \text{ kip/ft}) \times (48 \text{ in}) \times (7.75 \text{ ft})) \times \left[\left(\frac{13.375 \text{ ft}}{(7.75 \text{ ft})} + \frac{5.3466 \text{ ft}}{2 \times (7.75 \text{ ft})} \right) - \left[\left(\frac{4 \times (13.375 \text{ ft})}{(7.75 \text{ ft})} + 3 \right) \times \left(\frac{5.3466 \text{ ft}}{2 \times (7.75 \text{ ft})} \right)^3 \right] + \left[\left(\frac{3 \times (13.375 \text{ ft})}{(7.75 \text{ ft})} + 2 \right) \times \left(\frac{5.3466 \text{ ft}}{2 \times (7.75 \text{ ft})} \right)^4 \right] \right]$$

$$M_{max} = 56.608 \text{ kipft}$$

Minimum Reinforcement Check (LRFD)

Parameters:

$f'_{ck} = 3 \text{ ksi}$ - Concrete strength,
 $f_{yk} = 60 \text{ ksi}$ - Longitudinal reinforcement strength,
 $\phi = 0.65$ - Reduction factor for axial strength,
 $\alpha = 0.8$ - Alpha factor for axial strength,
 $A_g = 2304 \text{ in}^2$ - Gross area of concrete,

Table 22.4.2.1

Longitudinal reinforcement:

Required reinforcement due to axial load, $A_{st,required}$

22.4.2.2, 10.6.1.1

$A_{st,required}$

$$A_{st,required} = \text{Min} \left[\frac{\frac{P}{\phi \alpha} - (0.85 f'_{ck} A_g)}{f_{yk} - (0.85 f'_{ck})}, (0.08 A_g) \right]$$

$$A_{st,required} = \text{Min} \left[\frac{\frac{(11.576 \text{ kip})}{(0.65) \times (0.8)} - (0.85 \times (3 \text{ ksi}) \times (2304 \text{ in}^2))}{(60 \text{ ksi}) - (0.85 \times (3 \text{ ksi}))}, (0.08 \times (2304 \text{ in}^2)) \right]$$

$$A_{st,required} = -101.88 \text{ in}^2$$

A_{min} - Governing minimum reinforcement area,

$$A_{min} = \text{Max} [A_{st,required}, (0.0018 A_g)]$$

$$A_{min} = \text{Max} [(-101.88 \text{ in}^2), (0.0018 \times (2304 \text{ in}^2))]$$

$$A_{min} = 4.1472 \text{ in}^2$$

n_{rebar} - Required number of reinforcement,

$$n_{rebar} = \frac{A_{min}}{A_{rebar}}$$

$$n_{rebar} = \frac{(4.1472 \text{ in}^2)}{(0.3068 \text{ in}^2)}$$

$$n_{rebar} = 14$$

A_{st} - Actual total reinforcement area,

$$A_{st} = n_{rebar} \frac{\pi d_{bar}^2}{4}$$

$$A_{st} = (14) \times \frac{\pi \times (0.625 \text{ in})^2}{4}$$

$$A_{st} = 4.2951 \text{ in}^2$$

Ratio - Capacity

$$\text{Ratio} = \frac{A_{min}}{A_{st}}$$

$$\text{Ratio} = \frac{(4.1472 \text{ in}^2)}{(4.2951 \text{ in}^2)}$$

$$\text{Ratio} = 0.96556$$

Status: **PASS**
Ratio: **0.970**

25.2.3

s_{rebar} - Minimum spacing of reinforcement,

$$s_{rebar} = \text{Max} [1.5, (1.5 d_{bar})]$$

$$s_{rebar} = \text{Max} [1.5, (1.5 \times (0.625 \text{ in}))]$$

$$s_{rebar} = 1.5 \text{ in}$$

Ties:

25.7.2.2 Since longitudinal reinforcement is \leq No. 10: Use #3(0.375 in)

25.7.2.1 s_{ties} - Maximum spacing of ties,

$$s_{ties} = \text{Min} [(16 d_{bar}), (48 d_{ties}), \text{Min} (D, b)]$$

$$s_{ties} = \text{Min} [(16 \times (0.625 \text{ in})), (48 \times (0.375 \text{ in})), \text{Min} ((48 \text{ in}), (48 \text{ in}))]$$

$$s_{ties} = 10 \text{ in}$$

Summary:

Main reinforcement: **14 - #5 (0.625 in)**

Axial Compression Strength (ACI 318-19, LRFD)22.4.2.2 ϕP_N - Allowable axial compressive strength

$$\phi P_N = \phi 0.80 [(0.85 f'_{ck} [A_g - A_{st}]) + (f_{yk} A_{st})]$$

$$\phi P_N = (0.65) \times 0.80 \times [(0.85 \times (3 \text{ ksi}) \times [(2304 \text{ in}^2) - (4.2951 \text{ in}^2)]) + ((60 \text{ ksi}) \times (4.2951 \text{ in}^2))]$$

$$\phi P_N = 3183.4 \text{ kip}$$

Ratio - Capacity

$$\text{Ratio} = \frac{P}{\phi P_N}$$

$$\text{Ratio} = \frac{(11.576 \text{ kip})}{(3183.4 \text{ kip})}$$

$$\text{Ratio} = 0.0036363$$

Status: **PASS**
Ratio: **0.000****Shear Strength (ACI 318-19, LRFD)****Parameters:** $b_w = 48 \text{ in}$ - Effective width,22.5.2.2 d - Effective depth

$$d = 0.80 D$$

$$d = 0.80 \times (48 \text{ in})$$

$$d = 38.4 \text{ in}$$

22.5.5.1.3 λ_s - size effect modification factor

$$\lambda_s = \text{MIN} \left[\sqrt{\frac{2}{1 + \frac{d}{10}}}, 1 \right]$$

$$\lambda_s = \text{MIN} \left[\sqrt{\frac{2}{1 + \frac{(38.4 \text{ in})}{10}}}, 1 \right]$$

$$\lambda_s = 0.64282$$

The following variables were converted to be consistent with empirical formula $f'_{ck} = 3 \text{ ksi} \rightarrow 3000 \text{ psi}$,22.5.5.1.1 $V_{c,max}$ - Max shear strength of concrete

$$V_{c,max} = 5 \lambda_s \sqrt{f'_{ck}} b_w d$$

$$V_{c,max} = 5 \times (0.64282) \times \sqrt{(3000 \text{ psi})} \times (48 \text{ in}) \times (38.4 \text{ in})$$

$$V_{c,max} = 324.49 \text{ kip}$$

The following variables were converted to be consistent with empirical formula $f'_{ck} = 3 \text{ ksi} \rightarrow 3000 \text{ psi}$, $P = 11.576 \text{ kip} \rightarrow 11576 \text{ lbf}$,22.5.5.1.1(a) $V_{c,a}$ - Shear strength of concrete (a)

$$V_{c,a} = \left[2 \lambda_s \sqrt{f'_{ck}} + \frac{P}{6 A_g} \right] b_w d$$

$$V_{c,a} = \left[2 \times (0.64282) \times \sqrt{(3000 \text{ psi})} + \frac{(11576 \text{ lbf})}{6 \times (2304 \text{ in}^2)} \right] \times (48 \text{ in}) \times (38.4 \text{ in})$$

$$V_{c,a} = 131.34 \text{ kip}$$

The following variables were converted to be consistent with empirical formula $f'_{ck} = 3 \text{ ksi} \rightarrow 3000 \text{ psi}$,22.5.5.1.2 $V_{c,b}$ - Shear strength of concrete (b)

$$V_{c,b} = \left[2 \lambda_s \sqrt{f'_{ck}} + (0.05 f'_{ck}) \right] b_w d$$

$$V_{c,b} = \left[2 \times (0.64282) \times \sqrt{(3000 \text{ psi})} + (0.05 \times (3000 \text{ psi})) \right] \times (48 \text{ in}) \times (38.4 \text{ in})$$

$$V_{c,b} = 406.27 \text{ kip}$$

 V_c - Governing shear strength of concrete

$$V_c = \text{Min}[V_{c,max}, V_{c,a}, V_{c,b}]$$

$$V_c = \text{Min}[(324.49 \text{ kip}), (131.34 \text{ kip}), (406.27 \text{ kip})]$$

$$V_c = 131.34 \text{ kip}$$

<p>22.5.1.2</p>	<p>The following variables were converted to be consistent with empirical formula $f'_{ck} = 3 \text{ ksi} \rightarrow 3000 \text{ psi}$.</p> <p>$V_{s,a}$ - Shear strength of steel (a)</p> $V_{s,a} = 8 \sqrt{f'_{ck}} b_w d$ $V_{s,a} = 8 \times \sqrt{(3000 \text{ psi})} \times (48 \text{ in}) \times (38.4 \text{ in})$ $V_{s,a} = 807.65 \text{ kip}$ <p>A_v - Ties rebar area,</p> $A_v = \frac{\pi d_{ties}^2}{4}$ $A_v = \frac{\pi \times (0.375 \text{ in})^2}{4}$ $A_v = 0.11045 \text{ in}^2$ <p>22.5.8.5.3 $V_{s,b}$ - Shear strength of steel (b)</p> $V_{s,b} = \frac{2 A_v f_{ywk} d}{s_{ties}}$ $V_{s,b} = \frac{2 \times (0.11045 \text{ in}^2) \times (60 \text{ ksi}) \times (38.4 \text{ in})}{(10 \text{ in})}$ $V_{s,b} = 50.894 \text{ kip}$ <p>V_s - Governing shear strength of steel</p> $V_s = \text{MIN}[V_{s,a}, V_{s,b}]$ $V_s = \text{MIN}[(807.65 \text{ kip}), (50.894 \text{ kip})]$ $V_s = 50.894 \text{ kip}$ <p>22.5.1.1 ϕV_n - Allowable shear strength</p> $\phi V_n = \phi (V_c + V_s)$ $\phi V_n = (0.65) \times ((131.34 \text{ kip}) + (50.894 \text{ kip}))$ $\phi V_n = 118.45 \text{ kip}$ <p>Considering x-direction:</p> <p>$V_{max} = 15.36 \text{ kip}$ - Maximum shear force in the x-direction, Ratio - Capacity</p> $\text{Ratio} = \frac{V_{max}}{\phi V_n}$ $\text{Ratio} = \frac{(15.36 \text{ kip})}{(118.45 \text{ kip})}$ $\text{Ratio} = 0.12967$	<p>Status: PASS Ratio: 0.130</p>
<p>14.5.2.1b</p>	<p>Flexural Strength (ACI 318-19, LRFD)</p> <p>S_m - Section modulus</p> $S_m = \frac{b D^2}{6}$ $S_m = \frac{(48 \text{ in}) \times (48 \text{ in})^2}{6}$ $S_m = 18432 \text{ in}^3$ <p>$\lambda = 1$ - Concrete modification factor (Normal concrete), Allowable flexural strength: M_n shall be the lesser of: $\phi M_{n,1}$</p> $\phi M_{n,1} = \phi \times 5 \times \lambda \times \sqrt{f'_c} \times S_m$ $\phi M_{n,1} = 0.65 \times 5 \times 1 \times \sqrt{(3 \text{ ksi})} \times 18432.001 \text{ in}^3$ $\phi M_{n,1} = 273.423 \text{ kip ft}$ <p>$\phi M_{n,2}$</p> $\phi M_{n,2} = 0.85 f'_c S_m$	

$$\phi M_{n,z} = \phi S_x F_y$$

$$\phi M_{n,z} = (0.65) \times 0.85 \times (3 \text{ ksi}) \times (18432 \text{ in}^3)$$

$$\phi M_{n,z} = 2545.9 \text{ kipft}$$

Therefore,

ϕM_n - Allowable flexural strength,

$$\phi M_n = \text{MIN}[\phi M_{n,1}, \phi M_{n,2}]$$

$$\phi M_n = \text{MIN}[(273.42 \text{ kipft}), (2545.9 \text{ kipft})]$$

$$\phi M_n = 273.42 \text{ kipft}$$

Considering x-direction:

$M_{max} = 56.608 \text{ kipft}$ - Maximum moment in the x-direction,

Ratio - Capacity

$$\text{Ratio} = \frac{M_{max}}{\phi M_n}$$

$$\text{Ratio} = \frac{(56.608 \text{ kipft})}{(273.42 \text{ kipft})}$$

$$\text{Ratio} = 0.20704$$

Status: **PASS**
Ratio: **0.210**